

SHINING HILL ESTATE COLLECTION, INC. Shining Hill Estates, Phase 3, Town of Aurora

Transportation Mobility Plan

CONSULTING

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Attention: Mr. Paul Bailey

## Shining Hill Estates, Phase 3, Town of Aurora <br> Transportation Mobility Plan

Dear Mr. Bailey:

Please find enclosed a copy of our draft Transportation Mobility Plan prepared for Phase 3 of the Shining Hill Estates development in Aurora.

Should you have any questions or wish to discuss our findings, please contact me at (416) 229-4647, extension 2373, or at bhooton@dillon.ca.

Yours sincerely,

## DILLON CONSULTING LIMITED



Brent Hooton, Dipl.T.
Project Manager

Our File: 21-1332

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### 1.0 Introduction

## $1.1 \quad$ Purpose

Dillon Consulting Limited (Dillon) has been retained by Shining Hill Estate Collection, Inc. to prepare a transportation mobility plan (TMP) for Phase 3 of the proposed Shining Hill Estates development. The Phase 3 lands are within the town of Aurora, north of St. John's Sideroad opposite Willow Farm Lane. The development includes 88 detached residential lots, a medium density block anticipated to include approximately 200 units, and the repurposing of an existing residence for use as a private girls' school (St. Anne's School).

Background
In 2019, Dillon prepared a TMP ${ }^{1}$ for the overall Shining Hill Estates concept plan, which straddles the boundary of the towns of Newmarket and Aurora and would form much of the remaining undeveloped lands between Bathurst Street and Yonge Street, from St. John's Sideroad approximately 1.4 km northerly. A preliminary concept plan prepared by Malone Given Parsons Ltd. (MGP) envisioned approximately 3,500 residential units, a service commercial block, a school, and an open space / natural heritage system including a potential trail network. Access to the ultimate development area is proposed to Bathurst Street, St. John's Sideroad and Yonge Street (via Street "A", now known as Bennington Road, being constructed for Phase 1).

Phase 1 is located on the west side of Yonge Street south of Joe Persechini Drive and is currently under construction. Phase 2 is located on the north side of St. John's Sideroad east of Cliff Trail and is currently in the approval stage. Dillon has previously prepared traffic reports for both of these phases.

Since that time, the development concept plan has changed slightly, and the applicant is seeking Official Plan designation and Draft Plan of Subdivision approval for Phase 3, located within the town of Aurora.

Appendix A contains the updated overall concept plan and the proposed Draft Plan of Subdivision. Figure 1 illustrates the location of the site in relation to the surrounding road network and the remainder of the development lands.

[^0]Figure 1: Site Location

## 1.3 <br> Scope of Analysis



The study area consists of the following intersections:

- Bathurst Street at St. John's Sideroad;
- St. John's Sideroad at Willow Farm Lane and the proposed north/south collector road; and
- Yonge Street at St. John's Sideroad.

Analyses have been prepared for the AM and PM peak hours of a typical weekday.

Two horizon years have been assessed:

- A 2023 horizon year, reflecting the proposed build-out year; and
- A 2028 horizon year, or five years following build-out.

Shining Hill Estate Collection, Inc.

## 2.0 Existing Conditions

## 2.1 Existing Road Network

The road network in the study area is affected by two features:

- The original concession road network resulting in east-west and north-south arterials at relatively consistent 2-kilometre spacing; and
- The historic town centres and surrounding older residential areas of Newmarket and Aurora, located near Main Street and Water Street, and near Yonge Street and Wellington Street, respectively.

North-south travel in the study area is via Yonge Street and Bathurst Street. More broadly, Bayview Avenue is also available as the next concession road east of Yonge Street. In the study area, both Bathurst Street and Yonge Street are arterial roads with four-lane cross-sections; Bathurst Street has a 70 km/h speed limit, while Yonge Street has a $60 \mathrm{~km} / \mathrm{h}$ speed limit. However, while Bathurst Street has relatively consistent characteristics through Newmarket and Aurora, Yonge Street has varying characteristics and functions, serving as a suburban arterial with a primary traffic movement function through Newmarket and northern Aurora but a historic main street function within central Aurora. In a similar fashion, Bayview Avenue is a predominantly suburban arterial with a primary traffic movement function through Aurora and southern York Region, but in central Newmarket it becomes Prospect Street, a two-lane primary collector road through an older residential area east of the town centre. As such, while all three streets serve north-south travel through York Region, Bathurst Street is the only north-south arterial offering a continuous high-capacity route through both towns.

Yonge Street is also currently in transition, with investments in transit service and infrastructure that are intended to change the characteristics of the street to a more urban context that supports transit and active transportation rather than focusing on traffic movement.

East-west travel in the study area is via St. John's Sideroad ( $18^{\text {th }}$ Sideroad west of Bathurst Street), an arterial road under the jurisdiction of York Region. It has a four-lane urban cross-section through the eastern part of Aurora (east of Yonge Street), but a two-lane rural cross-section west of Yonge Street. It has a $60 \mathrm{~km} / \mathrm{h}$ posted speed limit, except for the section between Yonge Street and Industrial Parkway, which is posted at $50 \mathrm{~km} / \mathrm{h}$.

The local and collector road network in the developed areas surrounding the subject lands are characterized by a hierarchical and curvilinear street network that is typical for a suburban environment. The primary street of relevance to the subject development is Willow Farm Lane, a collector road that begins at St. John's Sideroad roughly 450 metres west of Yonge Street and then curves westerly and continues through the residential subdivision south of St. John's Sideroad. It has a two-lane crosssection and a posted speed limit of $40 \mathrm{~km} / \mathrm{h}$. It intersects with St. John's Sideroad at a two-way stop
controlled intersection. While it is not anticipated to be used by site traffic, it is relevant in that the site's proposed north-south collector would intersect with St. John's Sideroad opposite Willow Farm Lane.

Northern York Region is served by two north-south 400-series provincial highways:

- Highway 400 is roughly 7 km west of Bathurst Street. Access from the study area is via $18^{\text {th }}$ Sideroad / Lloydtown-Aurora Road (the westerly continuation of St. John's Sideroad).
- Highway 404 is roughly 5 km east of Yonge Street. St. John's Sideroad crosses Highway 404 but does not currently interchange with it. Access from the study area is either via Mulock Drive ( 2 km north of St. John's Sideroad) or via Wellington Street (2 km south of St. John’s Sideroad).

Figure 2 illustrates the existing traffic control and lane configuration at the primary intersections within the study area.

Figure 2: Existing Intersection Geometry and Traffic Control


## Existing Active Transportation Infrastructure

Much of the surrounding area is rural or has been developed with limited development at very low densities, and the on-street active transportation infrastructure is limited.

- Yonge Street:
- North of Joe Persechini Drive, sidewalks exist on both sides of the road.
- South of Joe Persechini Drive, a sidewalk extends 350 metres southerly on the east side of the street to the entrance to the Nokiidaa Trail. A sidewalk will also be built on the west side through this section (to the future Bennington Road) as part of the development of Phase 1.
- Between Bennington Road and St. John's Sideroad, no sidewalks exist other than a 150-metre section on the east side between St. John's Sideroad and the Hadley Grange driveway. There are paved shoulders that could be used by cyclists, although they are not signed or marked as cycling facilities.
- South of St. John's Sideroad, a sidewalk exists on the west side of the road.
- Bathurst Street:
- No sidewalks or bicycle facilities exist within the study area.
- St. John's Sideroad:
- No sidewalks or bicycle facilities west of Yonge Street, other than a sidewalk on the south side of the bridge over Tannery Creek, immediately west of Yonge Street.
- East of Yonge Street, a sidewalk exists on the south side of the road, and a sidewalk and bicycle path exist on the north side of the street.

All signalized intersections in the study area have crosswalks and pedestrian signals.

Beyond the study area, there is an extensive network of off-street bicycle paths and trails in the subdivisions to the north, south and east.

### 2.3 Existing Transit Network

2.3.1

York Region Transit (YRT) / VIVA
Local transit service in the study area is provided by York Region Transit (YRT). ${ }^{2}$ Figure 3 illustrates the bus routes operating within the study area.

Three different routes operate along Yonge Street through the study area:

- VIVA Blue is a limited-stop bus rapid transit (BRT) route that operates along Yonge Street between Davis Drive in Newmarket and Finch subway station in Toronto. It generally operates with frequent service and with limited, dedicated stops. Dedicated median lanes ("rapidways") are currently under construction along portions of the route in Newmarket and Richmond Hill, including through part of the study area (through the intersection with Mulock Drive). The only stop within the vicinity of the subject lands is at Joe Persechini Drive.
- The VIVA BRT service is supplemented by local service on two routes following Yonge Street through Newmarket and Aurora: 98 Yonge and 96 Keele-Yonge. Both of these routes operate less frequently but stop at additional locations not served by VIVA. In the vicinity of the site, this includes the stops on Yonge Street at St. John's Sideroad. 98 Yonge operates 7 days per week along Yonge Street between Green Line and Finch subway station. 96 Yonge-Keele operates weekdays only; it also follows Yonge Street through Newmarket and Aurora but then turns westerly to Keele Street, which it follows to York University.

[^1]Local service in north Aurora is provided by 31 Aurora North. This route operates in a clockwise loop predominantly through the northwest part of Aurora, with a stop at Yonge Street and St. John's Sideroad. It operates during weekday peak periods only.

Table 1 lists the operating hours and scheduled headway (interval between buses) on each of the routes listed above. To provide additional context related to typical transit service conditions in northern York Region, and recognizing the network effect of transit service, the operating periods and headways are also listed for other routes operating in Aurora. Most routes operate at infrequent headways of 30 minutes or greater, and service is limited on Sundays. Most routes also operate at irregular headways (e.g., 41 minutes) that result in buses arriving at different times each hour, rather than clockface headways that allow for consistent schedules from one hour to the next (e.g., at 17 and 47 minutes past each hour).

Figure 3: YRT/VIVA Network in Study Area


Table 1: Existing Transit Headways

| Route | Scheduled headway (minutes) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Weekday |  |  |  |  | Saturday |  |  |  |  | Sunday |  |  |  |  |
|  | AM | Mid | PM | Eve. | Late | Early | Morn. | Aft. | Eve. | Late | Early | Morn. | Aft. | Eve. | Late |
| Routes within the study area: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| VIVA Blue | 7.5 | 9 | 7.5 | 7.5 | 18 | 16 | 9 | 9 | 9 | 19 | - | 10.5 | 10.5 | 10.5 | 22 |
| 98 Yonge | 37 | 52 | 39 | 39 | 36 | 39 | 39 | 50 | 42 | 47 | 40 | 40 | 45 | 44 | 47 |
| 96 Keele-Yonge | 32 | 32 | 25 | 27 | 32 | - | - | - | - | - | - | - | - | - | - |
| 31 Aurora North | 35 | - | 35 | - | - | - | - | - | - | - | - | - | - | - | - |
| Other routes in Aurora: |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 32 Aurora South | 30 | 60 | 29 | - | - | - | - | - | - | - | - | - | - | - | - |
| 33 Wellington | 53 | 73 | 53 | 53 | - | 66 | 66 | 66 | 66 | - | - | - | - | - | - |
| 33A Wellington | 30 | 71 | 30 | 30 | - | 66 | 66 | 66 | 66 | - | - | - | - | - | - |
| 222 Aurora-Newmarket GO Shuttle | 30* | - | 30* | - | - | - | - | - | - | - | - | - | - | - | - |

*AM peak hour: southbound only; PM peak hour: northbound only

GO Transit
Commuter rail service to Toronto is provided via the Barrie GO line. The closest GO station to the subject site is the Aurora GO station, approximately 2 km south of St. John's Sideroad. The station is located on the south side of Wellington Street, 625 metres east of Yonge Street. It has a parking supply of 1,382 spaces (including 847 spaces in a parking garage), as well as a kiss-and-ride lot.

Under typical (pre-COVID) conditions, trains operate about every 15 to 30 minutes toward Toronto during the AM peak period, hourly during the morning and early afternoon, and hourly during the early evening. On the return trip from Toronto, trains operate hourly during the midday and early evening, and about every half hour during the PM peak period. There is also hourly train service in both directions on weekends. At times when trains are not operating, service is provided by GO buses that stop at the Aurora GO station.

### 2.4 Existing Traffic Volumes

Existing traffic volumes were carried forward from the 2019 TMP prepared by Dillon for the overall Shining Hill development area. This was in part to maintain consistency with previous analysis, and in part due to atypical traffic conditions resulting from the ongoing COVID-19 pandemic.

For the 2019 study, turning movement counts were undertaken on Wednesday, July 31, 2019 at the following intersections:

- Bathurst Street and St. John's Sideroad;
- St. John's Sideroad and Willow Farm Lane; and
- Yonge Street and St. John's Sideroad.

The surveys were undertaken for Dillon by Horizon Data Services Limited (HDSL) and were conducted from 7:00-9:00 AM and from 4:00-6:00 PM. The detailed count data are provided in Appendix B.

Figure 4 illustrates the peak hour traffic volumes surveyed at each intersection.

Figure 4: Existing Traffic Volumes (Surveyed)


The traffic volumes at the St. John's Sideroad intersections with Bathurst Street and with Yonge Street were compared against historical turning movement count data collected by Dillon in December 2015 and May / June 2017 as part of the applications for Phases 1 and 2. It was observed that the July 2019 data were understated on Bathurst Street and Yonge Street, and to a lesser extent on St. John's Sideroad, during the AM peak hour. Volumes on Yonge Street also appeared to be understated during the PM peak hour. It is possible that the 2019 volumes were understated due to the different months when the counts were undertaken (July vs. December, May and June); it is also possible that the traffic volume on Yonge Street reflected upstream constraints due to construction that was being undertaken at that time for the Yonge North VIVA rapidway. In the 2019 TMP, for analysis purposes the 2017 counts were used, and the volumes were increased to reflect two years of background traffic growth (using the same rates and method as documented in Section 3.2.1). For consistency with the 2019 study, these volumes were carried forward and used in the current study.

Figure 5 illustrates the existing peak hour traffic volumes after making the adjustments noted above.

Figure 5: Existing Traffic Volumes (Adjusted)


### 2.5 Existing Pedestrian Activity

Pedestrian volumes were recorded as part of the July 2019 traffic surveys referenced in Section 2.4. Table 2 lists the number of pedestrians observed in each crosswalk during the AM and PM peak hours. Pedestrian activity at the intersections in the study area was observed to be negligible. At Yonge Street and St. John's Sideroad, one pedestrian crossing was observed approximately every three to five traffic signal cycles. No pedestrians were observed at the other two intersections.

Table 2: Existing Pedestrian Crossing Activity

| Intersection | AM peak hour |  |  |  |  | PM peak hour |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | North leg | South leg | West leg | East <br> leg | Total | North leg | South leg | West leg | East <br> leg | Total |
| Bathurst Street at St. John's Sideroad | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Yonge Street at St. John's Sideroad | 0 | 2 | 4 | 0 | 6 | 2 | 3 | 5 | 1 | 11 |
| St. John's Sideroad at Willow Farm Lane | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

## 2.6 <br> Existing Cycling Activity

Cyclists were counted as part of the July 2019 traffic surveys referenced in Section 2.4. The number of cyclists observed was minimal. Over the full four-hour survey period, the following numbers of cyclists were observed in total at each intersection:

- 7 cyclists at Bathurst Street and St. John's Sideroad;
- 6 cyclists at Yonge Street and St. John's Sideroad; and
- 1 cyclist at St. John's Sideroad and Willow Farm Lane.


## 2.7 <br> Existing Modal Split

The existing modal split in the surrounding area was determined from data in the 2016 Transportation Tomorrow Survey (TTS) database. The modal split was calculated for home-based trips made by residents in Newmarket and Aurora, and reflects both inbound and outbound trips during the three-hour AM and PM peak periods. Table $\mathbf{3}$ presents the unadjusted modal split results as extracted from the TTS database.

Table 3: Existing Modal Split (Unadjusted)

| Primary travel mode: | AM peak hour |  | PM peak hour |  |
| :--- | :---: | :---: | :---: | :---: |
|  | In | Out | In | Out |
| Auto driver | $85 \%$ | $66 \%$ | $74 \%$ | $68 \%$ |
| Auto passenger | $7 \%$ | $13 \%$ | $12 \%$ | $27 \%$ |
| Taxi passenger | $1 \%$ | $0 \%$ | $0 \%$ | $0 \%$ |
| Local transit | $2 \%$ | $4 \%$ | $3 \%$ | $0 \%$ |
| GO rail + local transit | $0 \%$ | $1 \%$ | $2 \%$ | $0 \%$ |
| GO rail only | $0 \%$ | $3 \%$ | $3 \%$ | $0 \%$ |
| School bus | $0 \%$ | $4 \%$ | $1 \%$ | $0 \%$ |
| Walking | $5 \%$ | $7 \%$ | $5 \%$ | $3 \%$ |
| Cycling | $2 \%$ | $1 \%$ | $0 \%$ | $1 \%$ |

Note: Numbers may not add to $100 \%$ due to rounding.

A closer examination of the transit component of the TTS results indicates that the transit modal split is overstated when the point of reference is the "home" end of the trip:

- "GO rail" trips are largely made by transit, but the "home" end of the trip may involve use of a private vehicle to travel to and from the train station.
- For "Joint GO rail and local transit" trips, the "local transit" component does not necessarily refer to the "home" end of the trip; it can also refer to park-and-ride / kiss-and-ride trips where the rider transferred to the TTC subway after arriving at Union Station.
- "Local transit" trips similarly do not necessarily indicate use of YRT or VIVA services. This category is also used for trips where the rider drove to (or was dropped off at) a subway station in Toronto and completed the rest of their trip on transit, but began their trip in a private vehicle.

The TTS transit database, which uses the same data set as the main TTS database, was referenced for outbound AM peak period trips to determine the access mode to transit (to determine the proportion of GO trips involving a private vehicle) and to determine the correlation between first and second links on transit trips (to determine how many transit trips begin locally on a YRT or VIVA bus vs. how many start at a remote point on a TTC bus or subway line). The following was observed for outbound trips during the AM peak period:

- GO rail passengers access the GO station via the following modes:
- 55\% - auto driver (park-and-ride)
- $17 \%$ - auto passenger (kiss-and-ride)
- 14\% - walking
- 12\% - transfer from YRT
- 2\% - bicycle
- Although 6\% of trips are identified as being on "local transit," only 70\% of these trips begin locally on YRT/VIVA while the remaining $30 \%$ are passengers that board the TTC subway at Union Station or at an outlying station with park-and-ride facilities.

Table 4 presents the existing modal split as experienced at the "home" end of the trip.

Table 4: Existing Modal Split ("Home" End of Trip)

| Primary travel mode: | AM peak hour |  | PM peak hour |  |
| :--- | :---: | :---: | :---: | :---: |
|  | In | Out | In | Out |
| Auto driver | $85 \%$ | $68 \%$ | $76 \%$ | $68 \%$ |
| Auto passenger | $7 \%$ | $14 \%$ | $13 \%$ | $27 \%$ |
| Taxi passenger | $1 \%$ | $0 \%$ | $0 \%$ | $0 \%$ |
| Local transit | $2 \%$ | $5 \%$ | $4 \%$ | $0 \%$ |
| School bus | $0 \%$ | $4 \%$ | $1 \%$ | $0 \%$ |
| Walking | $5 \%$ | $8 \%$ | $5 \%$ | $3 \%$ |
| Cycling | $2 \%$ | $1 \%$ | $0 \%$ | $1 \%$ |

Note: Numbers may not add to 100\% due to rounding.

## 3.0 <br> Future Background Conditions

This section identifies changes to the transportation network that are proposed in the broader study area, and establishes the magnitude of traffic growth under future background conditions (i.e., traffic volumes that are forecasted without the proposed development in place).

Two future horizon years have been assessed:

- 2023, corresponding to the estimated build-out year; and
- 2028, corresponding to five years following build-out.


### 3.1 Future Transportation Network Changes

The following sections list changes that are planned to the transportation network in and around the study area, and identify how those changes were reflected in the future background analyses.

St. John's Sideroad Widening
In their most recent Transportation Master Plan, the Region of York identified the widening of St. John's Sideroad to a 4-lane cross-section between Bathurst Street and Yonge Street. The Transportation Master Plan tentatively identified this widening for the period between 2027 and 2031. This widening is also reflected in the Region's long-range transportation model (and therefore the model's growth forecasts, which formed the basis of the growth rates derived in Section 3.2.1, reflect the availability of this added capacity). It is anticipated that this project would also include the road's conversion from a rural to an urban cross-section including curb and gutter along with active transportation facilities. However, this widening is unfunded and unscheduled, and is not part of the Region's 10-year capital program. Further, an environmental assessment still needs to be undertaken to confirm the need for roadway modifications and to establish a preferred design / cross-section and a preferred means for undertaking the modifications (e.g., widen symmetrically; widen on north or south side).

Given that the project has been identified but not funded or programmed, the baseline future background analyses have been undertaken assuming the existing road cross-section, with the expectation that the planned widening could be considered as mitigation.

St. John's Sideroad / Highway 404 Interchange
The Region's Transportation Master Plan also identifies the future construction of an interchange at Highway 404 and St. John's Sideroad. Although the Region is protecting for this interchange in terms of property and policy measures (e.g., access management), there is similarly no funding or schedule associated with an interchange and it is not being actively pursued. As such, the trip distribution for site traffic has assumed that an interchange is not present.

Mulock GO Station
Metrolinx is planning for the construction of a new GO station on the south side of Mulock Drive. Current concepts for the station envision an unspecified number of parking spaces; kiss-and-ride facilities; and a bus loop. Access is envisioned from Mulock Drive and from Bayview Avenue via existing and proposed local streets connecting to those roadways. The new Mulock GO station may be an alternative to the Aurora GO station for Phase 3 residents and has been considered as such in the trip distribution of resident trips.

## $3.2 \quad$ Background Traffic Growth

Future background traffic volumes are calculated by applying a background growth rate to traffic volumes on major roadways in the study area, and adding site-specific traffic volumes generated by developments in the study area.

General Background Growth
Background traffic growth rates were derived from the Region's long-range transportation model. The Region provided AM peak hour model runs for the 2016, 2021, 2031 and 2041 horizon years. From the model results, the following annual growth rates were estimated during the AM peak hour:

- Bathurst Street: $0.5 \%$ northbound / $2.0 \%$ southbound
- Yonge Street: $0.5 \%$ northbound / $1.0 \%$ southbound
- St. John's Sideroad: $2.0 \%$ eastbound / $1.0 \%$ westbound

The growth rates listed above were applied to midblock volumes upstream and downstream from the major arterial intersections, and then the calculated approach and departure growth was distributed proportionally between the individual intersection turning movements.

The Region's model reflects AM peak hour conditions. For PM peak hour conditions, the AM peak hour growth rates were reversed (e.g., the AM peak hour's northbound growth rate was applied to the southbound direction during the PM peak hour).

Background Development Traffic

Active development applications in the towns of Newmarket and Aurora, within a radius of approximately 2.5 km of the site (or just over one concession), were reviewed to determine the potential to affect traffic volumes at the study area intersections. (Developments beyond this distance would have more opportunity to disperse before reaching the study area and would therefore have lower impact, and were assumed to be captured as part of the general background growth rates.) The following developments were considered:

- Phases 1 and 2 of the Shining Hill Estates development;
- A proposed townhouse development on the northeast corner of Yonge Street and St. John's Sideroad; and
- Several residential developments in the downtown area of Aurora.

Shining Hill Estates, Phases 1 and 2
Phase 1 of the Shining Hill Estates development is located southwest of Yonge Street and Joe Persechini Drive and consists of 174 detached, semi-detached and townhouse units. These units were not present while the traffic surveys were undertaken and therefore have been added to the existing traffic volumes.

Phase 2 is located on the north side of St. John's Sideroad, and is planned to consist of 90 detached residential units on a network of private roadways. A single unsignalized full-movement access to St. John's Sideroad is planned approximately 750 metres west of Willow Farm Lane. It will not have a vehicular connection to the remainder of the Shining Hill Estates collector road network.

Traffic projections for Phase 1 were most recently documented in a February 2018 letter report. Traffic projections for Phase 2 were most recently documented in a May 2019 letter report. Figure 6 illustrates the traffic volumes associated with Phases 1 and 2 of the Shining Hill Estates development. These volumes were carried forward for the Phase 3 background analyses.

Figure 6: Background Development Traffic (Shining Hill Estates Phases 1 and 2)


Proposed Townhouse Development, Yonge Street and St. John's Sideroad
A 68-unit townhouse development is proposed on the northeast corner of Yonge Street and St. John's Sideroad. Access would be via two existing full-movement accesses leading to Hadley Grange seniors apartment complex. The volume of traffic generated by this development was estimated using trip generation rates published by the Institute of Transportation Engineers (ITE) in the Trip Generation Manual ( $10^{\text {th }}$ edition). Trips were generated using ITE land use code 220 ("Multifamily Housing (Low-

Rise)"). The development is anticipated to generate 31 trips during the AM peak hour and 38 trips during the PM peak hour; Table 5 presents how these volumes were calculated.

Table 5: Background Development Trip Generation (Yonge Street and St. John's Sideroad Townhouses)

|  | AM peak hour |  |  | PM peak hour |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | In | Out | Total | In | Out | Total |
|  | $23 \%$ | $77 \%$ | 0.46 | $63 \%$ | $37 \%$ | 0.56 |
| Trips generated (68 units) | 7 | 24 | 31 | 24 | 14 | 38 |

Trips were distributed using the same directional distribution used for the subject site (see Section 4.3).

Trips were assigned logically to the two driveways. Only west- and south-oriented trips were assumed to travel through the Yonge Street and St. John's Sideroad intersection; north- and east-oriented trips were assumed to use the accesses north and east of the intersection, respectively.

Figure 7 illustrates the expected study area traffic volumes associated with the proposed residential development at Yonge Street and St. John's Sideroad.

Figure 7: Background Development Traffic (Yonge Street and St. John's Sideroad Townhouses)


Downtown Aurora Residential Development
Numerous development applications are currently active for residential development in the area of downtown Aurora. While most of these are relatively minor in size, collectively they add to approximately 900 units, broken down approximately as follows:

- 11 single detached units;
- 483 townhouse units; and
- 406 apartment/condominium units.

The volume of traffic generated by these developments was estimated using trip generation rates from the Trip Generation Manual ( $10^{\text {th }}$ edition). Trips were generated using ITE land use codes 210 ("SingleFamily Detached Housing"), 220 ("Multifamily Housing (Low-Rise)") and 221 ("Multifamily Housing (MidRise)"). All developments combined are anticipated to generate 376 trips during the AM peak hour and 460 trips during the PM peak hour;
Table 6 presents how these volumes were calculated.

Table 6: Background Development Trip Generation (Downtown Aurora)

|  | AM peak hour |  |  | PM peak hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | In | Out | Total | In | Out | Total |
| Single detached homes: |  |  |  |  |  |  |
| Trip generation rate (per unit) | 25\% | 75\% | 0.74 | 63\% | 37\% | 0.99 |
| Trips generated (11 units) | 2 | 6 | 8 | 7 | 4 | 11 |
| Townhouses: |  |  |  |  |  |  |
| Trip generation rate (per unit) | 23\% | 77\% | 0.46 | 63\% | 37\% | 0.56 |
| Trips generated (483 units) | 51 | 171 | 222 | 170 | 100 | 270 |
| Apartments/condominiums: |  |  |  |  |  |  |
| Trip generation rate (per unit) | 26\% | 74\% | 0.36 | 61\% | 39\% | 0.44 |
| Trips generated (406 units) | 38 | 108 | 146 | 109 | 70 | 179 |
| Total trips: | 91 | 285 | 376 | 286 | 174 | 460 |

There is a VIVA stop at Wellington Street in downtown Aurora, and a variety of complementary nonresidential uses that could attract some walking trips. Notwithstanding, to be conservative a modal split adjustment was not applied.

Trips were distributed using the same directional distribution used for the subject site (see Section 4.3). It was assumed that 50\% of north-oriented trips would travel north-south along Yonge Street through the study area; all other trips were assumed to not enter the study area.

Figure 8 illustrates the expected study area traffic volumes associated with the proposed residential developments in the downtown Aurora area.

Figure 8: Background Development Traffic (Downtown Aurora)


### 3.2.2.4 Summary of Background Development Traffic

Figure 9 presents the total volume of background development traffic assigned through the study area road network.

Figure 9: Combined Background Development Traffic


### 3.3 Future Background Traffic Volumes

Future background traffic volumes were calculated by applying the background growth rates to existing volumes up to the 2023 and 2028 horizons, and adding traffic generated by the identified background developments. The resulting future background traffic volumes are presented in Figure 10 (2023 horizon) and Figure 11 (2028 horizon).

Figure 10: Future Background Traffic Volumes (2023)


Figure 11: Future Background Traffic Volumes (2028)


### 4.0 Total Future Traffic Volumes <br> 4.1 Proposed Development

Phase 3 of the Shining Hill Estates development is within the town of Aurora, north of St. John's Sideroad opposite Willow Farm Lane. The development is proposed to include 88 detached residential lots, a medium density block anticipated to include approximately 200 units, and the repurposing of an existing residence for use as a private girls' school (St. Anne's School).

Access to Phase 3 will be via a new north-south collector road (Street " $A$ ") extending northerly from the existing intersection of St. John's Sideroad and Willow Farm Lane. In the interim, it will end at the Newmarket / Aurora boundary at the north end of the Phase 3 area. In the longer term, Street " $A$ " is planned to be extended farther to the north and connect to a new east-west collector extending between Bathurst Street and Yonge Street (Bennington Road, being constructed as part of Phase 1).

### 4.2 Site Trip Generation

This section primarily addresses automobile trip generation. Multi-modal trip generation is addressed in Section 7.1.
4.2.1

## Residential Units

Trips generated by the residential units were estimated based on trip generation rates published by ITE in the Trip Generation Manual, $10^{\text {th }}$ edition. Trip generation rates were referenced for the following land use codes:

- 210 - Single-Family Detached Housing (used for trips generated by the proposed single-family units);
- 221 - Multi-Family Housing (Mid-Rise) (used for trips generated by the proposed apartment units).

Table $\mathbf{7}$ presents the trip generation calculations applied to the residential portion of the development.

Table 7: $\quad$ Site Trip Generation (Residential Units)

|  | AM peak hour |  |  | PM peak hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | In | Out | Total | In | Out | Total |
| Single detached homes: |  |  |  |  |  |  |
| Trip generation rate (per unit) | 25\% | 75\% | 0.74 | 63\% | 37\% | 0.99 |
| Trips generated (88 units) | 17 | 49 | 66 | 55 | 32 | 87 |
| Apartments/condominiums: |  |  |  |  |  |  |
| Trip generation rate (per unit) | 26\% | 74\% | 0.36 | 61\% | 39\% | 0.44 |
| Trips generated (200 units) | 19 | 53 | 72 | 54 | 34 | 88 |
| Total trips: | 36 | 102 | 138 | 109 | 66 | 175 |

Shining Hill Estate Collection, Inc.
Shining Hill Estates, Phase 3, Town of Aurora


Trips generated by St. Anne's School were estimated from first principles. Trips were generated separately for students (pick-up/drop-off trips) and for staff.

At the five-year horizon, the school anticipates to have a population of 500 , comprised of approximately 435 students and 65 staff (i.e., 6.75 students per staff member). Enrolment will be lower in the first year: currently estimated at approximately 100 students, which would correspond to 15 staff assuming the same ratio.

Given the nature of the school, most students will reside outside walking distance from the school, and most will be picked up and dropped off by a parent (or guardian). This will generate one inbound and one outbound trip per student, both in the morning and in the afternoon.

The school does not anticipate offering busing in the first year, but expects to operate one to two school buses by the fifth year, which they anticipate could attract between 40 and 80 students. For analysis purposes, approximately $15 \%$ of students have been assumed to ride the school bus.

The remaining vehicle pick-up and drop-off demand will be offset by three factors:

- Families with more than one girl enrolled at the school will arrive with multiple students per vehicle;
- Given the relationship between the two schools, some families may also have sons enrolled at St.

Andrew's College and would therefore already be traveling in the study area; and

- In future years, the school proposes to offer school busing (for an additional fee).

For analysis purposes, it has been assumed that, on average:

- One-third of families have two girls enrolled at the school, resulting in a $25 \%$ reduction in the auto trips; and
- One-third of families have a son enrolled at St. Andrew's College, resulting in some of these trips being offset by duplication with trips being made under background conditions. A volume of traffic equivalent to one-third of the PU/DO vehicle demand was assumed to be removed from the broader study area.

Each staff member is anticipated to generate one inbound trip before school and one outbound trip after school.

Before school, it has been assumed that all trips will occur during the AM peak hour of traffic on the adjacent road network. After school, trips are expected to be more dispersed, with individual pick-up times depending on parents' work schedules and any participation in after-school extra-curricular activities. Based on an hourly distribution profile of trips to/from charter schools, published by ITE as a supplement to the Trip Generation Manual, approximately $25 \%$ of school trips have been assumed to
occur during the PM peak hour of traffic on the adjacent road network (i.e., the PM peak hour trips reflect $25 \%$ of the inverted AM peak hour trips).

Table 8: Site Trip Generation (School)

|  | 2023 |  |  |  |  |  | 2028 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AM peak hour |  |  | PM peak hour |  |  | AM peak hour |  |  | PM peak hour |  |  |
|  | In | Out | Total | In | Out | Total | In | Out | In | Out | In | Out |
| Student pick-up / drop-off (100 students in 2023; 435 students in 2028) |  |  |  |  |  |  |  |  |  |  |  |  |
| Unadjusted trips | 100 | 100 | 200 | 25 | 25 | 50 | 435 | 435 | 870 | 109 | 109 | 218 |
| Siblings traveling together | -25 | -25 | -50 | -6 | -6 | -12 | -109 | -109 | -218 | -27 | -27 | -54 |
| Total families | 75 | 75 | 150 | 19 | 19 | 38 | 326 | 326 | 652 | 82 | 82 | 164 |
| 15\% via school bus (2028 only) | 0 | 0 | 0 | 0 | 0 | 0 | -49 | -49 | -98 | -12 | -12 | -24 |
| Adjusted trips (gross) | 75 | 75 | 150 | 19 | 19 | 38 | 277 | 277 | 554 | 70 | 70 | 140 |
| Reduction in SAC trips | -25 | -25 | -50 | -6 | -6 | -12 | -92 | -92 | -184 | -23 | -23 | -46 |
| Net vehicle trips | 50 | 50 | 100 | 13 | 13 | 26 | 185 | 185 | 370 | 47 | 47 | 94 |
| Staff (15 staff in 2023; 65 staff in 2028) |  |  |  |  |  |  |  |  |  |  |  |  |
| Total trips | 15 | 0 | 15 | 0 | 4 | 4 | 65 | 0 | 65 | 0 | 16 | 16 |
| Total trips (gross): | 90 | 75 | 165 | 19 | 23 | 42 | 342 | 277 | 619 | 70 | 86 | 156 |
| Total trips (net): | 65 | 50 | 115 | 13 | 17 | 30 | 250 | 185 | 435 | 47 | 63 | 110 |

Table 9 presents the total number of trips anticipated to be generated by Phase 3 at the 2023 and 2028 horizons.

Table 9: Total Site Trip Generation

|  | AM peak hour |  |  | PM peak hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | In | Out | Total | In | Out | Total |
| 2023 horizon: |  |  |  |  |  |  |
| Residential units | 36 | 102 | 138 | 109 | 66 | 175 |
| St. Anne's School (gross) | 90 | 75 | 165 | 19 | 23 | 42 |
| Reduction in SAC trips | -25 | -25 | -50 | -6 | -6 | -12 |
| Total (gross) | 126 | 177 | 303 | 128 | 89 | 217 |
| Total (net) | 101 | 152 | 253 | 122 | 83 | 205 |
| 2028 horizon: |  |  |  |  |  |  |
| Residential units | 36 | 102 | 138 | 109 | 66 | 175 |
| St. Anne's School | 342 | 277 | 619 | 70 | 86 | 156 |
| Reduction in SAC trips | -92 | -92 | -184 | -23 | -23 | -46 |
| Total (gross) | 378 | 379 | 757 | 179 | 152 | 331 |
| Total (net) | 286 | 287 | 573 | 156 | 129 | 285 |

In 2023, the site is expected to generate approximately 303 vehicle trips during the AM peak hour and 217 vehicle trips during the PM peak hour.

By 2028, with increased enrolment at the school, the trip generation is expected to increase to approximately 757 vehicle trips during the AM peak hour and 331 vehicle trips during the PM peak hour.

After accounting for the double-counting of trips currently made to St. Andrew's College that will eventually be made to both schools, the net number of new trips made by the site is expected to be: - 253 net new vehicle trips during the AM peak hour and 205 net new vehicle trips during the PM peak hour in 2023; and

- 573 net new vehicle trips during the AM peak hour and 285 net new vehicle trips during the PM peak hour in 2028.


### 4.3 Site Traffic Distribution and Assignment

### 4.3.1 <br> Residential Trips

The same residential trip distribution was applied as in the 2019 report for the overall development. This trip distribution is based on origin-destination data from the 2016 Transportation Tomorrow Survey (TTS). The TTS data reflect inbound and outbound home-based auto driver trips made by residents of western Newmarket and Aurora during the AM and PM peak periods.

- In the 2019 analyses, the TTS auto driver trips were discounted to reflect local travel for which the trip purpose was listed as "facilitate passenger"; from the location of these trips, it appears that many of these are trips made to drop off or pick up children from school. The full development is planned to include a public elementary school in the Newmarket section north of Phase 3, and at full build-out of the development this trip purpose will be served locally within the subject lands. However, for the purpose of this analysis students will attend schools elsewhere in Aurora and the "facilitate passenger" trips were assigned to/from the south via Yonge Street.
- Conversely, the TTS auto driver trip distribution was adjusted to also reflect the auto driver or passenger component of GO train trips (i.e., a trip categorized in the TTS database as primarily involving GO rail would be experienced in the local area as an auto trip).
4.3.2

School Trips (Pick-Up/Drop-Off)
Morning drop-offs and evening pick-ups of students were distributed differently for the "home" end of the trip (carrying students) and the "return" trip (without student passengers).

The "home" end was distributed based on an estimated catchment area for students. School staff advise that they anticipate to attract students from a broad area of the northern GTA, including from Newmarket, Aurora, King, Stouffville, Markham, Richmond Hill, Thornhill, Vaughan and Caledon.

For the "return" trip, a blended distribution was developed based on some parents/guardians traveling to/from home, and other parents/guardians traveling to/from their workplace. For the workplace component, a distribution was estimated from TTS data showing the place of work for Aurora residents
commuting by automobile (or driving to a GO station), weighted to favour trips to workplaces within a range of roughly 30 to 45 minutes. (This is intended to reflect that some parents will already have driven for some time from homes outside Newmarket/Aurora, and that the "return" trip will be in addition to this.)

For the PU/DO trips involving both schools, it was assumed that parents would be slightly more likely to stop at St. Anne's School before stopping at St. Andrew's College (due to the added delay in making the northbound left turn at Yonge Street and St. John's Sideroad). The "Yonge south" component of the trip distribution for both "home" and "return" trips reflects this trip chaining between the two schools.

The trip chaining will displace existing trips that are currently made to/from St. Andrew's College. A directional distribution was estimated for these displaced trips, based broadly on the distribution for St. Anne's School but with adjustments to reflect the location of St. Andrew's College related to the study area (i.e., some displaced trips will be external only and will not travel through the study area).

The distribution of trips made by school staff was carried forward from the 2019 study, where staff trips generated by the public elementary school were assumed to be relatively evenly distributed between the cardinal directions.
4.3.4

Trip Distribution Summary
Based on the foregoing sections, Table 10 presents the trip distribution applied to residential and school PU/DO and staff trips.

Table 10: Trip Distribution

| To/from: | Residential trips |  |  |  | School PU/DO trips |  |  |  | School staff | Displaced St. Andrew's trips |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AM peak hour |  | PM peak hour |  | AM peak hour |  | PM peak hour |  |  |  |
|  | In | Out | In | All | In | Out | In | Out | All | All |
| West via $18{ }^{\text {th }}$ Sideroad | 7\% | 22\% | 22\% | 12\% | 17.5\% | 15\% | 15\% | 15\% | 20\% | 20\% |
| North via Bathurst Street | 15\% | 4\% | 9\% | 9\% | 10\% | 10\% | 10\% | 10\% | 15\% | 10\% |
| South via Bathurst Street | 10\% | 14\% | 19\% | 3\% | 15\% | 10\% | 12.5\% | 12.5\% | 15\% | 0\% |
| South via Willow Farm Lane | 0\% | 0\% | 0\% | 0\% | 5\% | 5\% | 5\% | 5\% | 0\% | 0\% |
| North via Yonge Street | 11\% | 21\% | 12\% | 24\% | 7.5\% | 7.5\% | 10\% | 5\% | 25\% | 10\% |
| South via Yonge Street | 39\% | 20\% | 12\% | 26\% | 17.5\% | 27.5\% | 17.5\% | 27.5\% | 10\% | 0\% |
| East via St. John's Sideroad | 18\% | 19\% | 26\% | 26\% | 27.5\% | 25\% | 30\% | 25\% | 15\% | 20\% |

The resulting site trips are illustrated in the following figures:

- Figure 12 illustrates the trips generated by the proposed residential units;
- Figure 13 illustrates the trips generated by the school at the 2023 horizon (including displaced St. Andrew's College trips);
- Figure 14 illustrates the trips generated by the school at the 2028 horizon (including displaced St.

Andrew's College trips);

- Figure 15 illustrates the total site trips generated at the 2023 horizon; and
- Figure 16 illustrates the total site trips generated at the 2023 horizon.

Figure 12: Site Trips (Residential Component)


Figure 13: Site Trips (St. Anne's School, 2023 Horizon)


Figure 14: Site Trips (St. Anne's School, 2028 Horizon)


Figure 15: Total Site Trips (2023 Horizon)


Figure 16: Total Site Trips (2028 Horizon)



## 4.4 <br> Total Future Traffic Volumes

Total future traffic volumes represent conditions anticipated with the proposed development in place, and are calculated by adding the site traffic volumes to the projected future background traffic volumes.
Figure 17 and Figure 18 illustrate total future traffic volumes at the 2023 and 2028 horizons, respectively.

Figure 17: Total Future Traffic Volumes (2023 Horizon)


Figure 18: Total Future Traffic Volumes (2028 Horizon)


## 5.0 Intersection Operations

Intersection operational analyses were completed for each of the four main arterial intersections using Trafficware's Synchro software (version 10). The analyses generally reflect the existing lane configurations at each intersection and current traffic signal timings obtained from the Region of York.

At signalized intersections, the volume-to-capacity (v/c) ratio, average vehicular delay, level of service and $95^{\text {th }}$ percentile queue were noted for each individual movement, and the average delay and level of service were noted for the intersection as a whole. At unsignalized (stop-controlled) intersections, the $\mathrm{v} / \mathrm{c}$ ratio, delay, level of service and $95^{\text {th }}$ percentile queue were noted for any stop-controlled movements. Level of service definitions are provided in Appendix D. Synchro analysis worksheets reports are provided in Appendix E.

At each intersection, critical movements were identified. The Region of York's Transportation Mobility Plan guidelines indicate that an individual movement or lane group is considered to be "critical" when its $\mathrm{v} / \mathrm{c}$ ratio exceeds 0.85 , or when its level of service is E or F .

Multi-modal levels of service are addressed in Section 7.0.

### 5.1 Yonge Street and St. John's Sideroad

### 5.1.1

Existing Configuration
At Yonge Street and St. John's Sideroad, two adjustments were made to better calibrate the analysis results with observations made in the field.

- The left turn saturated flow rate during the advance southbound left turn phase was increased. The unadjusted analyses resulted in a calculated capacity of 9 vehicles per cycle during the protected phase. Operations of the left turn movement were observed and videotaped over several cycles during the AM peak period, and the southbound advance phase was regularly observed to accommodate 12 vehicles per cycle. The protected saturation flow rate was increased by $28 \%$ to match observed conditions.
- The eastbound approach has two through lanes (one of which is shared with the right turn movement). However, the capacity of the eastbound approach is reduced because the second lane is only developed roughly 60 metres upstream from the stop bar. Both lanes of capacity are usable for the first 16 seconds of eastbound green, corresponding to eight vehicles discharging from both lanes. After this part of the eastbound queue is served, however, the eastbound approach is only fed by a single lane and the capacity during the remaining green interval is only half utilized. The eastbound lane utilization factor was reduced to 0.75 to better represent the existing eastbound capacity. This resulted in the eastbound through movement reaching capacity during the AM peak
hour, with a queue nearly reaching Willow Farm Lane, which matches conditions observed in the field during the AM peak hour.

Table 11 summarizes the operations at Yonge Street and St. John's Sideroad under each traffic volume scenario.

Table 11: Intersection Operations, Yonge Street and St. John's Sideroad

| Scenario: | Movement | AM peak hour |  |  |  | PM peak hour |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | v/c | LOS | Delay <br> (s/veh) | 95th $\%$ ile queue (m) | v/c | LOS | Delay (s/veh) | 95th $\%$ ile queue ( $m$ ) |
| Existing | EB left | 0.50 | C | 28.8 | 31 | 0.78 | D | 49.5 | 54 |
|  | EB through | 1.01 | E | 76.6 | 207 | 0.64 | D | 37.5 | 104 |
|  | WB left | 0.96 | F | 84.0 | 85 | 0.92 | E | 61.9 | 83 |
|  | WB through | 0.80 | D | 51.3 | 160 | 0.95 | E | 65.2 | 208 |
|  | WB right | 0.44 | A | 6.7 | 24 | 0.91 | D | 37.8 | 170 |
|  | NB left | 0.50 | D | 54.1 | 36 | 0.66 | E | 55.2 | 60 |
|  | NB through | 0.62 | D | 46.2 | 85 | 0.88 | D | 52.5 | 147 |
|  | NB right | 0.48 | B | 16.0 | 44 | 0.41 | A | 6.4 | 22 |
|  | SB left | 1.10 | F | 95.2 | 193 | 1.07 | F | 103 | 133 |
|  | SB through | 0.50 | C | 26.2 | 95 | 0.41 | C | 24.4 | 73 |
|  | SB right | 0.21 | A | 3.7 | 12 | 0.18 | A | 4.2 | 12 |
|  | Overall | - | D | 50.6 | - | - | D | 46.3 | - |
| 2023 future background | EB left | 0.60 | C | 33.8 | 34 | 0.97 | F | 85.7 | 79 |
|  | EB through | 1.13 | F | 113 | 246 | 0.68 | D | 38.3 | 115 |
|  | WB left | 1.03 | F | 102 | 94 | 1.05 | F | 93.7 | 100 |
|  | WB through | 0.85 | E | 55.6 | 184 | 1.03 | F | 84.1 | 245 |
|  | WB right | 0.46 | A | 8.1 | 30 | 1.00 | E | 58.1 | 213 |
|  | NB left | 0.55 | E | 58.0 | 38 | 0.84 | E | 75.8 | 78 |
|  | NB through | 0.66 | D | 47.4 | 91 | 0.97 | E | 65.6 | 165 |
|  | NB right | $0.51$ | B | 19.4 | 52 | 0.45 | A | 9.2 | $31$ |
|  | SB left | 1.24 | F | 148 | 222 | 1.18 | F | 141 | 151 |
|  | SB through | $0.54$ | B | $12.8$ | 38 | 0.45 | C | 25.4 | 79 |
|  | SB right | 0.24 | A | 0.8 | 0 | 0.20 | A | 4.1 | 12 |
|  | Overall | - | E | 64.4 | - | - | E | 61.1 | - |
| 2023 total future | EB left | 0.84 | E | 59.7 | 63 | 1.07 | F | 111 | 90 |
|  | EB through | 1.23 | F | 151 | 283 | 0.72 | D | 39.7 | 123 |
|  | WB left | 1.00 | F | 95.9 | 95 | 1.10 | F | 110.7 | 101 |
|  | WB through | 0.91 | E | 63.0 | 207 | 1.11 | F | 109.6 | 273 |
|  | WB right | 0.48 | A | 9.5 | 35 | 1.01 | E | 59.3 | 215 |
|  | NB left | 0.72 | E | 71.5 | 60 | 0.96 | F | 98.7 | 93 |
|  | NB through | 0.65 | D | 47.2 | 91 | 0.97 | E | 65.4 | 165 |
|  | NB right | 0.50 | C | 19.4 | 54 | 0.45 | A | 9.8 | 32 |
|  | SB left | 1.23 | F | 147.6 | 219 | 1.18 | F | 141 | 151 |
|  | SB through | 0.54 | B | 15.8 | 48 | 0.45 | C | 25.4 | 79 |
|  | SB right | 0.26 | A | 0.9 | 0 | 0.23 | A | 3.9 | 13 |
|  | Overall | - | E | 75.0 | - | - | E | 67.5 | - |

Table 11: Intersection Operations, Yonge Street and St. John's Sideroad (cont'd)

| Scenario: | Movement | AM peak hour |  |  |  | PM peak hour |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | v/c | LOS | Delay <br> (s/veh) | 95 ${ }^{\text {th }} \%$ ile queue ( $m$ ) | v/c | LOS | Delay <br> (s/veh) | 95 ${ }^{\text {th }} \%$ ile queue ( $m$ ) |
| 2028 future background | EB left | 0.69 | D | 41.8 | 38 | 1.03 | F | 99.1 | 85 |
|  | EB through | 1.22 | F | 148 | 276 | 0.71 | D | 39.5 | 122 |
|  | WB left | 1.08 | F | 118 | 101 | 1.14 | F | 126 | 108 |
|  | WB through | 0.90 | E | 61.2 | 200 | 1.12 | F | 113 | 278 |
|  | WB right | 0.48 | A | 9.2 | 35 | 1.07 | E | 78.5 | 241 |
|  | NB left | 0.62 | E | 63.0 | 44 | 0.91 | F | 88.7 | 86 |
|  | NB through | 0.67 | D | 47.8 | 93 | 1.01 | E | 75.4 | 177 |
|  | NB right | 0.55 | C | 22.8 | 60 | 0.48 | B | 11.4 | 38 |
|  | SB left | 1.33 | F | 188 | 248 | 1.21 | F | 153 | 157 |
|  | SB through | 0.56 | B | 13.7 | $42$ | 0.46 | C | 25.6 | 81 |
|  | SB right | 0.25 | A | 0.8 | 0 | 0.22 | A | 4.0 | 13 |
|  | Overall | - | F | 79.5 | - | - | E | 73.5 | - |
| 2028 total future | EB left | 1.09 | F | 124 | 87 | 1.15 | F | 137 | 100 |
|  | EB through | 1.44 | F | 239 | 347 | 0.79 | D | 42.9 | 138 |
|  | WB left | 0.98 | F | 89.4 | 87 | 1.27 | F | 175 | 121 |
|  | WB through | 1.07 | F | 100 | 262 | 1.21 | F | 144 | 305 |
|  | WB right | 0.51 | B | 13.5 | 47 | 1.07 | F | 79.7 | 243 |
|  | NB left | 0.96 | F | 113 | 80 | 1.01 | F | 111 | 98 |
|  | NB through | 0.66 | D | 47.4 | 91 | 1.01 | E | 74.7 | 176 |
|  | NB right | 0.51 | C | 21.4 | 55 | 0.48 | B | 12.1 | 40 |
|  | SB left | 1.32 | F | 183.5 | 242 | 1.21 | F | 153 | 157 |
|  | SB through | $0.56$ | B | 16.1 | 49 | 0.46 | C | 25.6 | 81 |
|  | SB right | 0.30 | A | 1.0 | OW | 0.24 | A | 3.9 | 13 |
|  | Overall | 一 | F | 109 | - | - | F | 83.1 | - |

The intersection of Yonge Street and St. John's Sideroad currently operates at a reasonable overall level of service (LOS D) during both peak hours. However, there are several movements identified as being critical from a capacity perspective:

- During the AM peak hour, the southbound and westbound left turns, and the eastbound through movement, are at or near capacity.
- During the PM peak hour, the southbound left turn is at capacity, all westbound movements are near capacity, and the northbound through movement is just above the critical threshold.

Most of the movements listed above are also critical from a level of service perspective.

As part of the previous 2019 study, Region staff specifically expressed interest in the queues on the eastbound approach during the AM peak hour. The $95^{\text {th }}$ percentile queue was calculated at 207 metres in the eastbound through lanes. However, this reflects a queue distributed between two lanes, with a combined total of 415 metres of queued vehicles. The available storage length in the outside lane is only approximately 60 to 65 metres, resulting in a 350-metre queue in the inside lane. This queue would extend approximately to the start of the westbound left turn taper for Willow Farm Lane. This calculation matches queue lengths observed during a site visit during the AM peak period in September 2019.

At the 2023 horizon, the overall level of service is anticipated to change to LOS E both under background conditions and with the development of the site. Several individual movements are expected to be at or above capacity, including most movements during the PM peak hour; as well, many movements are expected to operate at LOS E or F (whether due to capacity constraints or due to the long traffic signal cycle). Site traffic will contribute to some of these critical movements - particularly the eastbound through and left turn movements during the AM peak hour, and the eastbound left turn and westbound through movement during the PM peak hour - although most of these movements are already expected to be constrained without development of the site. The net impact of site traffic is projected to be an overall increase in delay of approximately 6 to 10 seconds per vehicle.

At the 2028 horizon, the overall level of service is anticipated to have reached LOS F during the AM peak hour under background conditions, and during the PM peak hour with development of the site. Many individual movements will continue to be critical at this horizon. In particular, the eastbound through movement and southbound left turn movement are both expected to be significantly above capacity during the AM peak hour (particularly with the addition of school drop-off traffic), as are the southbound left turn and westbound approach during the PM peak hour.

As noted in Section 3.1.1, the Region of York's most recent Transportation Master Plan recommended the widening of St. John's Sideroad to four lanes between Bathurst and Yonge Street and tentatively identified this widening to occur between 2027 and 2031. This widening is also reflected in the Region's long-range transportation model (and therefore the model's growth forecasts, which formed the basis of the growth rates derived in Section 3.2.1, reflect the availability of this added capacity). Given that this widening is unfunded and unscheduled within the Region's 10-year capital program, and that an environmental assessment still needs to be undertaken for the project, it has been assumed that mitigation will consist of adjustments to the traffic signals as a temporary measure until such time as the planned road widening can be completed.

Traffic signal timing adjustments were tested to mitigate the anticipated capacity constraints under the projected future background and total future volumes. The following changes were applied:

- The pedestrian phases were changed to remove pedestrian recall on the east leg, so that pedestrians will need to press the pushbutton to call a walk signal. This will enable the northbound through phase interval to be reduced during the AM peak period and provide additional green time to the southbound left turn phase. While normally removing pedestrian recall would not be preferred, in this case the number of pedestrian crossings is very low ( 0 pedestrians observed in the east crosswalk during the AM peak hour; 1 pedestrian observed during the PM peak hour) and therefore the number of pedestrians affected would be minimal.
- A northbound left turn phase was added in the 2028 total future scenario during the AM and PM peak hours.
- Green times were adjusted on individual phases in conjunction with the other two changes noted above.

The future background and total future volumes at both horizon years were analyzed under these revised timings. Table $\mathbf{1 2}$ presents the results.

Given the magnitude of the constraints anticipated under the existing timings, the proposed adjustments would have a relatively modest effect, with the overall level of service generally remaining unchanged. The timing and phasing adjustments would result in increased capacity on the southbound left turn, particularly during the AM peak hour when the opposing northbound through volume is lower. Overall, however, there would still be numerous critical movements at the intersection under both background and total future conditions. Any more significant mitigation would require measures such as the Region's planned road widening west of the intersection.

Table 12: Mitigated Intersection Operations, Yonge Street and St. John's Sideroad

| Scenario: | Movement | AM peak hour |  |  |  | PM peak hour |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | v/c | LOS | Delay (s/veh) | $\begin{gathered} 95^{\text {th }} \% \text { ile } \\ \text { queue }(m) \end{gathered}$ | v/c | LOS | Delay (s/veh) | 95 ${ }^{\text {th }} \%$ ile queue ( $m$ ) |
| 2023 future background | EB left | 0.67 | D | 41.5 | 38 | 1.14 | F | 139 | 86 |
|  | EB through | 1.13 | F | 113 | 246 | 0.73 | D | 42.5 | 119 |
|  | WB left | 1.18 | F | 151 | 101 | 1.08 | F | 104 | 102 |
|  | WB through | 0.87 | E | 59.3 | 188 | 1.03 | F | 84.1 | 245 |
|  | WB right | 0.47 | A | 8.5 | 31 | 0.99 | E | 55.0 | 210 |
|  | NB left | 0.70 | E | 79.5 | 47 | 0.81 | E | 70.9 | 77 |
|  | NB through | 0.83 | E | 61.1 | 99 | 0.94 | E | 59.6 | 161 |
|  | NB right | 0.61 | C | 27.3 | 62 | 0.46 | B | 12.6 | 40 |
|  | SB left | 1.04 | F | 80.9 | 210 | 1.12 | F | 118.4 | 147 |
|  | SB through | 0.52 | B | 13.0 | 40 | 0.43 | C | 23.9 | 77 |
|  | SB right | 0.24 | A | 0.8 | 1 | 0.20 | A | 3.8 | 12 |
|  | Overall | - | E | 61.1 | - | - | E | 60.8 | - |
| 2023 total future | EB left | 0.92 | E | 71.7 | 51 | 1.15 | F | 141 | 96 |
|  | EB through | 1.17 | F | 124 | 270 | 0.78 | D | 43.1 | 137 |
|  | WB left | 1.25 | F | 179 | 102 | 1.01 | F | 83.3 | 101 |
|  | WB through | 0.89 | E | 59.3 | 200 | 1.09 | F | 100.1 | 269 |
|  | WB right | 0.47 | A | 9.0 | 33 | 0.99 | E | 54.8 | 212 |
|  | NB left | 0.91 | F | 112 | 65 | 0.96 | F | 98.7 | 93 |
|  | NB through | 0.82 | E | 60.7 | 97 | 0.97 | E | 65.4 | 165 |
|  | NB right | 0.62 | C | 30.0 | 65 | 0.46 | B | 12.0 | 38 |
|  | SB left | 1.07 | F | 90.4 | 210 | 1.18 | F | 141 | 151 |
|  | SB through | 0.53 | B | 16.0 | 50 | 0.45 | C | 25.4 | 79 |
|  | SB right | 0.25 | A | 1.0 | 1 | 0.23 | A | 3.9 | 13 |
|  | Overall | - | E | 68.8 | - | - | E | 65.9 | - |
| 2028 future background | EB left | 0.76 | D | 50.8 | 45 | 1.20 | F | 160 | 93 |
|  | EB through | 1.16 | F | 125 | 268 | 0.77 | D | 44.1 | 127 |
|  | WB left | 1.35 | F | 216 | 112 | 1.12 | F | 115 | 112 |
|  | WB through | 0.88 | E | 58.1 | 196 | 1.10 | F | 103 | 273 |
|  | WB right | 0.48 | A | 8.7 | 33 | 1.06 | E | 73.6 | 240 |
|  | NB left | 0.78 | F | 90.7 | 52 | 0.88 | F | 82.0 | 84 |
|  | NB through | 0.85 | E | 62.4 | 105 | 0.98 | E | 67.7 | 173 |
|  | NB right | 0.68 | D | 34.8 | 74 | 0.49 | B | 14.8 | 48 |
|  | SB left | 1.15 | F | 118 | 241 | 1.21 | F | 154 | 158 |
|  | SB through | 0.56 | B | 14.2 | 45 | 0.45 | C | 24.8 | 80 |
|  | SB right | 0.25 | A | 0.8 | 1 | 0.21 | A | 3.9 | 13 |
|  | Overall | - | E | 72.9 | - | - | E | 72.3 | - |
| 2028 total future | EB left | 1.10 | F | 118 | 72 | 1.24 | F | 171 | 105 |
|  | EB through | 1.23 | F | 146 | 315 | 0.86 | D | 48.6 | 154 |
|  | WB left | 1.22 | F | 168 | 99 | 1.10 | F | 113 | 117 |
|  | WB through | 0.98 | E | 72.8 | 248 | 1.15 | F | 121 | 297 |
|  | WB right | 0.47 | B | 11.1 | 42 | 1.12 | F | 98.7 | 265 |
|  | NB left | 0.70 | E | 46.1 | 40 | 0.69 | D | 36.9 | 48 |
|  | NB through | 0.83 | E | 61.2 | 99 | 1.01 | E | 74.7 | 176 |
|  | NB right | 0.62 | C | 29.0 | 64 | 0.47 | B | 11.1 | 37 |
|  | SB left | 1.33 | F | 199 | 267 | 1.28 | F | 181 | 162 |
|  | SB through | 0.75 | D | 49.0 | 124 | 0.63 | D | 38.4 | 99 |
|  | SB right | 0.36 | B | 13.9 | 26 | 0.30 | A | 5.8 | 16 |
|  | Overall | - | F | 95.3 | - | - | F | 82.5 | - |

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|  | Bathurst Street and St. John's Sideroad |
| :--- | :--- |
| 5.2 | Existing Configuration |

Table 13 summarizes the operations at Bathurst Street and St. John's Sideroad under each traffic volume scenario.

Table 13: Intersection Operations, Bathurst Street and St. John's Sideroad

| Scenario: | Movement | AM peak hour |  |  |  | PM peak hour |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | v/c | LOS | Delay <br> (s/veh) | $\begin{gathered} 95^{\text {th }} \% \text { ile } \\ \text { queue }(m) \end{gathered}$ | v/c | LOS | Delay <br> (s/veh) | $\begin{aligned} & 95^{\text {th }} \% \text { ile } \\ & \text { queue }(m) \end{aligned}$ |
| Existing | EB left | 0.29 | B | 19.0 | 22 | 0.74 | D | 35.5 | 61 |
|  | EB through | 0.62 | C | 26.9 | 114 | 0.65 | C | 30.4 | 128 |
|  | WB left | 0.54 | D | 40.8 | 50 | 0.61 | D | 49.9 | 47 |
|  | WB through | 0.84 | D | 49.3 | 157 | 0.86 | E | 57.0 | 136 |
|  | WB right | 0.08 | A | 0.3 | 0 | 0.31 | B | 11.0 | 22 |
|  | NB left | 0.44 | D | 41.4 | 22 | 0.32 | C | 30.5 | 28 |
|  | NB through | 0.55 | C | 29.7 | 75 | 0.81 | D | 36.9 | 146 |
|  | NB right | 0.09 | A | 0.3 | 0 | 0.25 | A | 8.6 | 22 |
|  | SB left | 0.44 | C | 20.6 | 31 | 0.43 | C | 22.6 | 18 |
|  | SB through | 0.72 | C | 26.4 | 126 | 0.45 | C | 21.3 | 72 |
|  | SB right | 0.33 | A | 4.7 | 19 | 0.10 | A | 3.9 | 8 |
|  | Overall | - | C | 27.9 | - | - | C | 32.0 | - |
| 2023 future background | EB left | 0.34 | C | 20.4 | 23 | 0.88 | D | 51.8 | 85 |
|  | EB through | 0.65 | C | 28.6 | 127 | 0.70 | C | 32.2 | 142 |
|  | WB left | 0.71 | D | 52.6 | 74 | 0.79 | E | 68.4 | 65 |
|  | WB through | 0.87 | D | 53.5 | 180 | 0.92 | E | 64.9 | 159 |
|  | WB right | 0.08 | A | 0.3 | 0 | 0.33 | B | 12.9 | 27 |
|  | NB left | 0.58 | E | 56.0 | 28 | 0.35 | C | 31.4 | 30 |
|  | NB through | 0.56 | C | 30.4 | 77 | 0.87 | D | 41.4 | 172 |
|  | NB right | $0.11$ | A | $0.4$ | $1$ | 0.29 | A | 9.7 | 27 |
|  | SB left | 0.50 | C | 22.5 | 33 | 0.49 | C | 25.3 | 19 |
|  |  |  | C |  | $141$ | $0.46$ | C | $21.9$ | $73$ |
|  | SB right | $0.35$ | A | $5.4$ | $23$ | $0.16$ | A | $3.6$ | 10 |
|  | Overall | - | C | 30.7 | - | - | D | 36.3 | - |
| 2023 total future | EB left | 0.37 | C | 23.2 | 22 | 0.93 | E | 64.0 | 89 |
|  | EB through | 0.67 | C | 29.4 | 133 | 0.75 | D | 35.1 | 154 |
|  | WB left | $0.84$ | E | $67.8$ | $90$ | 0.96 | F | 106 | 75 |
|  | WB through | 0.93 | E | 60.7 | 196 | 0.94 | E | 69.6 | 165 |
|  | WB right | 0.10 | A | 0.3 | 0 | 0.35 | B | 13.2 | 28 |
|  | NB left | $0.58$ | E | 56.6 | $28$ | 0.36 | C | 31.8 | 30 |
|  | NB through | 0.56 | C | 30.4 | 77 | 0.90 | D | 44.3 | 172 |
|  | NB right | 0.14 | A | 2.0 | 4 | 0.34 | A | 9.7 | 30 |
|  | SB left | $0.55$ | C | $24.0$ | $36$ | 0.58 | C | 30.8 | 25 |
|  | SB through | 0.79 | C | 29.4 | 141 | 0.45 | C | 21.8 | 73 |
|  | SB right | 0.35 | A | 5.4 | 23 | 0.15 | A | 3.6 | 10 |
|  | Overall | - | C | 32.8 | - | - | D | 40.2 | - |



Table 13: Intersection Operations, Bathurst Street and St. John's Sideroad (cont'd)

| Scenario: |  | AM peak hour |  |  |  |  |  | PM peak hour |  |  |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

The intersection of Bathurst Street and St. John's Sideroad currently operates at a reasonable overall level of service (LOS C) during both peak hours. No critical movements are identified during the AM peak hour. During the PM peak hour, the westbound through movement is just over the critical capacity threshold and with delays just over the critical level of service threshold.

At the 2023 horizon, the intersection is expected to continue operating at a reasonable overall level of service (LOS C to D). By 2028, the overall level of service is expected to remain at LOS D in most scenarios; however, the increase in school drop-off traffic is expected to result in a poor level of service (LOS E) during the AM peak hour. Several critical movements are identified from a capacity or level of service perspective, but the only movement anticipated to significantly exceed capacity is the westbound left turn under 2028 total future volumes. This movement does not have an advance left turn phase and is expected to attract a high volume of traffic leaving the school.

Similar to the intersection at Yonge Street, the Region's planned widening of St. John's Sideroad would be expected to increase capacity; however, recognizing the uncertainty as to timing, it was been assumed that mitigation will consist of adjustments to the traffic signals as a temporary measure until such time as the planned road widening can be completed.

Traffic signal timing and phasing adjustments were tested to mitigate the anticipated capacity constraints under the projected future background and total future volumes. The following changes were made:

- During the AM peak hour, the existing eastbound left turn phase was deactivated and replaced with an advance westbound left turn phase, reflecting the higher demand on the westbound left turn phase in the morning.
- During the PM peak hour, the existing eastbound left turn phase was retained. The new westbound left turn phase was assumed to be deactivated during the PM peak hour, except that it would be activated under 2028 total future conditions.
- Maximum green times on the north-south and/or east-west phases were increased (in 5-second increments) in some cases.

The future background and total future volumes at both horizon years were analyzed under these revised timings. Table 14 presents the results.

While several critical movements would remain, the proposed traffic signal timing and phasing changes would enable the majority of movements to operate at or below capacity. An exception is the eastbound left turn, which would exceed capacity by $10 \%$ to $12 \%$ during the PM peak hour under both background and total conditions in 2028.

It is noted that the southbound left turn advance phase is operating below capacity. This is an indication that there may be fewer than 3 vehicles queued at the start of green during some cycles. With setback detection in the left turn lanes, the left turn phase would be skipped if fewer than 3 vehicles are queued, which would reduce the length of those cycles and increase the capacity available to other movements at the intersection. Synchro does not account for the effect that setback stop bars have on the proportion of cycles where the left turn phase is skipped. Therefore, the $\mathrm{v} / \mathrm{c}$ ratios on the other movements may be lower than shown in Table 14 after accounting for shorter cycles when the southbound left turn phase is skipped.

Table 14: Mitigated Intersection Operations, Bathurst Street and St. John's Sideroad

| Scenario: | Movement | AM peak hour |  |  |  | PM peak hour |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | v/c | LOS | Delay (s/veh) | $\begin{aligned} & \text { 95th \%ile } \\ & \text { queue }(m) \end{aligned}$ | v/c | LOS | Delay <br> (s/veh) | $\begin{aligned} & \text { 95 th \%ile } \\ & \text { queue }(m) \end{aligned}$ |
| 2023 future background | EB left | 0.39 | C | 34.5 | 34 | 0.91 | E | 58.2 | 81 |
|  | EB through | 0.90 | E | 55.3 | 173 | 0.70 | C | 32.1 | 142 |
|  | WB left | 0.75 | D | 41.4 | 53 | 0.80 | E | 69.0 | 64 |
|  | WB through | 0.65 | C | 29.2 | 126 | 0.87 | E | 55.6 | 146 |
|  | WB right | 0.06 | A | 0.9 | 2 | 0.32 | B | 11.4 | 25 |
|  | NB left | 0.55 | D | 51.0 | 24 | 0.35 | C | 32.2 | 31 |
|  | NB through | 0.56 | C | 29.4 | 72 | 0.87 | D | 41.4 | 180 |
|  | NB right | 0.10 | A | 0.3 | 0 | 0.30 | B | 10.7 | 29 |
|  | SB left | 0.50 | C | 21.0 | 31 | 0.49 | C | 25.8 | 20 |
|  | SB through | 0.78 | C | 28.2 | 129 | 0.46 | C | 22.2 | 76 |
|  | SB right | 0.36 | A | 6.8 | 26 | 0.16 | A | 3.9 | 11 |
|  | Overall | - | C | 30.4 | - | - | D | 35.7 | - |
| 2023 total future | EB left | 0.43 | D | 36.3 | 35 | 0.95 | E | 67.5 | 84 |
|  | EB through | 0.92 | E | 57.7 | 181 | 0.74 | D | 34.6 | 153 |
|  | WB left | 0.88 | E | 60.5 | 69 | 0.95 | F | 102 | 73 |
|  | WB through | 0.68 | C | 30.4 | 137 | 0.88 | E | 56.8 | 152 |
|  | WB right | 0.08 | A | 1.9 | 4 | 0.33 | B | 11.7 | 26 |
|  | NB left | 0.56 | D | 52.3 | 24 | 0.36 | C | 33.0 | 31 |
|  | NB through | 0.56 | C | 29.6 | 72 | 0.90 | D | 45.2 | 180 |
|  | NB right | 0.13 | A | 1.6 | 4 | 0.34 | B | 10.9 | 32 |
|  | SB left | 0.55 | C | 22.6 | 33 | 0.58 | D | 31.6 | 28 |
|  | SB through | 0.79 | C | 28.5 | 129 | 0.45 | C | 22.5 | 76 |
|  | SB right | 0.37 | A | 7.7 | 30 | 0.16 | A | 3.8 | 11 |
|  | Overall | - | C | 32.2 | - | - | D | 39.2 | - |
| 2028 future background | EB left | 0.44 | D | 37.8 | 36 | 1.09 | F | 110 | 114 |
|  | EB through | 0.94 | E | 62.2 | 190 | 0.73 | D | 36.3 | 162 |
|  | WB left | 0.94 | E | 76.3 | 68 | 0.97 | F | 108 | 81 |
|  | WB through | 0.67 | C | 31.3 | 134 | 0.95 | E | 71.7 | 185 |
|  | WB right | 0.07 | A | 1.7 | 3 | 0.35 | B | 15.7 | 34 |
|  | NB left | 0.82 | F | 102 | 38 | 0.39 | C | 34.1 | 36 |
|  | NB through | 0.54 | C | 30.6 | 79 | 0.95 | D | 51.9 | 210 |
|  | NB right | 0.10 | A | 0.3 | 1 | 0.31 | B | 12.3 | 34 |
|  | SB left | 0.56 | C | 24.6 | 37 | 0.58 | C | 32.8 | 24 |
|  | SB through | 0.85 | C | 33.2 | 161 | 0.45 | C | 23.4 | 81 |
|  | SB right | 0.38 | A | 7.8 | 33 | 0.16 | A | 3.6 | 11 |
|  | Overall | - | D | 36.2 | - | - | D | 47.0 | - |
| 2028 total future | EB left | 0.46 | D | 42.2 | 40 | 1.12 | F | 123 | 118 |
|  | EB through | 1.01 | F | 80.9 | 235 | 1.00 | E | 79.3 | 229 |
|  | WB left | 1.00 | F | 92.3 | 100 | 0.97 | F | 89.6 | 71 |
|  | WB through | 0.68 | C | 32.3 | 158 | 0.97 | E | 75.3 | 195 |
|  | WB right | 0.10 | A | 5.0 | 9 | 0.37 | B | 16.3 | 36 |
|  | NB left | 0.97 | F | 152 | 44 | 0.39 | C | 34.3 | 36 |
|  | NB through | 0.53 | C | 34.8 | 88 | 0.95 | D | 53.0 | 210 |
|  | NB right | 0.19 | A | 5.5 | 13 | 0.35 | B | 12.4 | 38 |
|  | SB left | 0.73 | D | 39.0 | 52 | 0.67 | D | 40.4 | 35 |
|  | SB through | 0.87 | D | 40.0 | 184 | 0.46 | C | 23.6 | 81 |
|  | SB right | 0.39 | A | 9.6 | 38 | 0.17 | A | 3.6 | 11 |
|  | Overall | - | D | 44.4 | - | - | D | 54.0 | - |

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The intersection of St. John's Sideroad and Willow Farm Lane was initially analyzed under the existing two-way stop control. For the total future scenarios, dedicated lanes were assumed for the eastbound left turn, westbound right turn, and southbound left turn movements. Table 15 presents the results of the intersection analyses under two-way stop control.

Table 15: Intersection Operations, St. John's Sideroad and Willow Farm Lane

| Scenario: | Movement | AM peak hour |  |  |  | PM peak hour |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | v/c | LOS | Delay (s/veh) | $95^{\text {th }} \% \mathrm{ile}$ $\text { queue ( } m \text { ) }$ | v/c | LOS | Delay (s/veh) | 95 ${ }^{\text {th }} \%$ ile queue ( $m$ ) |
| Existing | NB approach | 0.19 | C | 17.3 | 6 | 0.18 | C | 19.1 | 5 |
| 2023 future background | NB approach | 0.23 | C | 20.4 | 7 | 0.22 | C | 22.8 | 7 |
| 2028 future background | NB approach | 0.26 | C | 22.7 | 8 | 0.25 | D | 25.5 | 8 |
| 2023 total future | NB approach SB left SB right | $\begin{gathered} 0.30 \\ >2.00 \\ 0.22 \end{gathered}$ | D | $\begin{gathered} 26.1 \\ >200 \\ 18.3 \end{gathered}$ | $\begin{gathered} 10 \\ {[\mathrm{~N} / \mathrm{A}]} \\ 6 \end{gathered}$ | $\begin{gathered} 0.42 \\ >2.00 \\ 0.11 \end{gathered}$ | $\begin{aligned} & \mathrm{E} \\ & \mathrm{~F} \\ & \mathrm{C} \end{aligned}$ | $\begin{gathered} 47.4 \\ >200 \\ 20.5 \end{gathered}$ | $\begin{gathered} 15 \\ {[\mathrm{~N} / \mathrm{A}]} \\ 3 \end{gathered}$ |
| 2028 total future | NB approach SB left SB right | $\begin{gathered} 0.86 \\ >2.00 \\ 0.72 \end{gathered}$ | $\begin{aligned} & F \\ & F \\ & F \end{aligned}$ | $\begin{gathered} 133 \\ >200 \\ 55.3 \end{gathered}$ | $\begin{gathered} 39 \\ {[\mathrm{~N} / \mathrm{A}]} \\ 38 \end{gathered}$ | $\begin{gathered} 0.56 \\ >2.00 \\ 0.28 \end{gathered}$ | $\begin{aligned} & \text { F } \\ & \text { F } \\ & \text { D } \end{aligned}$ | $\begin{gathered} 74.7 \\ >200 \\ 28.6 \end{gathered}$ | $\begin{gathered} 21 \\ {[\mathrm{~N} / \mathrm{A}]} \\ 9 \end{gathered}$ |

Under existing and future background volumes, the northbound approach operates at a reasonable level of service (LOS C to D) and within capacity.

With the introduction of site traffic, the northbound level of service will continue to be reasonable during the AM peak hour, but will decrease to LOS E to F during the PM peak hour.

Under two-way stop control, the southbound left turn from Street " $A$ " is anticipated to be significantly over capacity with few gaps available.
5.3.2 Potential Mitigation

Recognizing the poor level of service under total future volumes with the existing two-way stop control in place, the total future volumes were tested under traffic signal control. The traffic signals were assumed to be coordinated with the Yonge Street and St. John's Sideroad intersection. At the 2023 horizon the intersection was tested with a half cycle ( 60 seconds during the AM peak hour; 65 seconds during the PM peak hour); at the 2028 horizon the half cycle was maintained during the PM peak hour but the cycle length was increased to match the signals at Yonge Street (120 seconds) during the AM
peak hour. An eastbound advance left turn phase was included at the 2028 horizon. Vehicular and pedestrian clearance intervals were assumed.

The results of the signalized intersection operational analyses are presented in Table 16.

Table 16: Signalized Intersection Operations, St. John's Sideroad and Willow Farm Lane

| Scenario: | Movement | AM peak hour |  |  |  | PM peak hour |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | v/c | LOS | Delay (s/veh) | 95 ${ }^{\text {th }}$ \%ile queue ( $m$ ) | v/c | LOS | Delay (s/veh) | 95 ${ }^{\text {th }} \%$ ile <br> queue ( $m$ ) |
| 2023 total future | EB left | 0.14 | A | 6.7 | 8 | 0.31 | A | 9.3 | 15 |
|  | EB through | 0.71 | B | 13.5 | 176 | 0.55 | A | 7.5 | 93 |
|  | EB right | 0.00 | A | 0.0 | 0 | 0.01 | A | 0.0 | 0 |
|  | WB left | 0.09 | A | 1.8 | 1 | 0.16 | A | 2.1 | 2 |
|  | WB through | 0.56 | A | 5.8 | 166 | 0.67 | A | 9.3 | 179 |
|  | WB right | 0.07 | A | 0.2 | 1 | 0.09 | A | 0.2 | 0 |
|  | NB approach | 0.23 | A | 8.7 | 9 | 0.23 | A | 10.8 | 9 |
|  | SB left | $0.51$ | C | $31.7$ | 26 | 0.36 | C | 27.6 | 17 |
|  | SB through |  |  | 8.5 | 0 | 0.11 | B | 1.2 |  |
|  | Overall | - | B | 10.7 | - | - | A | 8.6 | - |
| 2028 total future | EB left | 0.44 | B | 9.1 | 20 | 0.58 | A | 30.8 | 31 |
|  | EB through | 0.75 | B | 16.3 | 211 | 0.65 | A | 11.7 | 126 |
|  | EB right | 0.00 | A | 0.0 | 0 | 0.01 | A | 0.0 | 0 |
|  | WB left | 0.10 | A | 5.2 | 2 | 0.23 | A | 5.5 | 5 |
|  | WB through | 0.64 | A | 6.4 | 49 | 0.82 | A | 16.0 | 199 |
|  | WB right | 0.21 | A | 0.3 | 0 | 0.10 | A | 1.2 | 1 |
|  | NB approach | 0.22 | B |  | 18 | 0.19 | B | 9.4 | 9 |
|  | SB left | 0.95 | F | 96.7 | 120 | 0.48 | E | 28.5 | 23 |
|  | SB through | 0.35 | B | 11.4 | 23 | 0.18 | B | 9.2 | 8 |
|  | Overall | - | B | 19.0 | - | - | B | 14.2 | - |

With the installation of traffic signals, the intersection is expected to operate at a reasonable overall level of service (LOS A to B). At the 2023 horizon, all movements are expected to operate at LOS C or better. At the 2028 horizon, the southbound left turn is expected to operate a poor level of service (LOS E to F); the change in level of service from 2023 reflects higher southbound traffic volumes, as well as the change in cycle length from a half cycle to a full cycle during the AM peak hour.

### 5.4 Additional Mitigation

The mitigation described in the preceding sections assumes limited roadway modifications. Further capacity can be expected following the completion of the planned St. John's Sideroad widening. Further opportunities for mitigation of operating conditions are identified below.
5.4.1 Extension of Collector Road Network

In the fullness of time, Street "A" is planned to extend northerly to an east-west collector road ("Bennington Road") extending from Bathurst Street to Yonge Street. The extended collector road
network will form part of future submissions for subsequent development phases. Once this additional connectivity is in place, there will be alternate routes available for site trips (particularly pick-up and drop-off trips) to enter and exit the site, decreasing pressure on St. John's Sideroad.

Additional Capacity for Strategic Movements
Certain movements are expected to experience particularly high volumes. One such pair of movements is the southbound left turn and westbound right turn pair at Yonge Street and St. John's Sideroad. The high volumes on these complementary movements reflects the discontinuity in the north-south arterial network through Newmarket and Aurora (i.e., Yonge Street becomes more constrained south of St. John's Sideroad; Bayview Avenue becomes more constrained north of Mulock Drive). While the Region currently prefers not to introduce new dual left turn lanes, in particular due to considerations related to urban design, pedestrian conditions and intersection footprint, this intersection may be a location where a dual left turn lane or alternative unconventional higher-capacity treatment may be desirable to accommodate a strategic movement pair and/or to encourage diversion of traffic away from more traffic-sensitive areas. It would be appropriate to consider alternative treatments as part of a future EA assessing alternatives for the St. John's Sideroad corridor. Such a venue would allow proper comparison of different considerations and priorities (e.g., traffic capacity; impact on other travel modes; urban design; environmental impact; property and cost implications, etc.).

Transportation Demand Management
Given that the majority of traffic in Phase 3 will be generated by the school, transportation demand management measures in the short term will be primarily associated with the school.

The school plans to operate a busing service, using one or two buses, and tentatively expects approximately 40 to 80 students to use this service. The traffic projections used in this report are based on approximately $15 \%$ of students riding to and from school on the bus.

Traffic projections are also affected by the proportion of families with more than one student attending the school (i.e., more than one student per drop-off). To some extent, this will also be applicable to families with a girl attending St. Anne's School and a boy attending St. Andrew's College, although the TDM effect would be primarily felt at a more regional level.

Traffic volumes may also be dependent on activities that require students to arrive early or leave late. The projections assume that afternoon pick-ups will be dispersed due to extra-curricular activities and varying work schedules, but that morning drop-offs will all occur within a peak hour.

To mitigate the effect of school traffic on the road network, the school should consider measures that would:

- Encourage and maximize the use of the school bus service;
- Incentivize attendance by more than one student per family; and
- Enable the morning drop-off peak to be further spread out (e.g., scheduling staggered entry for junior and senior students; offering extracurricular activities during the morning before school).

Given the distance of Phase 3 from existing transit service, the current lack of other amenities within walking distance, and the relative small size of the residential component compared to future phases, other TDM measures will be less applicable from the outset but should be considered as further development phases are carried forward:

- Introduction of a new VIVA stop at Bennington Road or St. John's Sideroad.
- Creation of a new transit route traveling through the site and offering connections to VIVA and other destinations within the surrounding area, provided that the level of service (particularly service frequency, but also the directness of the route and the span of service) is high enough to be attractive to potential riders).
- Creation of a YRT GO shuttle linking residents to the Aurora or future Mulock GO station.
- Provision of an extensive trail and pathway network within the site, generally as envisioned in the concept plan, with connections to other existing trails outside the site.
- Provision of pedestrian and cyclist crossing opportunities along collector roads at regular intervals and at strategic locations (e.g., at trail crossings).
- Consideration of means of providing complementary land uses within the site, particularly in proximity to the higher-density residential areas, to allow daily activities to be undertaken within walking distance and without requiring travel by vehicle on the surrounding road network.

| 6.0 | Site Access Considerations |
| :--- | :--- |
| 6.1 | Site Access to St. John's Sideroad |
|  | The following sections document design considerations related to the proposed site access to St. John's <br> Sideroad opposite Willow Farm Lane. |
| Traffic Signal Warrants |  |

As noted in Section 5.3.1, the Street "A" site access to St. John's Sideroad is expected to significantly exceed capacity during the AM and PM peak hours when pick-up and drop-off activity is occurring at the school. Because the need for traffic signals is heavily affected by school traffic, which is concentrated into short periods, an 8 -hour traffic signal warrant is not expected to be met. Ontario Traffic Manual (OTM) Book 12 identifies a four-hour warrant (Justification 4) for such locations where a side street does not have prolonged demand throughout the day but experiences significant surges over a shorter period of time. For urban conditions where a 2-lane major street carries more than 1,100 vehicles per hour, Justification 4 considers traffic signals to be warranted when the higher-volume minor approach exceeds 80 vehicles per hour. Given that the school traffic during the PM peak hour is expected to comprise approximately $25 \%$ of the total PM peak period traffic, it was assumed that the AM peak hour would be reflective of one of the four hours, and the PM peak hour would be reflective of the remaining four hours.

The projected volumes were compared against the Justification 4 minor approach threshold:

- In 2023, the southbound AM peak hour volume is expected to be 177 vehicles, including 107 left turns, which would exceed the Justification 4 threshold.
- In 2023, the southbound PM peak hour volume is expected to be 89 vehicles, including 63 left turns. The overall volume would exceed the Justification 4 threshold, while the left turns alone are approaching the threshold.
- Further growth in enrolment at the school would result in additional traffic that would be sufficient to meet the Justification 4 threshold during the PM peak hour.
6.1.2 Intersection Configuration

The intersection of St. John's Sideroad and Willow Farm Lane currently operates under two-way stop control. There is a short (approximately 15 metres) westbound left turn lane on St. John's Sideroad, in addition to an eastbound right turn taper.

It is anticipated that the construction of the new northerly leg for Street " $A$ " will occur prior to other widening on St. John's Sideroad, and will therefore require an interim configuration. It is recommended that the intersection be modified as follows:

- Widening of the east leg of the intersection to accommodate a westbound right turn lane.
- Widening of the west leg of the intersection to convert the existing runout lane to a left turn lane.
- Construction of a left turn lane and a shared through/right turn lane on the southbound approach.

Under traffic signal control, the analysis of 2028 total future operations during the AM peak hour identified a $95^{\text {th }}$ percentile queue length of 20 metres in the eastbound left turn lane, and 120 metres in the southbound left turn lane. Left and right turn lane dimensions should be as per Region of York standards.

## Longer-Term Considerations

In the longer term, three factors will affect traffic volumes and intersection design:

- The completion of the collector road network to the north will disperse traffic destined to and from the school rather than focusing it on a single access point.
- The reduction in school traffic will be offset by an increase in traffic destined to additional development in the Newmarket section of the development. The 2019 analyses for the overall development projected approximately 340 to 400 vehicles per hour in the peak direction on Street "A" north of St. John's Sideroad; this included traffic from the proposed Phase 3 residential units but did not include St. Anne's School.
- The St. John's Sideroad widening will provide additional east-west capacity and provide more flexibility in setting signal timings.

It is expected that the lane configuration for the widened intersection would be identified as part of the planning stage for the St. John's Sideroad widening.

## 6.2

## Access to St. Anne's School

Access to St. Anne's School is still under negotiation between the school and the applicant. In the long term, the primary vehicular access to the site is intended to be from Street " A " on the north side of the school parcel. However, in the interim Street "A" will terminate at the municipal boundary and alternate access arrangements will be required. Possible alternatives include a connection to Street " B " through Block 53; a connection to Street "B", Lane "A" or St. John's Sideroad that makes use of some or all of the existing driveway; or a temporary connection through part of Block 91 (the neighbourhood park).

Depending on which access scenario is selected, there will be revisions to the Plan of Subdivision to reflect impacts to residential lots. There may also be further changes in the future to the Plan of Subdivision once Street " $A$ " is extended farther to the north, enabling the school to be accessed directly from Street " $A$ ".

- If interim access is proposed through Block 53 , it is possible that this access may be maintained as a permanent access; if so, it is recommended that the internal vehicular circulation within the school site be configured so that pick-up and drop-off activity be required to enter and exit the site via Street " A " on the north side of the site, and that the access through Block 53 be maintained for visitors and ceremonial functions only.
- If interim access is proposed via other blocks, it is recommended that the access be removed once access is available directly from Street " $A$ ", enabling those blocks to be released.

The existing driveway leading to the future school building intersects with St. John's Sideroad approximately 140 metres west of Willow Farm Lane. In the event that interim school access is via the full length of the existing driveway, additional analysis will be required to identify geometric and traffic control requirements and impacts.

## 6.3 <br> Internal Roadway Configuration

The 2019 report recommended the application of alternative roadway cross-sections as a means of traffic calming. It was recommended that the roadway cross-section and surrounding urban form (e.g., distance between building faces; landscaping) be compact in nature so that the streets in the neighbourhood are designed to encourage low driving speeds and so that the major internal roadways are not perceived as being barriers.

The following policies and standards are proposed for application when preparing roadway designs within Phase 3:

- Collector roads will be designed with a pavement width of 7.0 metres, measured from curb to curb. This width accommodates one 3.5 -metre travel lane in each direction, which is adequate to accommodate projected traffic volumes and is wide enough to accommodate the vehicles expected to use these streets (including buses, emergency vehicles and single-unit trucks).
- Local streets will be designed with a pavement width of 6.0 metres, measured from curb to curb. This width accommodates one 3.0-metre travel lane in each direction, which is sufficient for low traffic volumes and is consistent with driveway widths specified in the Ontario Building Code for fire routes on private property.
- Where a parking lane is provided, the pavement width will be increased by 2.0 metres. Parking lanes will be defined by curb extensions such that they are only provided where a relatively continuous parking lane can be provided, and will be terminated with curb extensions where parking is not or cannot be provided (including at approaches to intersections), and where parking is not reasonably anticipated to be used.
- Additional pavement width will not be provided for bicycle lanes. Instead, bicycle facilities will be provided off-street within the right-of-way.
- Opportunities should be considered for cross-sections and building forms that reduce the right-ofway width and/or the optical width of the street by bringing building faces closer to the sidewalk and through placement of street trees. This would apply both to local streets and to collector roads.
- Traffic capacity will not be a governing consideration, other than to ensure that traffic entering from Regional roads does not affect operations of through traffic on those roads. To the extent that traffic volumes increase friction, they have a positive impact on reducing travel speeds.
- Additional pavement width will not be provided for auxiliary turn lanes or two-way left turn lanes (other than auxiliary lanes that may be provided at intersections with arterial roads).
- To reduce vehicle turning speeds and reduce pedestrian crossing distances, intersection corner radii will be the minimum that will accommodate the largest vehicle that would typically be expected within the subdivision (e.g., a single-unit truck).
- The corner radii will assume that these occasional large vehicles will be able to use as much of the roadway as necessary when completing a turn, subject to the likelihood that that part of the roadway would not normally be expected to be occupied by a vehicle for extended periods (e.g., parked cars; higher-volume stop or signal controlled intersection approaches).
- Sidewalks will be provided on both sides of all collector roads and both sides of all local streets. Sidewalks on local streets may be positioned directly adjacent to the curb (or formed with monolithic curb and gutter) to reduce the perceived width of the street.
- Bicycle paths will be provided adjacent to all collector roads in the form of separate dedicated or multi-use paths generally adjacent to the road and within the right-of-way. Bicycle travel elsewhere will be in mixed traffic on local streets, or on off-street trails and paths.
- Pedestrian crossings will be provided at regular intervals and strategic locations along collector roads (e.g., trail crossings). These may be in the form of all-way stop controlled intersections (if warranted), pedestrian crossovers, pedestrian refuge islands or reduced roadway width with curb extensions.

These principles are proposed to apply to the new local and collector roads in Phase 3, except as follows:

- Sidewalks are only proposed on one side of local streets; and
- Curb extensions are not proposed on Street "C", since this will be a short cul-de-sac where there will be less need for traffic calming features than on other streets.

The widths listed above would result in the following pavement widths on Streets "A" and "B":

- Street "A": 7.0 metres curb to curb, increasing to 9.0 metres where on-street parking bays are provided.
- Street "B": 6.0 metres curb to curb, increasing to 8.0 metres where on-street parking bays are provided.

As engineering plans progress, consideration may be given to a pedestrian crossing of Street " A " in the vicinity of the neighbourhood park north of Street "B" at a location to be determined.

These principles and standards are intended to be consistent with recent industry guidelines (e.g., "complete street" guidelines published by various municipalities; NACTO publications addressing urban streets and bikeways) that aim to rebalance the use of streets in urban areas. In addition to serving as a traffic management measure, narrower cross-sections will also reduce roadway footprint and would be more compatible with crossings of environmentally sensitive areas.

The north-south collector is planned to ultimately extend into Newmarket, which has a different standard collector road cross-section from the Town of Aurora. The same cross-section is proposed to be continuous across the municipal boundary and extend as far as the future east-west collector in Newmarket.


## 7.0 <br> Non-Auto Travel Modes

### 7.1 Multi-Modal Trip Generation

Table 4 in Section 2.7 documents the existing modal split for home-based trips made by Newmarket and
Aurora residents during the AM and PM peak periods, calculated using data from the 2016
Transportation Tomorrow Survey (TTS).

The estimated number of multi-modal trips generated by the residential component of site was calculated as follows:

- The number of vehicle trips generated by the site were converted to person trips by dividing by the auto driver modal split from the 2016 TTS.
- The person trips were then divided into the various other modes by applying the modal splits identified from the 2016 TTS.

The results are presented in Table 17.

Table 17: Non-Auto Site Trip Generation (Residential Component)

| Travel mode | AM peak hour |  |  |  |  | PM peak hour |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Modal split |  | Trips generated |  |  | Modal split |  | Trips generated |  |  |
|  | In | Out | In | Out | Total | In | Out | In | Out | Total |
| Auto driver | 85\% | 68\% | 36 | 102 | 138 | 76\% | 68\% | 109 | 66 | 175 |
| Person trips | 100\% | 100\% | 42 | 150 | 192 | 100\% | 100\% | 143 | 97 | 240 |
| Auto passenger | 7\% | 14\% | 3 | 21 | 24 | 13\% | 27\% | 19 | 26 | 45 |
| Local transit | 2\% | 5\% | 1 | 8 | 9 | 4\% | 0\% | 6 | 0 | 6 |
| School bus | 0\% | 4\% | 0 | 6 | 6 | 1\% | 0\% | 1 | 0 | 1 |
| Walk* | 5\% | 8\% | 2 | 12 | 14 | 5\% | 3\% | 7 | 3 | 10 |
| Bicycle / other* | 2\% | 1\% | 1 | 2 | 3 | 0\% | 1\% | 0 | 1 | 1 |

*Does not include walking or cycling trips to transit stops.

The results in Table 17 do not include GO rail trips, because the modal splits in the table reflect the mode used for trips to/from the GO station. As shown in Table 3 (see Section 2.7), the projected GO rail riders are equivalent $4 \%$ of outbound trips during the AM peak hour, and 5\% of inbound person trips during the PM peak hour. This represents the following number of riders:

- 6 outbound trips during the AM peak hour; and
- 7 inbound trips during the PM peak hour.

As calculated in Section 4.3.2, the following number of students are anticipated to travel by a non-single-passenger mode by 2028:

- Local carpoolers (i.e., resulting in a vehicle trip reduction entering and exiting the site due to siblings traveling together to St. Anne's School):
- AM peak hour: 109 students
- PM peak hour: 27 students
- Regional carpoolers (i.e., resulting in a vehicle trip reduction at a regional level due to siblings traveling together to St. Anne's School and St. Andrew's College:
- AM peak hour: 109 students
- PM peak hour: 27 students
- School bus riders:
- AM peak hour: 65 students ( 49 families)
- PM peak hour: 16 students (12 families)


### 7.2 Transit Considerations

### 7.2.1

## Transit Levels of Service

The transit level of service assessment considered three different factors that influence riders' perception of transit service:

- The walking distance from the subject site to the closest transit stop (how long will it take to get to the stop);
- The average headway between successive vehicles (how long will riders wait for the next vehicle); and
- Delays and $\mathrm{v} / \mathrm{c}$ ratios on intersection approaches used by transit vehicles (congestion and delays experienced by riders while on the bus).

The level of service criteria applied to the analyses have been taken from the Region's TMP guidelines, and are outlined in Table 18.

Table 18: Transit Level of Service Criteria

| Level of <br> Service | Access to transit stops | Transit <br> headway | Intersection <br> delay | Intersection <br> v/c |
| :---: | :---: | :---: | :---: | :---: |
| A | $90 \%$ within $\leq 200 \mathrm{~m}$ | $\leq 5$ minutes | $\leq 10 \mathrm{~s} / \mathrm{veh}$ | 0 to 0.60 |
| B | $90 \%$ within $\leq 500 \mathrm{~m}$ <br> and $70 \%$ within $\leq 200$ | $>5-10$ minutes | $>10-20 \mathrm{~s} / \mathrm{veh}$ | 0.61 to 0.70 |
| C | $90 \%$ within $\leq 500 \mathrm{~m}$ <br> and $50 \%$ within $\leq 200 \mathrm{~m}$ | $>10-15$ minutes | $>20-35 \mathrm{~s} / \mathrm{veh}$ | 0.71 to 0.80 |
| D | $100 \%$ within $\leq 600 \mathrm{~m}$ | $>15-20$ minutes | $>35-55 \mathrm{~s} / \mathrm{veh}$ | 0.81 to 0.90 |
| E | $100 \%$ within $\leq 800 \mathrm{~m}$ | $>20-30$ minutes | $>55-80 \mathrm{~s} / \mathrm{veh}$ | 0.91 to 1.00 |
| F | $100 \%>800 \mathrm{~m}$ | $>30$ minutes | $>80 \mathrm{~s} / \mathrm{veh}$ | $>1.00$ |

YRT has a target that $90 \%$ of residents in urban areas should reside within a 500-metre walk of a transit stop. (The target does not specify the level of service provided at that stop - frequency, span, etc. only the presence of some level of transit service.) This target was compared against the concept plan assuming the existing network is in place.

The closest transit stop is at Yonge Street and St. John's Sideroad, roughly 450 metres east of Street " A ". YRT local routes serve this stop. The majority of the proposed units are beyond 500 metres from this stop.

The majority of residential lots are within 800 metres of a transit stop, except for approximately 14 lots in the northwest part of Street "B". Given that there are units that are more than 800 metres from transit, the site is currently at LOS F from a transit access perspective.

The closest VIVA stop is at Joe Persechini Drive / Savage Road, approximately 900 metres north of St. John's Sideroad. There is no VIVA stop at St. John's Sideroad because the surrounding area is predominantly rural and low-density suburban with few transit trip generators within walking distance of that intersection, and because there are no intersecting transit routes that could generate transferring activity. There is a gap of nearly 2 kilometres between the stops at Savage Road in Newmarket and at Orchard Heights Boulevard in Aurora. Therefore, VIVA service will be outside walking distance from the proposed development.

### 7.2.1.2 Transit Headway

Table 19 lists the scheduled headway (interval between successive buses) for the routes closest to the site during the AM and PM peak periods, and during off-peak times, and the associated level of service for each route. The Yonge Street VIVA route is not included since there is not a stop in the vicinity of the site.

Two local routes operate along Yonge Street and therefore the average combined headway is lower than for each individual route. However, this does not affect the level of service because they operate at different headways and therefore the waiting time is governed by the route with the shortest headway rather than the average of the two.

Table 19: Existing Transit Level of Service (Scheduled Headway)

| Route | AM peak period |  | Weekday midday |  | PM peak period |  | Saturday |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Headway | LOS | Headway | LOS | Headway | LOS | Headway | LOS |
| 98 Yonge | 37 | F | 52 | F | 39 | F | $39-50$ | F |
| 96 Keele-Yonge | 32 | F | 32 | F | 25 | E | - | F |
| 31 Aurora North | 35 | F | - | F | 35 | F | - | F |

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Shining Hill Estates, Phase 3, Town of Aurora

With the exception of Route 96 (Keele-Yonge) during the PM peak period, all local routes operate at headways wider than 30 minutes, corresponding to LOS F conditions.

### 7.2.1.3

Intersection Approach
Table 20 lists the average delay and $\mathrm{v} / \mathrm{c}$ ratios for intersection approaches and turning movements where buses operate in mixed traffic, and the corresponding level of service. The delays and $\mathrm{v} / \mathrm{c}$ ratios were obtained from the Synchro analyses.

Table 20: Transit Level of Service (Intersection Approaches), Yonge Street at St. John's Sideroad

| Movement | Scenario | AM peak hour |  |  |  | PM peak hour |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Delay |  | v/c ratio |  | Delay |  | v/c ratio |  |
|  |  | s/veh | LOS | v/c | LOS | s/veh | LOS | v/c | LOS |
| NB through | Existing | 46.2 | D | 0.62 | B | 52.5 | D | 0.88 | D |
|  | 2023 future background | 61.1 | E | 0.83 | D | 59.6 | E | 0.94 | E |
|  | 2023 total future | 60.7 | E | 0.82 | D | 65.4 | E | 0.97 | E |
|  | 2028 future background | 62.4 | E | 0.85 | D | 67.7 | E | 0.98 | E |
|  | 2028 total future | 61.2 | E | 0.83 | D | 74.7 | E | 1.01 | F |
| SB through | Existing | 26.2 | C | 0.50 | A | 24.4 | C | 0.41 | A |
|  | 2023 future background | 13.0 | B | 0.52 | A | 23.9 | C | 0.43 | A |
|  | 2023 total future | 16.0 | B | 0.53 | A | 25.4 | C | 0.45 | A |
|  | 2028 future background | 14.2 | B | 0.56 | A | 24.8 | C | 0.45 | A |
|  | 2028 total future | 49.0 | D | 0.75 | C | 38.4 | D | 0.63 | B |

In terms of delay, the northbound approach is currently at LOS D during the AM and PM peak hours, and is expected to be at LOS E under all future horizons. The increase in delay reflects the recommended signal timing adjustments to mitigate conditions on the southbound left turn. The southbound approach is currently at LOS C; the level of service is expected to improve to LOS B during the AM peak hour and remain at LOS C during the PM peak hour under all scenarios except the 2028 total future scenario, when the level of service is expected to decrease to LOS D during the AM and PM peak hours.

In terms of $\mathrm{v} / \mathrm{c}$, during the AM peak hour the northbound approach is currently at LOS B and is expected to be at LOS D under the future scenarios, and during the PM peak hour it is currently at LOS B and is expected to be at LOS E to F under the future scenarios. The southbound approach is currently at LOS A and is expected to be at LOS A under most future scenarios, except the 2028 total future scenario, when it is expected to be at LOS B to C .
7.2.2 Potential Longer-Term Measures

### 7.2.2.1 Potential Longer-Term Service Expansion

Increasing the accessibility of more areas of the site to a variety of transit routes serving a variety of areas, and making those services more attractive, would help make transit more useful for more
residents within the site and for a wider range of trips, which would potentially impact the non-auto modal split within the site and reduce the number of single-occupant vehicle trips made by residents.

As the remainder of the Shining Hill Estates development is built out, the completed collector road network will provide an opportunity for a new or extended transit route to provide service through the community. The 2019 report identified a variety of potential routes within the subdivision. Service could be provided through the modification of Route 31 (Aurora North), or the creation of a new eastwest grid route generally along St. John's Sideroad extending easterly and southerly to the State Farm Way / First Commerce Drive area. Creation of a new route would also enable service to be provided to other areas in northeast Aurora that are outside YRT's area of coverage.

New VIVA Stop
With a substantial increase in development in the currently undeveloped area between Newmarket and Aurora, it would be appropriate to consider an additional VIVA stop in north Aurora / south Newmarket. St. John's Sideroad would be appropriate from the perspective of stop spacing to the north and south. However, Bennington Road might result in more accessible service in terms of number of residents within walking distance of the stop. Stop location could also be influenced by the ultimate route for local transit service (if any) within the overall development lands, so that transfer activity between the two routes can be accommodated. Given the distance between Phase 3 and Yonge Street, an additional VIVA stop would be of less benefit for Phase 3 but should be considered as future phases are developed.

### 7.3 Active Transportation

### 7.3.1

External Active Transportation Facilities
St. John's Sideroad currently has a rural cross-section with no pedestrian or cycling facilities. The bridge crossing Tannery Creek immediately west of Yonge Street has a sidewalk on the south side, but not on the north side. The planned widening of St. John's Sideroad would also include the urbanization of the cross-section and provision of active transportation facilities. The type, configuration and location of active transportation facilities would be determined as part of the development of alternative roadway cross-sections as part of a future environmental assessment.

## Internal Active Transportation Facilities

The surrounding neighbourhoods in Newmarket and Aurora both feature an extensive off-street trail network. A trail network is also proposed as part of the overall Shining Hill Estates development, with connections to existing trails to the north and east. The potential off-street trail network is shown in the overall concept plan (see Appendix A). In addition, alternative collector road cross-sections have been recommended (see Section 6.3) that include provision for off-street cycle paths within the right-of-way, which would offer more direct routes for utilitarian cycling.

On Street "A", a sidewalk will provided on one side and a multi-use trail will be provided on the other side. Local streets are currently proposed to have a sidewalk on one side.

Pedestrian Levels of Service
The level of service of the pedestrian environment has been determined for facilities along midblock road segments and for intersection crossings.

- For pedestrian facilities along road segments, the level of service relates to the type and width of facility and the separation distance from vehicle traffic. The Region's level of service criteria for midblock segments are listed in Table 21.
- For pedestrian crossings at intersections, the Region's level of service criteria primarily relate to the same criteria as midblock segments (i.e., type and width of facility; separation distance from vehicle traffic). These criteria are less applicable to pedestrian conditions at intersections, where the primary factors affecting the ease of crossing the intersection are delay time and exposure to traffic (crossing distance). Table 21 lists the level of service criteria that have been applied instead for pedestrian crossings at intersections, which are based on thresholds applied by the City of Ottawa in their Multi-Modal Level of Service Guidelines.

Table 21: Pedestrian Level of Service Criteria

| Level of <br> service | Segment | Intersection (Delay) | Intersection (Exposure) |
| :---: | :---: | :---: | :---: |
| A | $\geq 2.0$ m sidewalk with minimum 3.5 m buffer including <br> planting and edge zone; or $\geq 3.0 \mathrm{~m}$ multi-use path <br> $\geq 1.5 \mathrm{~m}$ sidewalk with minimum 1.0 m buffer including <br> edge zone; or $<3.0 \mathrm{~m}$ multi-use path | $<10 \mathrm{~s}$ per intersection leg | 3 lanes crossed or fewer |
| B | $\geq 1.5 \mathrm{~m}$ curb-faced sidewalk (no buffer) | $\geq 10$ to 20 s | 4 lanes crossed |
| C | $<1.5 \mathrm{~m}$ sidewalk | $>20$ to 30 s | 5 lanes crossed |
| D | Paved shoulder or no sidewalk provision | $>30$ to 40 s | 6 lanes crossed |
| E | No sidewalk provision | $>40$ to 60 s | 7 lanes crossed |
| F |  | $>60 \mathrm{~s}$ | 8 lanes crossed or more |

### 7.3.3.1 Segment Level of Service

Table 22 documents the existing pedestrian level of service along road segments. All levels of service reflect existing facilities, except Street " $A$ " reflects the proposed cross-section.

Table 22: Pedestrian Level of Service (Segments)

| Street | Segment | Level of service |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | West side | East <br> side | North side | South side |
| Bathurst Street | North of St. John's Sideroad | F | F | - | - |
| Bathurst Street | South of St. John's Sideroad | F | F | - | - |
| Street "A" | North of St. John's Sideroad | B | A | - | - |
| Willow Farm Lane | South of St. John's Sideroad | F | B | - | - |
| Yonge Street | North of St. John's Sideroad | E | E | - | - |
| Yonge Street | South of St. John's Sideroad | B | F | - | - |
| $18^{\text {th }}$ Sideroad | West of Bathurst Street | - | - | F | F |
| St. John's Sideroad | Bathurst Street to Yonge Street | - | - | F | F |
| St. John's Sideroad | East of Yonge Street | - | - | A | B |

Most regional roads in the vicinity do not have sidewalks and therefore offer LOS E to F conditions. Existing and planned local streets are at LOS B on at least one side of the street.

Intersection Delays
Table 23 documents the crossing delays and associated level of service at the intersection of Yonge Street and St. John's Sideroad under the various volume scenarios. Table 24 presents the same information at Bathurst Street and St. John's Sideroad. Crossing delays vary depending on the actuated green times for conflicting phases. In all cases the effective walk interval has been assumed to extend 4 seconds into the flashing don't walk interval, reflecting pedestrians that begin their crossing after the walk interval has ended (as observed to occur during traffic surveys at other intersections experiencing higher pedestrian volumes).

Table 23: Pedestrian Level of Service (Intersection Delay), Yonge Street at St. John's Sideroad

| Peak hour | Scenario | Average crossing delay (s/ped) |  |  |  | Level of service |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | West side | East <br> side | North side | South side | West side | East <br> side | North side | South side |
| AM | Existing | 32 | 53 | 50 | 52 | D | E | E | E |
|  | 2023 future background | 31 | 60 | 51 | 52 | D | E | E | E |
|  | 2023 total future | 32 | 60 | 49 | 50 | D | E | E | E |
|  | 2028 future background | 32 | 60 | 49 | 50 | D | E | E | E |
|  | 2028 total future | 44 | 60 | 47 | 46 | E | E | E | E |
| PM | Existing | 33 | 47 | 48 | 48 | D | E | E | E |
|  | 2023 future background | 32 | 47 | 47 | 50 | D | E | E | E |
|  | 2023 total future | 33 | 48 | 46 | 50 | D | E | E | E |
|  | 2028 future background | 33 | 47 | 46 | 50 | D | E | E | E |
|  | 2028 total future | 45 | 48 | 45 | 50 | E | E | E | E |

Table 24: Pedestrian Level of Service (Intersection Delay), Bathurst Street at St. John's Sideroad

| Peak hour | Scenario | Average crossing delay (s/ped) |  |  |  | Level of service |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | West side | East <br> side | North side | South side | West side | East <br> side | North side | South side |
| AM | Existing | 21 | 30 | 34 | n/a | C | C | D | - |
|  | 2023 future background | 27 | 36 | 31 | n/a | C | D | D | - |
|  | 2023 total future | 28 | 37 | 31 | n/a | C | D | D | - |
|  | 2028 future background | 28 | 37 | 32 | n/a | C | D | D | - |
|  | 2028 total future | 32 | 40 | 32 | n/a | D | E | D | - |
| PM | Existing | 28 | 34 | 46 | n/a | C | D | E | - |
|  | 2023 future background | 28 | 34 | 44 | n/a | C | D | E | - |
|  | 2023 total future | 28 | 36 | 45 | n/a | C | D | E | - |
|  | 2028 future background | 28 | 36 | 47 | n/a | C | D | E | - |
|  | 2028 total future | 29 | 37 | 47 | $\mathrm{n} / \mathrm{a}$ | C | D | E | - |

From the perspective of crossing delay, crossings at Yonge Street and St. John's Sideroad are at LOS E in all directions, except that the west crosswalk is at LOS D. Introducing a northbound left turn phase under 2028 total future conditions would change this crosswalk to LOS E as well.

At Bathurst Street and St. John's Sideroad, the west and east crosswalks are at LOS C to D during the AM and PM peak hours, and the north crosswalk is at LOS D during the AM peak hour and LOS E during the PM peak hour. Site traffic is not expected to affect the level of service, except that a minor increase in delay will cause the west and crosswalks to change from LOS C/D to LOS D/E during the AM peak hour in 2028.

Table 25 documents the crossing delays and associated level of service at the intersection of St. John's Sideroad and Willow Farm Lane / Street " $A$ " under the total future scenarios, assuming the installation of traffic signals and assuming the signal timings applied in the intersection analyses. Delays are expected to correspond to LOS A to B crossing the north and south legs; LOS D crossing the east and west legs in 2023; LOS C crossing St. John’s Sideroad during the 2028 AM peak hour; and LOS E crossing St. John’s Sideroad during the 2028 PM peak hour (the poorer level of service corresponding to doubling the cycle length to match the adjacent signals at Yonge Street).

Table 25: Pedestrian Level of Service (Intersection Delay), St. John's Sideroad at Willow Farm Lane / Street " $A$ "

| Peak hour | Scenario | Average crossing delay (s/ped) |  |  |  | Level of service |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | West side | East <br> side | North side | South side | West side | East <br> side | North side | South side |
| AM | 2023 total future | 32 | 32 | 4 | 4 | D | D | A | A |
|  | 2028 total future | 50 | 50 | 11 | 7 | E | E | B | A |
| PM | 2023 total future | 31 | 32 | 3 | 3 | D | D | A | A |
|  | 2028 total future | 30 | 30 | 5 | 5 | C | C | A | A |

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Table 26 presents the number of lanes crossed by pedestrians at each intersection and the corresponding level of service. The St. John's Sideroad intersections at Bathurst Street and Yonge Street reflect existing conditions; the intersection at Willow Farm Lane reflects total future conditions.

Table 26: Pedestrian Level of Service (Intersection Exposure)

| St. John's Sideroad at: | Number of lanes crossed |  |  |  | Level of service |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | West <br> side | East <br> side | North <br> side | South <br> side | West <br> side | East <br> side | North <br> side | South <br> side |
| Bathurst Street | 3 | 4 | 6 | - | A | B | D | - |
| Willow Farm Lane / Street "A" | 4 | 4 | 3 | 2 | B | B | A | A |
| Yonge Street | 5 | 5 | 6 | 6 | C | C | D | D |

The level of service crossing Bathurst Street and Yonge Street is LOS D; the level of service crossing St. John's Sideroad at Yonge Street is LOS C; and all other existing or planned crossings are LOS A to B.

Cycling Levels of Traffic Stress
Although the Region's TMP guidelines have level of service criteria for bicycle facilities, the assessment in this report has been based instead on Level of Traffic Stress (LTS) criteria developed in 2012 by Maaza Mekuria, Peter Furth and Hilary Nixon in a research report published by the Mineta Transportation Institute. ${ }^{3}$ Whereas the Region's LOS criteria assign a level of service based on the presence (or lack) of a dedicated bicycle facility, its physical relation to traffic lanes, and its width, the LTS criteria instead categorize the cycling network according to the type of cyclist that would feel comfortable riding on each section, based on factors such as traffic volume and speed in addition to the type and design of cycling facility. Furth describes the LTS categories as follows: ${ }^{4}$

- LTS 1: Strong separation from all except low speed, low volume traffic. Simple crossings. Suitable for children.
- LTS 2: Except in low speed / low volume traffic situations, cyclists have their own place to ride that keeps them from having to interact with traffic except at formal crossings. Physical separation from higher speed and multilane traffic. Crossings that are easy for an adult to negotiate. Corresponds to design criteria for Dutch bicycle route facilities. A level of traffic stress that most adults can tolerate, particularly those sometimes classified as "interested but concerned."
- LTS 3: Involves interaction with moderate speed or multilane traffic, or close proximity to higher speed traffic. A level of traffic stress acceptable to those classified as "enthused and confident."
- LTS 4: Involves interaction with higher speed traffic or close proximity to high speed traffic. A level of stress acceptable only to those classified as "strong and fearless."

[^2]On-road facilities are categorized based on factors such as the number of travel lanes on the adjacent road, the speed and volume of traffic, the presence and width of bicycle lanes, and the degree of separation from traffic. Appendix $\boldsymbol{D}$ presents the LTS criteria for on-road facilities (adapted to use metric units). ${ }^{5}$ Table 27 lists the ratings of existing LTS for each roadway segment in the study area and the underlying factors influencing those LTS ratings.

Table 27: Existing Level of Traffic Stress for Cyclists

| Street / section | Cycling context | Number of lanes | Approx. AADT | Approx. travel speed | LTS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Bathurst Street north of St. John's Sideroad | Mixed traffic | 2 thru lanes per direction | 22,600 veh/day | $72 \mathrm{~km} / \mathrm{h}$ | LTS 4 |
| Bathurst Street south of St. John's Sideroad | Mixed traffic | 2 thru lanes per direction | 20,850 veh/day | $72 \mathrm{~km} / \mathrm{h}$ | LTS 4 |
| Willow Farm Lane south of St. John's Sideroad | Mixed traffic | Unlaned 2-way street (no centreline) | 1,150 veh/day | $48 \mathrm{~km} / \mathrm{h}$ | LTS 2 |
| Yonge Street north of St. John's Sideroad | Paved shoulders (buffered NB) | 2 thru lanes per direction | 26,400 veh/day | 64 km/h | LTS 3 |
| Yonge Street south of St. John's Sideroad | Mixed traffic | 2 thru lanes per direction | 21,400 veh/day | 64 km/h | LTS 4 |
| $18^{\text {th }}$ Sideroad west of Bathurst Street | Mixed traffic | 1 thru lane per direction | 13,000 veh/day | 64 km/h | LTS 4 |
| St. John's Sideroad west of Willow Farm Lane | Mixed traffic | 1 thru lane per direction | 14,000 veh/day | 64 km/h | LTS 4 |
| St. John's Sideroad east of Willow Farm Lane | Mixed traffic | 1 thru lane per direction | 14,950 veh/day | $64 \mathrm{~km} / \mathrm{h}$ | LTS 4 |
| St. John's Sideroad east of Yonge Street | Multi-use trail (north side) | 2 thru lanes per direction | 24,650 veh/day | $56 \mathrm{~km} / \mathrm{h}$ | LTS 1 |

Under current conditions:

- Cyclists comfortable using LTS 1 or 2 facilities would be able to cycle on Willow Farm Lane, and on St. John's Sideroad east of Yonge Street.
- Cyclists comfortable using up to LTS 3 facilities would also be able to cycle on Yonge Street north of St. John's Sideroad.
- Only cyclists comfortable using LTS 4 facilities would be willing to cycle on any other road segments in the study area.

These levels of traffic stress are not expected to change due to future volume increases.

Street " $A$ " is proposed to have an off-street multi-use trail on one side and will serve a wide range of cyclists.

[^3]
## 8.0 Summary

This Transportation Mobility Plan has been prepared as part of the application for Phase 3 of the Shining Hill Estates development within the town of Aurora. The site is located north of St. John's Sideroad opposite Willow Farm Lane, west of Yonge Street. Phase 3 is proposed to include 88 detached residential units and a medium-density block estimated to accommodate approximately 200 residential units. It would also include the opening of St. Anne's School, an all-girls private school, within an existing building on the site; enrolment is expected to start at approximately 100 students in the first year of operations, and increase to approximately 435 students by the fifth year.

Phase 3 forms the southerly part of a concept plan developed by Malone Given Parsons Inc. (MGP) that envisions approximately 3,500 residential units, in addition to a school, a small service commercial block, and an extensive natural heritage / open space network with an associated trail system. Two collector roads would provide access from the surrounding arterial roads: an east-west collector (Bennington Road) extending between Bathurst Street and Yonge Street, and a north-south collector extending between Bennington Road and St. John's Sideroad. A prior TMP report was prepared by Dillon in 2019 examining the overall development at a high level.

Access to Phase 3 from the regional road network would be via the north-south collector (Street " $A$ ") planned for the overall development; it would extend northerly from the St. John's Sideroad and Willow Farm Lane intersection as far as the Newmarket/Aurora boundary, where it would temporarily terminate pending the further expansion of development on the Newmarket side of the boundary. Street " $A$ " would be extended farther to the north as part of subsequent development phases.

Access to the school from Street " $A$ " is still under negotiation. The school site will not have direct frontage to Street " $A$ " until the street is extended northerly into Newmarket, and other access arrangements will be required in the interim. One potential scenario involves access to Street "B" through Block 53, which may be maintained as a permanent access; if so, it is recommended that the internal vehicular circulation within the school site be configured so that pick-up and drop-off activity be required to enter and exit the site via Street " $A$ " on the north side of the site, and that the access through Block 53 be maintained for visitors and ceremonial functions only.

Trips were generated at a 2023 horizon (build-out year) and a 2028 horizon (five years following buildout).

- In 2023, the site is expected to generate approximately 303 vehicle trips during the AM peak hour and 217 vehicle trips during the PM peak hour.
- By 2028, with increased enrolment at the school, the trip generation is expected to increase to approximately 757 vehicle trips during the AM peak hour and 331 vehicle trips during the PM peak hour.

Because of the relationship between existing St. Andrew's College and the new St. Anne's School, it is anticipated that some parents of girls attending the new school will already have sons attending St. Andrew's College and will drop both children off at the same time. Because the pick-up and drop-off trips to St. Andrew's College would already be traveling on the broader study area road network, they will offset some of the trips generated by the school. After accounting for this trip chaining, the site will generate a lower net number of new trips:

- In 2023, the site is expected to generate approximately 253 net new vehicle trips during the AM peak hour and 205 net new vehicle trips during the PM peak hour.
- By 2028, with increased enrolment at the school, the trip generation is expected to increase to approximately 573 net new vehicle trips during the AM peak hour and 285 net new vehicle trips during the PM peak hour.

Traffic conditions at study area intersections are affected by St. John's Sideroad, a two-lane road with a rural cross-section. East of Yonge Street it widens to a four-lane urban cross-section. The Region's Transportation Master Plan recommended that St. John's Sideroad be widened to four lanes between Bathurst Street and Yonge Street sometime between 2027 and 2031, but the widening is not currently scheduled in the Region's 10-year capital plan and an EA has not been undertaken. The existing roadway is near capacity and is expected to reach capacity on many intersection movements under future background conditions; projected site traffic is expected to further affect intersection operations. Some interim mitigation has been identified in the form of adjustments to traffic signal timings and phasing at the signalized intersections at Bathurst Street and at Yonge Street; in particular, a westbound left turn phase is recommended at Bathurst Street and St. John's Sideroad.

The Street " $A$ " access to St. John's Sideroad is expected to require traffic signals to accommodate pick-up and drop-off traffic at the school. Traffic signals are expected to be justified (or nearly justified) based on the 4-hour warrant (Justification 4) in OTM Book 12. At the intersection with St. John's Sideroad, an eastbound left turn lane, a westbound right turn lane, and a southbound right turn lane are recommended.

Given the existing largely rural nature of the area, there is no active transportation infrastructure on St. John's Sideroad, and transit service is outside walking distance of most residents. The widening of St. John's Sideroad would be expected to include conversion to an urban cross-section with sidewalks (or multi-use trails to accommodate cycling). Also in the longer term, the continued expansion of the development area to the north would include a continuous collector road network that would enable the expansion of local transit service into the area.

The eventual northerly extension of Street " $A$ ", and internal connections west to Bathurst Street and east to Yonge Street, will disperse school traffic and reduce pressure on St. John's Sideroad, although some of this effect will be offset by additional traffic generated by future development in the area to the north.

Transporation demand management measures were considered to reduce the traffic impact of the proposed development. Given that the majority of traffic in Phase 3 will be generated by the school, TDM measures in the short term will be primarily associated with the school. To mitigate the effect of school traffic on the road network, the school should consider measures that would:

- Encourage and maximize the use of its planned school bus service (to reduce the number of students being dropped off by private vehicle);
- Incentivize attendance by more than one student per family (to increase the average vehicle occupancy for pick-up and drop-off trips); and
- Enable the morning drop-off peak to be further spread out (e.g., scheduling staggered entry for junior and senior students; offering extracurricular activities during the morning before school).




## Appendix A

Proposed Draft Plan of Subdivision and Overall Concept Plan


Shining Hill Estate Collection, Inc.
Shining Hill Estates, Phase 3, Town of Aurora
Transportation Mobility Plan
March 2021 - 21-1332




## Appendix B

## Traffic Survey Data



Shining Hill Estate Collection, Inc.
Shining Hill Estates, Phase 3, Town of Aurora
Transportation Mobility Plan
March 2021 - 21-1332

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|  | Bathurst St From North |  |  |  |  | St John`s SdRd From East} & \multicolumn{5}{\|l|}{Bathurst St From South} & \multicolumn{5}{|l|}{St John`s SdRd From West |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 Peak Hour for Entire Intersection Begins at 08:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 08:00 AM | 59 | 194 | 30 | 0 | 283 | 15 | 102 | 28 | 0 | 145 | 28 | 118 | 12 | 0 | 158 | 15 | 94 | 9 | 0 | 118 | 704 |
| 08:15 AM | 49 | 205 | 52 | 0 | 306 | 15 | 108 | 23 | 0 | 146 | 29 | 125 | 10 | 0 | 164 | 10 | 95 | 12 | 0 | 117 | 733 |
| 08:30 AM | 51 | 166 | 33 | 0 | 250 | 18 | 75 | 25 | 0 | 118 | 36 | 157 | 7 | 0 | 200 | 22 | 90 | 19 | 0 | 131 | 699 |
| 08:45 AM | 36 | 215 | 45 | 0 | 296 | 18 | 87 | 26 | 0 | 131 | 45 | 144 | 11 | 0 | 200 | 14 | 102 | 19 | 0 | 135 | 762 |
| Total Volume | 195 | 780 | 160 | 0 | 1135 | 66 | 372 | 102 | 0 | 540 | 138 | 544 | 40 | 0 | 722 | 61 | 381 | 59 | 0 | 501 | 2898 |
| \% App. Total | 17.2 | 68.7 | 14.1 | 0 |  | 12.2 | 68.9 | 18.9 | 0 |  | 19.1 | 75.3 | 5.5 | 0 |  | 12.2 | 76 | 11.8 | 0 |  |  |
| PHF | . 826 | . 907 | . 769 | . 000 | . 927 | . 917 | . 861 | . 911 | . 000 | . 925 | . 767 | . 866 | . 833 | . 000 | . 903 | . 693 | . 934 | . 776 | . 000 | . 928 | . 951 |
| Cars | 194 | 757 | 159 | 0 | 1110 | 65 | 358 | 101 | 0 | 524 | 133 | 519 | 39 | 0 | 691 | 60 | 365 | 56 | 0 | 481 | 2806 |
| \% Cars | 99.5 | 97.1 | 99.4 | 0 | 97.8 | 98.5 | 96.2 | 99.0 | 0 | 97.0 | 96.4 | 95.4 | 97.5 | 0 | 95.7 | 98.4 | 95.8 | 94.9 | 0 | 96.0 | 96.8 |
| Trucks | 1 | 7 | 0 | 0 | 8 | 0 | 6 | 1 | 0 | 7 | 4 | 1 | 1 | 0 | 6 | 0 | 11 | 1 | 0 | 12 | 33 |
| \% Trucks | 0.5 | 0.9 | 0 | 0 | 0.7 | 0 | 1.6 | 1.0 | 0 | 1.3 | 2.9 | 0.2 | 2.5 | 0 | 0.8 | 0 | 2.9 | 1.7 | 0 | 2.4 | 1.1 |
| Heavys | 0 | 16 | 1 | 0 | 17 | 1 | 8 | 0 | 0 | 9 | 1 | 23 | 0 | 0 | 24 | 1 | 5 | 2 | 0 | 8 | 58 |
| \% Heavys | 0 | 2.1 | 0.6 | 0 | 1.5 | 1.5 | 2.2 | 0 | 0 | 1.7 | 0.7 | 4.2 | 0 | 0 | 3.3 | 1.6 | 1.3 | 3.4 | 0 | 1.6 | 2.0 |
| Cyclists | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| \% Cyclists | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.2 | 0 | 0 | 0.1 | 0 | 0 | 0 | 0 | 0 | 0.0 |



Horizon Data Services Ltd

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\hline \multicolumn{22}{|l|}{| File Name : Bathurst St at St John`s Sideroad |
| :--- |
| Site Code : 00000000 |
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| Page No : 6 |} <br>

\hline \& \multicolumn{5}{|l|}{Bathurst St From North} \& \multicolumn{5}{|l|}{St John`s SdRd From East} & \multicolumn{5}{|l|}{Bathurst St From South} & \multicolumn{5}{|l|}{St John`s SdRd From West} \& <br>
\hline Start Time \& Right \& Thru \& Left \& Peds \& App. Total \& Right \& Thru \& Left \& Peds \& App. Total \& Right \& Thru \& Left \& Peds \& App. Total \& Right \& Thru \& Left \& Peds \& App. Total \& Int. Total <br>
\hline \multicolumn{22}{|l|}{\multirow[t]{2}{*}{Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 Peak Hour for Entire Intersection Begins at 04:45 PM}} <br>
\hline \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& \& <br>
\hline 04:45 PM \& 25 \& 193 \& 33 \& 0 \& 251 \& 53 \& 102 \& 32 \& 0 \& 187 \& 41 \& 255 \& 10 \& 0 \& 306 \& 12 \& 138 \& 57 \& 0 \& 207 \& 951 <br>
\hline 05:00 PM \& 22 \& 176 \& 28 \& 0 \& 226 \& 51 \& 107 \& 20 \& 0 \& 178 \& 39 \& 274 \& 20 \& 0 \& 333 \& 15 \& 123 \& 50 \& 0 \& 188 \& 925 <br>
\hline 05:15 PM \& 27 \& 195 \& 35 \& 0 \& 257 \& 64 \& 99 \& 30 \& 0 \& 193 \& 30 \& 288 \& 26 \& 0 \& 344 \& 7 \& 108 \& 51 \& 0 \& 166 \& 960 <br>
\hline 05:30 PM \& 27 \& 131 \& 25 \& 0 \& 183 \& 38 \& 106 \& 25 \& 0 \& 169 \& 50 \& 241 \& 19 \& 0 \& 310 \& 9 \& 140 \& 56 \& 0 \& 205 \& 867 <br>
\hline Total Volume \& 101 \& 695 \& 121 \& 0 \& 917 \& 206 \& 414 \& 107 \& 0 \& 727 \& 160 \& 1058 \& 75 \& 0 \& 1293 \& 43 \& 509 \& 214 \& 0 \& 766 \& 3703 <br>
\hline \% App. Total \& 11 \& 75.8 \& 13.2 \& 0 \& \& 28.3 \& 56.9 \& 14.7 \& 0 \& \& 12.4 \& 81.8 \& 5.8 \& 0 \& \& 5.6 \& 66.4 \& 27.9 \& 0 \& \& <br>
\hline PHF \& . 935 \& . 891 \& . 864 \& . 000 \& . 892 \& . 805 \& . 967 \& . 836 \& . 000 \& . 942 \& . 800 \& . 918 \& . 721 \& . 000 \& . 940 \& . 717 \& . 909 \& . 939 \& . 000 \& . 925 \& . 964 <br>
\hline Cars \& 100 \& 682 \& 118 \& 0 \& 900 \& 206 \& 404 \& 104 \& 0 \& 714 \& 158 \& 1043 \& 74 \& 0 \& 1275 \& 42 \& 504 \& 213 \& 0 \& 759 \& 3648 <br>
\hline \% Cars \& 99.0 \& 98.1 \& 97.5 \& 0 \& 98.1 \& 100 \& 97.6 \& 97.2 \& 0 \& 98.2 \& 98.8 \& 98.6 \& 98.7 \& 0 \& 98.6 \& 97.7 \& 99.0 \& 99.5 \& 0 \& 99.1 \& 98.5 <br>
\hline Trucks \& 1 \& 4 \& 2 \& \& 7 \& \& 6 \& 2 \& 0 \& 8 \& 0 \& 6 \& 1 \& 0 \& 7 \& 1 \& 2 \& 0 \& 0 \& 3 \& 25 <br>
\hline \% Trucks \& 1.0 \& 0.6 \& 1.7 \& 0 \& 0.8 \& - \& 1.4 \& 1.9 \& 0 \& 1.1 \& 0 \& 0.6 \& 1.3 \& 0 \& 0.5 \& 2.3 \& 0.4 \& 0 \& 0 \& 0.4 \& 0.7 <br>
\hline Heavys \& 0 \& 8 \& , \& - \& 9 \& 0 \& 4 \& 1 \& 0 \& 5 \& 2 \& 9 \& 0 \& 0 \& 11 \& 0 \& 3 \& 1 \& 0 \& 4 \& 29 <br>
\hline \% Heavys \& 0 \& 1.2 \& 0.8 \& 0 \& 1.0 \& \& 1.0 \& 0.9 \& 0 \& 0.7 \& 1.3 \& 0.9 \& 0 \& 0 \& 0.9 \& 0 \& 0.6 \& 0.5 \& 0 \& 0.5 \& 0.8 <br>
\hline Cyclists \& - \& \& - \& - \& \& 0 \& 0 \& 0 \& 0 \& 0 \& 0 \& 0 \& 0 \& 0 \& 0 \& 0 \& 0 \& 0 \& 0 \& 0 \& <br>
\hline \% Cyclists \& - \& 0.1 \& 0 \& - \& 0.1 \& 0 \& 0 \& - \& 0 \& \& - \& 0 \& 0 \& 0 \& 0 \& 0 \& 0 \& - \& 0 \& 0 \& 0.0 <br>
\hline
\end{tabular}



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Horizon Data Services Ltd






Horizon Data Services Ltd

## 318 Simonst L3T 4T5 <br> ＂we always count．．．never estimated＂

File Name ：Yonge St at St John｀s Sideroad
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Horizon Data Services Ltd

## 318 Simonston Blvd Thornhill, ON L3T 4T5 <br> "we always count...never estimated"

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|  | Yonge St From North |  |  |  |  | St John`s SdRd From East} & \multicolumn{5}{\|l|}{Yonge St From South} & \multicolumn{5}{|l|}{St John`s SdRd From West |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 Peak Hour for Entire Intersection Begins at 08:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 08:00 AM | 19 | 93 | 101 | 0 | 213 | 44 | 115 | 44 | 0 | 203 | 43 | 56 | 14 | 0 | 113 | 16 | 135 | 20 | 3 | 174 | 703 |
| 08:15 AM | 23 | 106 | 113 | 0 | 242 | 49 | 103 | 48 | 0 | 200 | 45 | 58 | 8 | 0 | 111 | 12 | 143 | 8 |  | 164 | 717 |
| 08:30 AM | 24 | 100 | 83 | 0 | 207 | 53 | 87 | 51 | 0 | 191 | 55 | 89 | 20 | 0 | 164 | 44 | 133 | 13 | 0 | 190 | 752 |
| 08:45 AM | 22 | 107 | 107 | 0 | 236 | 71 | 99 | 61 | 0 | 231 | 77 | 78 | 13 | 2 | 170 | 46 | 150 | 16 | 0 | 212 | 849 |
| Total Volume | 88 | 406 | 404 | 0 | 898 | 217 | 404 | 204 | 0 | 825 | 220 | 281 | 55 | 2 | 558 | 118 | 561 | 57 | 4 | 740 | 3021 |
| \% App. Total | 9.8 | 45.2 | 45 | 0 |  | 26.3 | 49 | 24.7 | 0 |  | 39.4 | 50.4 | 9.9 | 0.4 |  | 15.9 | 75.8 | 7.7 | 0.5 |  |  |
| PHF | . 917 | . 949 | . 894 | . 000 | . 928 | . 764 | . 878 | . 836 | . 000 | . 893 | . 714 | . 789 | . 688 | . 250 | . 821 | . 641 | . 935 | . 713 | . 333 | . 873 | . 890 |
| Cars | 85 | 380 | 390 | 0 | 855 | 200 | 393 | 202 | 0 | 795 | 217 | 265 | 54 | 2 | 538 | 116 | 548 | 53 | 4 | 721 | 2909 |
| \% Cars | 96.6 | 93.6 | 96.5 | 0 | 95.2 | 92.2 | 97.3 | 99.0 | 0 | 96.4 | 98.6 | 94.3 | 98.2 | 100 | 96.4 | 98.3 | 97.7 | 93.0 | 100 | 97.4 | 96.3 |
| Trucks | 2 | 6 | 4 | 0 | 12 | 3 | 6 | 1 | 0 | 10 | 2 | 5 | 0 | 0 | 7 | 2 | 7 | 4 | 0 | 13 | 42 |
| \% Trucks | 2.3 | 1.5 | 1.0 | 0 | 1.3 | 1.4 | 1.5 | 0.5 | 0 | 1.2 | 0.9 | 1.8 | 0 | 0 | 1.3 | 1.7 | 1.2 | 7.0 | 0 | 1.8 | 1.4 |
| Heavys | 1 | 20 | 10 | 0 | 31 | 14 | 5 | 1 | 0 | 20 | 1 | 11 | 1 | 0 | 13 | 0 | 6 | 0 | 0 | 6 | 70 |
| \% Heavys | 1.1 | 4.9 | 2.5 | 0 | 3.5 | 6.5 | 1.2 | 0.5 | 0 | 2.4 | 0.5 | 3.9 | 1.8 | 0 | 2.3 | 0 | 1.1 | 0 | 0 | 0.8 | 2.3 |
| Cyclists | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| \% Cyclists | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |



Horizon Data Services Ltd 318 Simonston Blvd
Thornhill, ON L3T 4T5
"we always count...never estimated"
File Name : Yonge St at St John`s Sideroad


|  | Yonge St From North |  |  |  |  | St John`s SdRd From East} & \multicolumn{5}{\|l|}{Yonge St From South} & \multicolumn{5}{|l|}{St John`s SdRd From West |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Int. Total |
| Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 04:30 PM | 23 | 105 | 74 | 2 | 204 | 135 | 170 | 56 | 1 | 362 | 67 | 144 | 41 | 1 | 253 | 21 | 119 | 22 | 3 | 165 | 984 |
| 04:45 PM | 27 | 112 | 84 | 0 | 223 | 140 | 160 | 54 | 0 | 354 | 62 | 130 | 27 | 0 | 219 | 10 | 177 | 37 | 0 | 224 | 1020 |
| 05:00 PM | 26 | 111 | 77 | 0 | 214 | 122 | 133 | 56 | 0 | 311 | 85 | 158 | 33 | 0 | 276 | 13 | 143 | 47 | 2 | 205 | 1006 |
| 05:15 PM | 22 | 134 | 85 | 0 | 241 | 156 | 178 | 58 | 0 | 392 | 79 | 153 | 31 | 2 | 265 | 17 | 137 | 30 | 0 | 184 | 1082 |
| Total Volume | 98 | 462 | 320 | 2 | 882 | 553 | 641 | 224 | 1 | 1419 | 293 | 585 | 132 | 3 | 1013 | 61 | 576 | 136 | 5 | 778 | 4092 |
| \% App. Total | 11.1 | 52.4 | 36.3 | 0.2 |  | 39 | 45.2 | 15.8 | 0.1 |  | 28.9 | 57.7 | 13 | 0.3 |  | 7.8 | 74 | 17.5 | 0.6 |  |  |
| PHF | . 907 | . 862 | . 941 | . 250 | . 915 | . 886 | . 900 | . 966 | . 250 | . 905 | . 862 | . 926 | . 805 | . 375 | . 918 | . 726 | . 814 | . 723 | 417 | . 868 | . 945 |
| Cars | 95 | 446 | 315 | , | 858 | 553 | 632 | 221 | 1 | 1407 | 290 | 571 | 132 | 3 | 996 | 61 | 563 | 136 | 5 | 765 | 4026 |
| \% Cars | 96.9 | 96.5 | 98.4 | 100 | 97.3 | 100 | 98.6 | 98.7 | 100 | 99.2 | 99.0 | 97.6 | 100 | 100 | 98.3 | 100 | 97.7 | 100 | 100 | 98.3 | 98.4 |
| Trucks | 2 | 2 | 1 | 0 |  | 0 | 3 | 3 | 0 | 6 | 0 | , | , | 0 | 6 | 0 | 8 |  | 0 | 8 | 25 |
| \% Trucks | 2.0 | 0.4 | 0.3 | 0 | 0.6 | 0 | 0.5 | 1.3 | 0 | 0.4 | 0 | 1.0 | 0 | 0 | 0.6 | 0 | 1.4 | 0 | 0 | 1.0 | 0.6 |
| Heavys | 1 | 12 | 4 | 0 | 17 | 0 | 6 |  | 0 | 6 | 3 | 8 |  | 0 | 11 | 0 | 4 | 0 | 0 | 4 | 38 |
| \% Heavys | 1.0 | 2.6 | 1.3 | 0 | 1.9 | 0 | 0.9 | 0 | 0 | 0.4 | 1.0 | 1.4 | 0 | 0 | 1.1 | 0 | 0.7 | 0 | 0 | 0.5 | 0.9 |
| Cyclists | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 3 |
| \% Cyclists | 0 | 0.4 | 0 | 0 | 0.2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.2 | 0 | 0 | 0.1 | 0.1 |




## Appendix C

## Traffic Signal Timings




Shining Hill Estate Collection, Inc.
Shining Hill Estates, Phase 3, Town of Aurora
Transportation Mobility Plan
March 2021 - 21-1332



PPEEK




|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MIN GREEN | 0 | 20 | 0 | 10 | 7 | 20 | 7 | 10 |
| PASSAGE | 0 | 6.0 | 0 | 3.0 | 3.0 | 6.0 | 3.0 | 3.0 |
| YELLOW | 0 | 5.0 | 0 | 4.5 | 3.0 | 5.0 | 3.0 | 4.5 |
| RED | 0 | 2.5 | 0 | 3.0 | 1.0 | 2.5 | 1.0 | 3.0 |
| MAX I | 0 | 40 | 0 | 30 | 7 | 40 | 12 | 30 |
| MAX II | 0 | 50 | 0 | 50 | 20 | 50 | 12 | 50 |
| WALK | 0 | 7 | 0 | 0 | 0 | 7 | 0 | 7 |
| PED CLEAR | 0 | 22 | 0 | 0 | 0 | 22 | 0 | 24 |
| S/A | 0 | 2.0 | 0 | 0 | 0 | 2.0 | 0 | 0 |
| TBR | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TTR | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| MIN GAP | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| MAX VI | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| MAX EXT | 0 | 30 | 0 | 0 | 0 | 30 | 0 | 0 |
| AUTO MAX | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| AMR | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Range: 0-9.9 or 127 except max times and auto max which are $0-255$ secs.

## Appendix D

## Level of Service Definitions




Shining Hill Estate Collection, Inc.
Shining Hill Estates, Phase 3, Town of Aurora
Transportation Mobility Plan
March 2021 - 21-1332


## LEVEL OF SERVICE ${ }^{1}$

Level of Service (LOS) is defined as a qualitative measure describing operational conditions within a traffic stream, and their perception by motorists and/or passengers. This concept was introduced in the 1965 Highway Capacity Manual as a criteria for interrupted flow conditions. The 2000 Highway Capacity Manual changed the basis for measuring Level of Service at intersections to control delay ${ }^{2}$.

Six Levels of Service are defined with LOS A representing the best operating conditions, and LOS $F$ the worst (briefly described below). It should be noted that there is often significant variability in the amount of delay experienced by individual drivers.

LOS A: This Level of Service describes the highest quality of traffic flow and is referred to as free flow. The approach appears open, turning movements are easily made and drivers have freedom of operation. Control delay is less than 10 seconds/vehicle.

LOS B: $\quad$ This Level of Service is referred to as a stable flow. Drivers feel somewhat restricted and occasionally may have to wait to complete the minor movement. Control delay is $10-15$ seconds/vehicle for unsignalized intersections and 10-20 seconds/vehicle for signalized intersections.

LOS C: $\quad$ At this level, the operation is stable. Drivers feel more restricted and may have to wait, with queues developing for short periods. Control delay is 1525 seconds/vehicle at unsignalized intersections and 20-35 seconds/vehicle at signalized intersections.

LOS D: At this level, traffic is approaching unstable flow. The motorist experiences increasing restriction and instability of flow. There are substantial delays to approaching vehicles during short peaks within the peak period, but there are enough gaps to lower demand to permit occasional clearance of developing queues and prevent excessive back-ups. Control delay is $25-35$ seconds/vehicle at unsignalized intersections and $35-55$ seconds/vehicle at signalized intersections.

LOS E: At this level capacity occurs. Long queues of vehicles exist and delays to vehicles may extend. Control delay is $35-50$ seconds/vehicle at unsignalized intersections and 55-80 seconds/vehicle at signalized intersections.

LOS F: At this Level of Service, the intersection has failed. Capacity of the intersection has been exceeded. Control delay exceeds 50 seconds/vehicle at unsignalized intersections and exceeds 80 seconds/vehicle at signalized intersections.

Transportation Research Board: Highway Capacity Manual 1965, 2000
Control delay is defined as the component of delay that results when a control signal causes a lane group to reduce speed or to stop; it is measured by comparison with the uncontrolled condition.

Level of Traffic Stress Criteria for Road Segments, version 2.0, June, 2017 (converted to metric units)

## Mixed traffic criteria

| Number of lanes | Effective ADT* | Prevailing Speed |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\leq 32 \mathrm{~km} / \mathrm{h}$ | $40 \mathrm{~km} / \mathrm{h}$ | $48 \mathrm{~km} / \mathrm{h}$ | $56 \mathrm{~km} / \mathrm{h}$ | $64 \mathrm{~km} / \mathrm{h}$ | $72 \mathrm{~km} / \mathrm{h}$ | 80+km/h |
| Unlaned 2-way street (no centerline) | 0-750 | $\begin{aligned} & \text { LTS } 1 \\ & \text { LTS } 1 \end{aligned}$ | $\begin{aligned} & \text { LTS } 1 \\ & \text { LTS } 1 \end{aligned}$ | $\begin{aligned} & \hline \text { LTS } 2 \\ & \text { LTS } 2 \end{aligned}$ | LTS 2 | LTS 3 | LTS 3 | LTS 3 |
|  | 751-1500 |  |  |  | LTS 3 | LTS 3 | LTS 3 | LTS 4 |
|  | 1501-3000 | $\begin{aligned} & \text { LTS } 2 \\ & \text { LTS } 2 \end{aligned}$ | LTS 2 | LTS 2 | LTS 3 | LTS 4 | LTS 4 | LTS 4 |
|  | 3000+ |  | LTS 3 | LTS 3 | LTS 3 | LTS 4 | LTS 4 | LTS 4 |
| 1 thru lane per direction (1-way, 1lane street or 2-way street with centerline) | 0-750 | LTS 1 | LTS 1 | LTS 2 | LTS 2 | LTS 3 | LTS 3 | LTS 3 |
|  | 751-1500 | $\begin{aligned} & \text { LTS } 2 \\ & \text { LTS } 2 \end{aligned}$ | LTS 2 |  | LTS 3 | LTS 3 | LTS 3 | LTS 4 |
|  | 1501-3000 |  | LTS 3 | LTS 3 | LTS 3 | LTS 4 | LTS 4 | LTS 4 |
|  | 3000+ | LTS 3 | LTS 3 | LTS 3 | LTS 3 | LTS 4 | LTS 4 | LTS 4 |
| 2 thru lanes per direction | 0-8000 | $\begin{aligned} & \hline \text { LTS } 3 \\ & \text { LTS } 3 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline \text { LTS } 3 \\ & \text { LTS } 3 \end{aligned}$ | $\begin{aligned} & \hline \text { LTS } 3 \\ & \text { LTS } 4 \end{aligned}$ | $\begin{aligned} & \hline \text { LTS } 3 \\ & \text { LTS } 4 \end{aligned}$ | $\begin{aligned} & \hline \text { LTS } 4 \\ & \text { LTS } 4 \end{aligned}$ | $\begin{aligned} & \hline \text { LTS } 4 \\ & \text { LTS } 4 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { LTS } 4 \\ & \text { LTS } 4 \end{aligned}$ |
|  | 8001+ |  |  |  |  |  |  |  |
| 3+ thru lanes per direction | any ADT | LTS 3 | LTS 3 | LTS 4 | LTS 4 | LTS 4 | LTS 4 | LTS 4 |

* Effective ADT = ADT for two-way roads; Effective ADT = 1.5*ADT for one-way roads


## Bike lanes and shoulders not adjacent to a parking lane

| Number of lanes | Bike lane width | Prevailing Speed |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\leq 40 \mathrm{~km} / \mathrm{h}$ | $48 \mathrm{~km} / \mathrm{h}$ | $56 \mathrm{~km} / \mathrm{h}$ | $64 \mathrm{~km} / \mathrm{h}$ | $72 \mathrm{~km} / \mathrm{h}$ | 80+ km/h |
| 1 thru lane per direction, or unlaned | $1.8+\mathrm{m}$ | LTS 1 | LTS 2 | LTS 2 | LTS 3 | LTS 3 | LTS 3 |
|  | 1.2 or 1.5 m | LTS 2 | LTS 2 | LTS 2 | LTS 3 | LTS 3 | LTS 4 |
| 2 thru lanes per direction | $1.8+\mathrm{m}$ | LTS 2 | LTS 2 | LTS 2 | LTS 3 | LTS 3 | LTS 3 |
|  | 1.2 or 1.5 m | LTS 2 | LTS 2 | LTS 2 | LTS 3 | LTS 3 | LTS 4 |
| 3+ lanes per direction | any width | LTS 3 | LTS 3 | LTS 3 | LTS 4 | LTS 4 | LTS 4 |

Notes 1. If bike lane / shoulder is frequently blocked, use mixed traffic criteria.
2. Qualifying bike lane / shoulder should extend at least 1.2 m from a curb at least 1.0 m from a pavement edge or discontinuous gutter pan seam
3.Bike lane width includes any marked buffer next to the bike lane.

Bike lanes alongside a parking lane
Bike lane reach $=$

| Number of lanes | Bike lane reach = <br> Bike + Pkg lane | Prevailing Speed |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | width | $\leq 40 \mathrm{~km} / \mathrm{h}$ | $48 \mathrm{~km} / \mathrm{h}$ | $56 \mathrm{~km} / \mathrm{h}$ |
| 1 lane per direction | 4.6+ m | LTS 1 | LTS 2 | LTS 3 |
|  | $3.7-4.3 \mathrm{~m}$ | LTS 2 | LTS 2 | LTS 3 |
| 2 lanes per direction (2-way) | $4.6+$ m | LTS 2 | LTS 3 | LTS 3 |
| 2-3 lanes per direction (1-way) |  | LTS 2 | LTS 3 | LTS 3 |
| other multilane |  | LTS 3 | LTS 3 | LTS 3 |

Notes 1. If bike lane is frequently blocked, use mixed traffic criteria.
2. Qualifying bike lane must have reach (bike lane width + parking lane width) $\geq 3.7 \mathrm{~m}$
3.Bike lane width includes any marked buffer next to the bike lane.

## Appendix E

## Synchro Analysis Worksheets




Shining Hill Estate Collection, Inc.
Shining Hill Estates, Phase 3, Town of Aurora
Transportation Mobility Plan
March 2021 - 21-1332


|  | 4 | $\rightarrow$ |  | $\checkmark$ | $\checkmark$ |  | 4 | 4 | $p$ | ＊ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 中 ${ }^{\text {a }}$ |  | \％ | $\uparrow$ | F | \％ | ¢ $\uparrow$ | F | \％ | 个4 | 「 |
| Traffic Volume（vph） | 105 | 605 | 150 | 175 | 425 | 265 | 70 | 470 | 240 | 490 | 705 | 140 |
| Future Volume（vph） | 105 | 605 | 150 | 175 | 425 | 265 | 70 | 470 | 240 | 490 | 705 | 140 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.2 | 3.6 | 3.7 | 3.2 | 3.6 | 3.7 | 3.0 | 3.4 | 4.0 | 3.0 | 3.7 | 3.3 |
| Storage Length（ m ） | 65.0 |  | 50.0 | 70.0 |  | 0.0 | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ m ） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | ＊0．75 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  | 1.00 |  | 1.00 |  |  | 1.00 |  |  |  |  | 0.97 |
| Frt |  | 0.970 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1612 | 2703 | 0 | 1708 | 1845 | 1512 | 1652 | 3330 | 1670 | ＊2068 | 3444 | 1516 |
| Flt Permitted | 0.228 |  |  | 0.095 |  |  | 0.352 |  |  | 0.284 |  |  |
| Satd．Flow（perm） | 387 | 2703 | 0 | 171 | 1845 | 1512 | 610 | 3330 | 1670 | 484 | 3444 | 1473 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 17 |  |  |  | 281 |  |  | 186 |  |  | 157 |
| Link Speed（kh） |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance（m） |  | 448.3 |  |  | 341.9 |  |  | 505.9 |  |  | 2054.7 |  |
| Travel Time（s） |  | 26.9 |  |  | 20.5 |  |  | 30.4 |  |  | 123.3 |  |
| Confl．Peds．（\＃／hr） |  |  | 2 | 2 |  |  | 4 |  |  |  |  | 4 |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles（\％） | 7\％ | 2\％ | 2\％ | 1\％ | 3\％ | 8\％ | 2\％ | 6\％ | 1\％ | 4\％ | 6\％ | 3\％ |
| Adj．Flow（vph） | 118 | 680 | 169 | 197 | 478 | 298 | 79 | 528 | 270 | 551 | 792 | 157 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 118 | 849 | 0 | 197 | 478 | 298 | 79 | 528 | 270 | 551 | 792 | 157 |
| Turn Type | pm＋pt | NA |  | pm＋pt | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split（s） | 11.0 | 45.0 |  | 11.0 | 45.0 | 45.0 | 39.5 | 39.5 | 39.5 | 11.0 | 39.5 | 39.5 |
| Total Split（s） | 13.0 | 48.0 |  | 15.0 | 50.0 | 50.0 | 41.0 | 41.0 | 41.0 | 26.0 | 67.0 | 67.0 |
| Total Split（\％） | 10．0\％ | 36．9\％ |  | 11．5\％ | 38．5\％ | 38．5\％ | 31．5\％ | 31．5\％ | 31．5\％ | 20．0\％ | 51．5\％ | 51．5\％ |
| Maximum Green（s） | 9.0 | 40.0 |  | 11.0 | 42.0 | 42.0 | 33.5 | 33.5 | 33.5 | 22.0 | 59.5 | 59.5 |
| Yellow Time（s） | 3.0 | 4.5 |  | 3.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 1.0 | 3.5 |  | 1.0 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 1.0 | 3.0 | 3.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 8.0 |  | 4.0 | 8.0 | 8.0 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None | None | C－Max | C－Max | C－Max | None | C－Max | C－Max |
| Walk Time（s） |  | 7.0 |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  | 30.0 |  |  | 30.0 | 30.0 | 25.0 | 25.0 | 25.0 |  | 25.0 | 25.0 |
| Pedestrian Calls（\＃／hr） |  | 0 |  |  | 0 | 0 | 5 | 5 | 5 |  | 5 | 5 |
| Act Effct Green（s） | 52.7 | 40.0 |  | 57.3 | 42.3 | 42.3 | 33.5 | 33.5 | 33.5 | 63.0 | 59.5 | 59.5 |
| Actuated g／C Ratio | 0.41 | 0.31 |  | 0.44 | 0.33 | 0.33 | 0.26 | 0.26 | 0.26 | 0.48 | 0.46 | 0.46 |


|  | 4 |  |  | 4 |  |  | 4 | 4 | \% |  | $\dagger$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.50 | 1.01 |  | 0.96 | 0.80 | 0.44 | 0.50 | 0.62 | 0.48 | 1.10 | 0.50 | 0.21 |
| Control Delay | 28.8 | 76.6 |  | 84.0 | 51.3 | 6.7 | 54.1 | 46.2 | 16.0 | 95.2 | 26.2 | 3.7 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 28.8 | 76.6 |  | 84.0 | 51.3 | 6.7 | 54.1 | 46.2 | 16.0 | 95.2 | 26.2 | 3.7 |
| LOS | C | E |  | F | D | A | D | D | B | F | C | A |
| Approach Delay |  | 70.8 |  |  | 44.3 |  |  | 37.6 |  |  | 49.2 |  |
| Approach LOS |  | E |  |  | D |  |  | D |  |  | D |  |
| Queue Length 50th (m) | 18.4 | $\sim 152.4$ |  | 36.2 | 117.6 | 3.1 | 18.2 | 66.4 | 17.8 | $\sim 124.2$ | 77.5 | 0.0 |
| Queue Length 95th (m) | 30.9 | \#207.0 |  | \#84.9 | 159.7 | 23.9 | 36.2 | 85.0 | 43.5 | \#192.5 | 94.9 | 12.0 |
| Internal Link Dist (m) |  | 424.3 |  |  | 317.9 |  |  | 481.9 |  |  | 030.7 |  |
| Turn Bay Length (m) | 65.0 |  |  | 70.0 |  |  | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Base Capacity (vph) | 242 | 843 |  | 205 | 600 | 681 | 157 | 858 | 568 | 502 | 1576 | 759 |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.49 | 1.01 |  | 0.96 | 0.80 | 0.44 | 0.50 | 0.62 | 0.48 | 1.10 | 0.50 | 0.21 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 35 (27\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.10 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 50.6 Intersection LOS: D |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 91.6\% ICU Level of Service F |  |  |  |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| * User Entered Value |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 210: Yonge Street \& St. John's Sideroad


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |



Splits and Phases: 220: Bathurst Street \& 18th Sideroad/St. John's Sideroad



|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


|  | 4 |  |  | $\checkmark$ |  |  | 4 | $\dagger$ | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.60 | 1.13 |  | 1.03 | 0.85 | 0.46 | 0.55 | 0.66 | 0.51 | 1.24 | 0.54 | 0.24 |
| Control Delay | 34.2 | 113.2 |  | 101.9 | 55.6 | 8.1 | 58.0 | 47.4 | 19.4 | 148.0 | 12.8 | 0.8 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 34.2 | 113.2 |  | 101.9 | 55.6 | 8.1 | 58.0 | 47.4 | 19.4 | 148.0 | 12.8 | 0.8 |
| LOS | C | F |  | F | E | A | E | D | B | F | B | A |
| Approach Delay |  | 103.7 |  |  | 50.5 |  |  | 39.7 |  |  | 61.1 |  |
| Approach LOS |  | F |  |  | D |  |  | D |  |  | E |  |
| Queue Length 50th (m) | 20.5 | $\sim 196.0$ |  | $\sim 43.4$ | 127.8 | 6.7 | 19.3 | 71.5 | 24.6 | $\sim 155.0$ | 31.8 | 0.0 |
| Queue Length 95th (m) | 33.8 | \#246.4 |  | \#94.0 | \#183.7 | 29.7 | 37.9 | 90.9 | 52.3 m | \#221.5 | m37.5 | m 0.0 |
| Internal Link Dist (m) |  | 424.3 |  |  | 317.9 |  |  | 481.9 |  |  | 2030.7 |  |
| Turn Bay Length (m) | 65.0 |  |  | 70.0 |  |  | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Base Capacity (vph) | 218 | 843 |  | 205 | 599 | 680 | 148 | 858 | 557 | 489 | 1576 | 776 |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.60 | 1.13 |  | 1.03 | 0.85 | 0.46 | 0.55 | 0.66 | 0.51 | 1.24 | 0.54 | 0.24 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 35 (27\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 150 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.24 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 64.4 Intersection LOS: E |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 98.2\% ICU Level of Service F |  |  |  |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| * User Entered Value |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| m Volume for 95th percentile queue is metered by upstream signal. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 210: Yonge Street \& St. John's Sideroad


|  | $\rangle$ |  |  | 7 |  |  | 4 | 4 | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\uparrow$ |  | \% | $\uparrow$ | F | \% | ¢ $\uparrow$ | F | \% | 性 | F |
| Traffic Volume (vph) | 90 | 419 | 50 | 158 | 457 | 43 | 50 | 600 | 61 | 151 | 1100 | 280 |
| Future Volume (vph) | 90 | 419 | 50 | 158 | 457 | 43 | 50 | 600 | 61 | 151 | 1100 | 280 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.7 | 3.7 | 3.7 | 3.0 | 3.5 | 3.7 | 3.2 | 3.7 | 4.0 | 3.1 | 3.3 | 3.7 |
| Storage Length (m) | 30.0 |  | 0.0 | 50.0 |  | 50.0 | 60.0 |  | 60.0 | 60.0 |  | 60.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length ( $m$ ) | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  | 1.00 |  |  |  |  |  |  |  |  |  |  |
| Fit |  | 0.984 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1738 | 1819 | 0 | 1668 | 1807 | 1601 | 1675 | 3510 | 1622 | 1688 | 3388 | 1617 |
| Flt Permitted | 0.175 |  |  | 0.439 |  |  | 0.164 |  |  | 0.275 |  |  |
| Satd. Flow (perm) | 320 | 1819 | 0 | 771 | 1807 | 1601 | 289 | 3510 | 1622 | 489 | 3388 | 1617 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 7 |  |  |  | 122 |  |  | 122 |  |  | 243 |
| Link Speed (kh) |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance (m) |  | 129.9 |  |  | 1758.6 |  |  | 451.2 |  |  | 794.7 |  |
| Travel Time (s) |  | 7.8 |  |  | 105.5 |  |  | 23.2 |  |  | 40.9 |  |
| Confl. Bikes (\#/hr) |  |  | 1 |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles (\%) | 5\% | 4\% | 2\% | 1\% | 4\% | 2\% | 3\% | 4\% | 4\% | 1\% | 3\% | 1\% |
| Adj. Flow (vph) | 95 | 441 | 53 | 166 | 481 | 45 | 53 | 632 | 64 | 159 | 1158 | 295 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 95 | 494 | 0 | 166 | 481 | 45 | 53 | 632 | 64 | 159 | 1158 | 295 |
| Turn Type | pm+pt | NA |  | Perm | NA | Perm | Perm | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 7 | 4 |  |  | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 8 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial ( $s$ ) | 7.0 | 10.0 |  | 10.0 | 10.0 | 10.0 | 20.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 |
| Minimum Split (s) | 11.0 | 17.5 |  | 38.5 | 38.5 | 38.5 | 36.5 | 36.5 | 36.5 | 11.0 | 36.5 | 36.5 |
| Total Split (s) | 16.0 | 37.5 |  | 37.5 | 37.5 | 37.5 | 47.5 | 47.5 | 47.5 | 11.0 | 47.5 | 47.5 |
| Total Split (\%) | 14.3\% | 33.5\% |  | 33.5\% | 33.5\% | 33.5\% | 42.4\% | 42.4\% | 42.4\% | 9.8\% | 42.4\% | 42.4\% |
| Maximum Green (s) | 12.0 | 30.0 |  | 30.0 | 30.0 | 30.0 | 40.0 | 40.0 | 40.0 | 7.0 | 40.0 | 40.0 |
| Yellow Time (s) | 3.0 | 4.5 |  | 4.5 | 4.5 | 4.5 | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 |
| All-Red Time (s) | 1.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 2.5 | 2.5 | 2.5 | 1.0 | 2.5 | 2.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.0 | 7.5 |  | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead/Lag | Lead |  |  | Lag | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 6.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 |
| Recall Mode | None | None |  | None | None | None | Min | Min | Min | None | Min | Min |
| Walk Time (s) |  |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk (s) |  |  |  | 24.0 | 24.0 | 24.0 | 22.0 | 22.0 | 22.0 |  | 22.0 | 22.0 |
| Pedestrian Calls (\#/hr) |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Act Effct Green (s) | 44.5 | 41.0 |  | 30.2 | 30.2 | 30.2 | 31.8 | 31.8 | 31.8 | 46.5 | 43.0 | 43.0 |
| Actuated g/C Ratio | 0.45 | 0.41 |  | 0.30 | 0.30 | 0.30 | 0.32 | 0.32 | 0.32 | 0.47 | 0.43 | 0.43 |



Splits and Phases: 220: Bathurst Street \& 18th Sideroad/St. John's Sideroad



|  | $\rangle$ |  |  | 7 | $\checkmark$ |  | 4 | 4 | $p$ | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | $\uparrow \uparrow$ |  | \％ | $\uparrow$ | F | \％ | ¢ $\uparrow$ | F | \％ | 个个 | 「 |
| Traffic Volume（vph） | 121 | 737 | 179 | 198 | 477 | 291 | 78 | 510 | 268 | 573 | 792 | 173 |
| Future Volume（vph） | 121 | 737 | 179 | 198 | 477 | 291 | 78 | 510 | 268 | 573 | 792 | 173 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.2 | 3.6 | 3.7 | 3.2 | 3.6 | 3.7 | 3.0 | 3.4 | 4.0 | 3.0 | 3.7 | 3.3 |
| Storage Length（m） | 65.0 |  | 50.0 | 70.0 |  | 0.0 | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ $m$ ） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | ＊0．75 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  | 1.00 |  |  |  |  | 1.00 |  |  |  |  | 0.97 |
| Fit |  | 0.971 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1612 | 2706 | 0 | 1708 | 1845 | 1512 | 1652 | 3330 | 1670 | ＊2068 | 3444 | 1516 |
| Flt Permitted | 0.149 |  |  | 0.095 |  |  | 0.320 |  |  | 0.251 |  |  |
| Satd．Flow（perm） | 253 | 2706 | 0 | 171 | 1845 | 1512 | 555 | 3330 | 1670 | 428 | 3444 | 1473 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 17 |  |  |  | 275 |  |  | 162 |  |  | 194 |
| Link Speed（k／h） |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance（m） |  | 448.3 |  |  | 341.9 |  |  | 505.9 |  |  | 2054.7 |  |
| Travel Time（s） |  | 26.9 |  |  | 20.5 |  |  | 30.4 |  |  | 123.3 |  |
| Confl．Peds．（\＃／hr） |  |  | 2 | 2 |  |  | 4 |  |  |  |  | 4 |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles（\％） | 7\％ | 2\％ | 2\％ | 1\％ | 3\％ | 8\％ | 2\％ | 6\％ | 1\％ | 4\％ | 6\％ | 3\％ |
| Adj．Flow（vph） | 136 | 828 | 201 | 222 | 536 | 327 | 88 | 573 | 301 | 644 | 890 | 194 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 136 | 1029 | 0 | 222 | 536 | 327 | 88 | 573 | 301 | 644 | 890 | 194 |
| Turn Type | pm＋pt | NA |  | pm＋pt | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split（s） | 11.0 | 45.0 |  | 11.0 | 45.0 | 45.0 | 39.5 | 39.5 | 39.5 | 11.0 | 39.5 | 39.5 |
| Total Split（s） | 13.0 | 48.0 |  | 15.0 | 50.0 | 50.0 | 41.0 | 41.0 | 41.0 | 26.0 | 67.0 | 67.0 |
| Total Split（\％） | 10．0\％ | 36．9\％ |  | 11．5\％ | 38．5\％ | 38．5\％ | 31．5\％ | 31．5\％ | 31．5\％ | 20．0\％ | 51．5\％ | 51．5\％ |
| Maximum Green（s） | 9.0 | 40.0 |  | 11.0 | 42.0 | 42.0 | 33.5 | 33.5 | 33.5 | 22.0 | 59.5 | 59.5 |
| Yellow Time（s） | 3.0 | 4.5 |  | 3.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 1.0 | 3.5 |  | 1.0 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 1.0 | 3.0 | 3.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 8.0 |  | 4.0 | 8.0 | 8.0 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None | None | C－Max | C－Max | C－Max | None | C－Max | C－Max |
| Walk Time（s） |  | 7.0 |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  | 30.0 |  |  | 30.0 | 30.0 | 25.0 | 25.0 | 25.0 |  | 25.0 | 25.0 |
| Pedestrian Calls（\＃／hr） |  | 0 |  |  | 0 | 0 | 5 | 5 | 5 |  | 5 | 5 |
| Act Effct Green（s） | 52.9 | 40.0 |  | 57.1 | 42.1 | 42.1 | 33.5 | 33.5 | 33.5 | 63.0 | 59.5 | 59.5 |
| Actuated g／C Ratio | 0.41 | 0.31 |  | 0.44 | 0.32 | 0.32 | 0.26 | 0.26 | 0.26 | 0.48 | 0.46 | 0.46 |


|  |  |  |  |  |  |  |  | $\uparrow$ | 7 |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.69 | 1.22 |  | 1.08 | 0.90 | 0.48 | 0.62 | 0.67 | 0.55 | 1.33 | 0.56 | 0.25 |
| Control Delay | 41.8 | 147.8 |  | 117.7 | 61.2 | 9.2 | 63.0 | 47.8 | 22.8 | 187.8 | 13.7 | 0.8 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 41.8 | 147.8 |  | 117.7 | 61.2 | 9.2 | 63.0 | 47.8 | 22.8 | 187.8 | 13.7 | 0.8 |
| LOS | D | F |  | F | E | A | E | D | C | F | B | A |
| Approach Delay |  | 135.4 |  |  | 57.1 |  |  | 41.3 |  |  | 77.2 |  |
| Approach LOS |  | F |  |  | E |  |  | D |  |  | E |  |
| Queue Length 50th (m) | 21.5 | $\sim 225.4$ |  | $\sim 49.6$ | 137.8 | 9.8 | 21.0 | 73.3 | 31.4 | $\sim 180.2$ | 35.7 | 0.0 |
| Queue Length 95th (m) | \#38.2 | \#276.2 |  | \#100.8 | \#200.0 | 34.7 | \#44.0 | 92.8 | 60.4 m | \#248.4 | m41.9 | m0.0 |
| Internal Link Dist (m) |  | 424.3 |  |  | 317.9 |  |  | 481.9 |  |  | 2030.7 |  |
| Turn Bay Length (m) | 65.0 |  |  | 70.0 |  |  | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Base Capacity (vph) | 197 | 844 |  | 205 | 597 | 675 | 143 | 858 | 550 | 484 | 1576 | 779 |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.69 | 1.22 |  | 1.08 | 0.90 | 0.48 | 0.62 | 0.67 | 0.55 | 1.33 | 0.56 | 0.25 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 35 (27\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 150 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.33 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 79.5 |  |  |  | Intersection LOS: E |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 102.8\% |  |  |  | ICU Level of Service G |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| * User Entered Value |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| $m$ Volume for 95 th percentile queue is metered by upstream signal. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 210: Yonge Street \& St. John's Sideroad


|  | $\rangle$ |  |  | 7 |  |  | 4 | 4 | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | $\uparrow$ |  | \％ | $\uparrow$ | F | \％ | 个个 | F | \％ | 个个 | F |
| Traffic Volume（vph） | 95 | 459 | 55 | 168 | 482 | 48 | 55 | 610 | 61 | 166 | 1205 | 300 |
| Future Volume（vph） | 95 | 459 | 55 | 168 | 482 | 48 | 55 | 610 | 61 | 166 | 1205 | 300 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.7 | 3.7 | 3.7 | 3.0 | 3.5 | 3.7 | 3.2 | 3.7 | 4.0 | 3.1 | 3.3 | 3.7 |
| Storage Length（m） | 30.0 |  | 0.0 | 50.0 |  | 50.0 | 60.0 |  | 60.0 | 60.0 |  | 60.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ $m$ ） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  | 1.00 |  |  |  |  |  |  |  |  |  |  |
| Fit |  | 0.984 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1738 | 1819 | 0 | 1668 | 1807 | 1601 | 1675 | 3510 | 1622 | 1688 | 3388 | 1617 |
| Flt Permitted | 0.121 |  |  | 0.351 |  |  | 0.127 |  |  | 0.283 |  |  |
| Satd．Flow（perm） | 221 | 1819 | 0 | 616 | 1807 | 1601 | 224 | 3510 | 1622 | 503 | 3388 | 1617 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 7 |  |  |  | 122 |  |  | 122 |  |  | 238 |
| Link Speed（kh） |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance（m） |  | 129.9 |  |  | 1758.6 |  |  | 451.2 |  |  | 794.7 |  |
| Travel Time（s） |  | 7.8 |  |  | 105.5 |  |  | 23.2 |  |  | 40.9 |  |
| Confl．Bikes（\＃／hr） |  |  | 1 |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles（\％） | 5\％ | 4\％ | 2\％ | 1\％ | 4\％ | 2\％ | 3\％ | 4\％ | 4\％ | 1\％ | 3\％ | 1\％ |
| Adj．Flow（vph） | 100 | 483 | 58 | 177 | 507 | 51 | 58 | 642 | 64 | 175 | 1268 | 316 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 100 | 541 | 0 | 177 | 507 | 51 | 58 | 642 | 64 | 175 | 1268 | 316 |
| Turn Type | pm＋pt | NA |  | Perm | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | 4 |  |  | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 8 | 8 | 8 | 6 | 6 | － | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（ $s$ ） | 7.0 | 10.0 |  | 10.0 | 10.0 | 10.0 | 20.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 |
| Minimum Split（s） | 11.0 | 17.5 |  | 38.5 | 38.5 | 38.5 | 36.5 | 36.5 | 36.5 | 11.0 | 36.5 | 36.5 |
| Total Split（s） | 16.0 | 37.5 |  | 37.5 | 37.5 | 37.5 | 47.5 | 47.5 | 47.5 | 11.0 | 47.5 | 47.5 |
| Total Split（\％） | 14．3\％ | 33．5\％ |  | 33．5\％ | 33．5\％ | 33．5\％ | 42．4\％ | 42．4\％ | 42．4\％ | 9．8\％ | 42．4\％ | 42．4\％ |
| Maximum Green（s） | 12.0 | 30.0 |  | 30.0 | 30.0 | 30.0 | 40.0 | 40.0 | 40.0 | 7.0 | 40.0 | 40.0 |
| Yellow Time（s） | 3.0 | 4.5 |  | 4.5 | 4.5 | 4.5 | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 |
| All－Red Time（s） | 1.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 2.5 | 2.5 | 2.5 | 1.0 | 2.5 | 2.5 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 7.5 |  | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead |  |  | Lag | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes |  |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 6.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 |
| Recall Mode | None | None |  | None | None | None | Min | Min | Min | None | Min | Min |
| Walk Time（s） |  |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  |  |  | 24.0 | 24.0 | 24.0 | 22.0 | 22.0 | 22.0 |  | 22.0 | 22.0 |
| Pedestrian Calls（\＃／hr） |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Act Effct Green（s） | 45.0 | 41.4 |  | 30.3 | 30.3 | 30.3 | 36.2 | 36.2 | 36.2 | 50.9 | 47.3 | 47.3 |
| Actuated g／C Ratio | 0.43 | 0.40 |  | 0.29 | 0.29 | 0.29 | 0.35 | 0.35 | 0.35 | 0.49 | 0.46 | 0.46 |



Splits and Phases: 220: Bathurst Street \& 18th Sideroad/St. John's Sideroad



|  | $\rangle$ |  |  | 7 |  |  | 4 | $\dagger$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 个1 |  | \％ | $\uparrow$ | F | \％ | 个个 | F | \％ | 个4 | F |
| Traffic Volume（vph） | 144 | 717 | 202 | 183 | 482 | 281 | 95 | 497 | 248 | 538 | 754 | 182 |
| Future Volume（vph） | 144 | 717 | 202 | 183 | 482 | 281 | 95 | 497 | 248 | 538 | 754 | 182 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.2 | 3.6 | 3.7 | 3.2 | 3.6 | 3.7 | 3.0 | 3.4 | 4.0 | 3.0 | 3.7 | 3.3 |
| Storage Length（m） | 65.0 |  | 50.0 | 70.0 |  | 0.0 | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ m ） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | ＊0．75 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  | 1.00 |  |  |  |  | 1.00 |  |  |  |  | 0.97 |
| Fit |  | 0.967 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1612 | 2694 | 0 | 1708 | 1845 | 1512 | 1652 | 3330 | 1670 | ＊2068 | 3444 | 1516 |
| Flt Permitted | 0.140 |  |  | 0.095 |  |  | 0.334 |  |  | 0.262 |  |  |
| Satd．Flow（perm） | 238 | 2694 | 0 | 171 | 1845 | 1512 | 579 | 3330 | 1670 | 447 | 3444 | 1473 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 20 |  |  |  | 262 |  |  | 167 |  |  | 204 |
| Link Speed（kh） |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance（m） |  | 448.3 |  |  | 341.9 |  |  | 505.9 |  |  | 608.7 |  |
| Travel Time（s） |  | 26.9 |  |  | 20.5 |  |  | 30.4 |  |  | 36.5 |  |
| Confl．Peds．（\＃／hr） |  |  | 2 | 2 |  |  | 4 |  |  |  |  | 4 |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles（\％） | 7\％ | 2\％ | 2\％ | 1\％ | 3\％ | 8\％ | 2\％ | 6\％ | 1\％ | 4\％ | 6\％ | 3\％ |
| Adj．Flow（vph） | 162 | 806 | 227 | 206 | 542 | 316 | 107 | 558 | 279 | 604 | 847 | 204 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 162 | 1033 | 0 | 206 | 542 | 316 | 107 | 558 | 279 | 604 | 847 | 204 |
| Turn Type | pm＋pt | NA |  | pm＋pt | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（ s ） | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split（s） | 11.0 | 45.0 |  | 11.0 | 45.0 | 45.0 | 39.5 | 39.5 | 39.5 | 11.0 | 39.5 | 39.5 |
| Total Split（s） | 13.0 | 48.0 |  | 15.0 | 50.0 | 50.0 | 41.0 | 41.0 | 41.0 | 26.0 | 67.0 | 67.0 |
| Total Split（\％） | 10．0\％ | 36．9\％ |  | 11．5\％ | 38．5\％ | 38．5\％ | 31．5\％ | 31．5\％ | 31．5\％ | 20．0\％ | 51．5\％ | 51．5\％ |
| Maximum Green（s） | 9.0 | 40.0 |  | 11.0 | 42.0 | 42.0 | 33.5 | 33.5 | 33.5 | 22.0 | 59.5 | 59.5 |
| Yellow Time（s） | 3.0 | 4.5 |  | 3.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 1.0 | 3.5 |  | 1.0 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 1.0 | 3.0 | 3.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 8.0 |  | 4.0 | 8.0 | 8.0 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None | None | C－Max | C－Max | C－Max | None | C－Max | C－Max |
| Walk Time（s） |  | 7.0 |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  | 30.0 |  |  | 30.0 | 30.0 | 25.0 | 25.0 | 25.0 |  | 25.0 | 25.0 |
| Pedestrian Calls（\＃／hr） |  | 0 |  |  | 0 | 0 | 5 | 5 | 5 |  | 5 | 5 |
| Act Effct Green（s） | 53.0 | 40.0 |  | 57.0 | 42.0 | 42.0 | 33.5 | 33.5 | 33.5 | 63.0 | 59.5 | 59.5 |
| Actuated g／C Ratio | 0.41 | 0.31 |  | 0.44 | 0.32 | 0.32 | 0.26 | 0.26 | 0.26 | 0.48 | 0.46 | 0.46 |


|  | 4 |  |  | $\dagger$ |  |  | 4 | $\dagger$ | \% |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.84 | 1.23 |  | 1.00 | 0.91 | 0.48 | 0.72 | 0.65 | 0.50 | 1.23 | 0.54 | 0.26 |
| Control Delay | 59.7 | 150.8 |  | 95.9 | 63.0 | 9.5 | 71.5 | 47.2 | 19.4 | 147.6 | 15.8 | 0.9 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 59.7 | 150.8 |  | 95.9 | 63.0 | 9.5 | 71.5 | 47.2 | 19.4 | 147.6 | 15.8 | 0.9 |
| LOS | E | F |  | F | E | A | E | D | B | F | B | A |
| Approach Delay |  | 138.4 |  |  | 53.5 |  |  | 41.8 |  |  | 62.1 |  |
| Approach LOS |  | F |  |  | D |  |  | D |  |  | E |  |
| Queue Length 50th (m) | 26.0 | $\sim 226.8$ |  | ~39.3 | 139.9 | 10.2 | 26.4 | 71.0 | 24.4 | ~155.8 | 41.2 | 0.0 |
| Queue Length 95th (m) | \#58.9 | \#277.7 |  | \#90.6 | \#203.9 | 34.6 | \#56.3 | 90.1 | 51.7 m | \#216.8 | m47.2 | m0.0 |
| Internal Link Dist (m) |  | 424.3 |  |  | 317.9 |  |  | 481.9 |  |  | 584.7 |  |
| Turn Bay Length (m) | 65.0 |  |  | 70.0 |  |  | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Base Capacity (vph) | 192 | 842 |  | 205 | 596 | 665 | 149 | 858 | 554 | 490 | 1576 | 784 |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.84 | 1.23 |  | 1.00 | 0.91 | 0.48 | 0.72 | 0.65 | 0.50 | 1.23 | 0.54 | 0.26 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 35 (27\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 150 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.23 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 75.0 Intersection LOS: E |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 99.9\% ICU Level of Service F |  |  |  |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| * User Entered Value |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| $m$ Volume for 95th percentile queue is metered by upstream signal. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 210: Yonge Street \& St. John's Sideroad


|  | $\rangle$ |  |  | 7 |  |  | 4 | 4 | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | $\uparrow$ |  | \％ | $\uparrow$ | F | \％ | ¢ $\uparrow$ | 「 | \％ | 个个 | F |
| Traffic Volume（vph） | 90 | 433 | 50 | 180 | 485 | 52 | 50 | 600 | 78 | 164 | 1100 | 280 |
| Future Volume（vph） | 90 | 433 | 50 | 180 | 485 | 52 | 50 | 600 | 78 | 164 | 1100 | 280 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.7 | 3.7 | 3.7 | 3.0 | 3.5 | 3.7 | 3.2 | 3.7 | 4.0 | 3.1 | 3.3 | 3.7 |
| Storage Length（m） | 30.0 |  | 0.0 | 50.0 |  | 50.0 | 60.0 |  | 60.0 | 60.0 |  | 60.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ $m$ ） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  | 1.00 |  |  |  |  |  |  |  |  |  |  |
| Fit |  | 0.984 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1738 | 1819 | 0 | 1668 | 1807 | 1601 | 1675 | 3510 | 1622 | 1688 | 3388 | 1617 |
| Flt Permitted | 0.140 |  |  | 0.419 |  |  | 0.163 |  |  | 0.275 |  |  |
| Satd．Flow（perm） | 256 | 1819 | 0 | 736 | 1807 | 1601 | 287 | 3510 | 1622 | 489 | 3388 | 1617 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 6 |  |  |  | 122 |  |  | 122 |  |  | 243 |
| Link Speed（kh） |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance（m） |  | 129.9 |  |  | 1758.6 |  |  | 451.2 |  |  | 794.7 |  |
| Travel Time（s） |  | 7.8 |  |  | 105.5 |  |  | 23.2 |  |  | 40.9 |  |
| Confl．Bikes（\＃／hr） |  |  | 1 |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles（\％） | 5\％ | 4\％ | 2\％ | 1\％ | 4\％ | 2\％ | 3\％ | 4\％ | 4\％ | 1\％ | 3\％ | 1\％ |
| Adj．Flow（vph） | 95 | 456 | 53 | 189 | 511 | 55 | 53 | 632 | 82 | 173 | 1158 | 295 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 95 | 509 | 0 | 189 | 511 | 55 | 53 | 632 | 82 | 173 | 1158 | 295 |
| Turn Type | pm＋pt | NA |  | Perm | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | 4 |  |  | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 8 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（ $s$ ） | 7.0 | 10.0 |  | 10.0 | 10.0 | 10.0 | 20.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 |
| Minimum Split（s） | 11.0 | 17.5 |  | 38.5 | 38.5 | 38.5 | 36.5 | 36.5 | 36.5 | 11.0 | 36.5 | 36.5 |
| Total Split（s） | 16.0 | 37.5 |  | 37.5 | 37.5 | 37.5 | 47.5 | 47.5 | 47.5 | 11.0 | 47.5 | 47.5 |
| Total Split（\％） | 14．3\％ | 33．5\％ |  | 33．5\％ | 33．5\％ | 33．5\％ | 42．4\％ | 42．4\％ | 42．4\％ | 9．8\％ | 42．4\％ | 42．4\％ |
| Maximum Green（s） | 12.0 | 30.0 |  | 30.0 | 30.0 | 30.0 | 40.0 | 40.0 | 40.0 | 7.0 | 40.0 | 40.0 |
| Yellow Time（s） | 3.0 | 4.5 |  | 4.5 | 4.5 | 4.5 | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 |
| All－Red Time（s） | 1.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 2.5 | 2.5 | 2.5 | 1.0 | 2.5 | 2.5 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 7.5 |  | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead |  |  | Lag | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes |  |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 6.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 |
| Recall Mode | None | None |  | None | None | None | Min | Min | Min | None | Min | Min |
| Walk Time（s） |  |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  |  |  | 24.0 | 24.0 | 24.0 | 22.0 | 22.0 | 22.0 |  | 22.0 | 22.0 |
| Pedestrian Calls（\＃／hr） |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Act Effct Green（s） | 44.8 | 41.3 |  | 30.5 | 30.5 | 30.5 | 32.0 | 32.0 | 32.0 | 46.7 | 43.2 | 43.2 |
| Actuated g／C Ratio | 0.45 | 0.41 |  | 0.31 | 0.31 | 0.31 | 0.32 | 0.32 | 0.32 | 0.47 | 0.43 | 0.43 |


|  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Splits and Phases: 220: Bathurst Street \& 18th Sideroad/St. John's Sideroad


|  | $\rangle$ |  |  | 7 |  |  |  | $\dagger$ | + |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\uparrow$ | F | \% | $\uparrow$ | 「 |  | ¢ |  | \% | $\hat{F}$ |  |
| Traffic Volume (veh/h) | 52 | 890 | 3 | 20 | 666 | 72 | 1 | 4 | 65 | 107 | 4 | 66 |
| Future Volume (Veh/h) | 52 | 890 | 3 | 20 | 666 | 72 | 1 | 4 | 65 | 107 | 4 | 66 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Hourly flow rate (vph) | 55 | 947 | 3 | 21 | 709 | 77 | 1 | 4 | 69 | 114 | 4 | 70 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (m/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  | None |  |  | None |  |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal ( $m$ ) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| VC , conflicting volume | 786 |  |  | 950 |  |  | 1880 | 1885 | 947 | 1879 | 1811 | 709 |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu, unblocked vol | 786 |  |  | 950 |  |  | 1880 | 1885 | 947 | 1879 | 1811 | 709 |
| tC , single (s) | 4.1 |  |  | 4.1 |  |  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 2.2 |  |  | 2.2 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free \% | 93 |  |  | 97 |  |  | 98 | 94 | 78 | 0 | 94 | 84 |
| cM capacity (veh/h) | 842 |  |  | 711 |  |  | 41 | 65 | 317 | 38 | 72 | 438 |
| Direction, Lane \# | EB 1 | EB 2 | EB 3 | WB 1 | WB 2 | WB 3 | NB 1 | SB 1 | SB 2 |  |  |  |
| Volume Total | 55 | 947 | 3 | 21 | 709 | 77 | 74 | 114 | 74 |  |  |  |
| Volume Left | 55 | 0 | 0 | 21 | 0 | 0 | 1 | 114 | 0 |  |  |  |
| Volume Right | 0 | 0 | 3 | 0 | 0 | 77 | 69 | 0 | 70 |  |  |  |
| cSH | 842 | 1700 | 1700 | 711 | 1700 | 1700 | 244 | 38 | 343 |  |  |  |
| Volume to Capacity | 0.07 | 0.56 | 0.00 | 0.03 | 0.42 | 0.05 | 0.30 | 2.99 | 0.22 |  |  |  |
| Queue Length 95th ( m ) | 1.7 | 0.0 | 0.0 | 0.7 | 0.0 | 0.0 | 9.9 | 102.5 | 6.4 |  |  |  |
| Control Delay (s) | 9.6 | 0.0 | 0.0 | 10.2 | 0.0 | 0.0 | 26.1 | 1119.2 | 18.3 |  |  |  |
| Lane LOS | A |  |  | B |  |  | D | F | C |  |  |  |
| Approach Delay (s) | 0.5 |  |  | 0.3 |  |  | 26.1 | 685.9 |  |  |  |  |
| Approach LOS |  |  |  |  |  |  | D | F |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 63.5 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 66.1\% |  | CU Level | f Service |  |  | C |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |


|  | $\stackrel{ }{*}$ |  |  | 7 |  |  | 4 | 4 | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个 ${ }^{\text {a }}$ |  | \％ | 4 | F | ${ }^{7}$ | 个4 | F | \％ | 个4 | F |
| Traffic Volume（vph） | 164 | 833 | 247 | 179 | 570 | 291 | 123 | 501 | 250 | 573 | 782 | 214 |
| Future Volume（vph） | 164 | 833 | 247 | 179 | 570 | 291 | 123 | 501 | 250 | 573 | 782 | 214 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.2 | 3.6 | 3.7 | 3.2 | 3.6 | 3.7 | 3.0 | 3.4 | 4.0 | 3.0 | 3.7 | 3.3 |
| Storage Length（ m ） | 65.0 |  | 50.0 | 70.0 |  | 0.0 | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ m ） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | ＊0．75 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  | 1.00 |  |  |  |  | 1.00 |  |  |  |  | 0.97 |
| Frt |  | 0.966 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1612 | 2690 | 0 | 1708 | 1845 | 1512 | 1652 | 3330 | 1670 | ＊2068 | 3444 | 1516 |
| Flt Permitted | 0.100 |  |  | 0.095 |  |  | 0.323 |  |  | 0.258 |  |  |
| Satd．Flow（perm） | 170 | 2690 | 0 | 171 | 1845 | 1512 | 560 | 3330 | 1670 | 440 | 3444 | 1473 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 21 |  |  |  | 230 |  |  | 156 |  |  | 240 |
| Link Speed（kh） |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance（m） |  | 448.3 |  |  | 341.9 |  |  | 505.9 |  |  | 608.7 |  |
| Travel Time（s） |  | 26.9 |  |  | 20.5 |  |  | 30.4 |  |  | 36.5 |  |
| Confl．Peds．（\＃／hr） |  |  | 2 | 2 |  |  | 4 |  |  |  |  | 4 |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles（\％） | 7\％ | 2\％ | 2\％ | 1\％ | 3\％ | 8\％ | 2\％ | 6\％ | 1\％ | 4\％ | 6\％ | 3\％ |
| Adj．Flow（vph） | 184 | 936 | 278 | 201 | 640 | 327 | 138 | 563 | 281 | 644 | 879 | 240 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 184 | 1214 | 0 | 201 | 640 | 327 | 138 | 563 | 281 | 644 | 879 | 240 |
| Turn Type | pm＋pt | NA |  | pm＋pt | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split（s） | 11.0 | 45.0 |  | 11.0 | 45.0 | 45.0 | 39.5 | 39.5 | 39.5 | 11.0 | 39.5 | 39.5 |
| Total Split（s） | 13.0 | 48.0 |  | 15.0 | 50.0 | 50.0 | 41.0 | 41.0 | 41.0 | 26.0 | 67.0 | 67.0 |
| Total Split（\％） | 10．0\％ | 36．9\％ |  | 11．5\％ | 38．5\％ | 38．5\％ | 31．5\％ | 31．5\％ | 31．5\％ | 20．0\％ | 51．5\％ | 51．5\％ |
| Maximum Green（s） | 9.0 | 40.0 |  | 11.0 | 42.0 | 42.0 | 33.5 | 33.5 | 33.5 | 22.0 | 59.5 | 59.5 |
| Yellow Time（s） | 3.0 | 4.5 |  | 3.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 1.0 | 3.5 |  | 1.0 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 1.0 | 3.0 | 3.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 8.0 |  | 4.0 | 8.0 | 8.0 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None | None | C－Max | C－Max | C－Max | None | C－Max | C－Max |
| Walk Time（s） |  | 7.0 |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  | 30.0 |  |  | 30.0 | 30.0 | 25.0 | 25.0 | 25.0 |  | 25.0 | 25.0 |
| Pedestrian Calls（\＃／hr） |  | 0 |  |  | 0 | 0 | 5 | 5 | 5 |  | 5 | 5 |
| Act Effct Green（s） | 53.0 | 40.0 |  | 57.0 | 42.0 | 42.0 | 33.5 | 33.5 | 33.5 | 63.0 | 59.5 | 59.5 |
| Actuated g／C Ratio | 0.41 | 0.31 |  | 0.44 | 0.32 | 0.32 | 0.26 | 0.26 | 0.26 | 0.48 | 0.46 | 0.46 |


|  | 4 |  |  | $\downarrow$ |  |  | 4 | $\dagger$ | \% |  | $\dagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 1.09 | 1.44 |  | 0.98 | 1.07 | 0.51 | 0.96 | 0.66 | 0.51 | 1.32 | 0.56 | 0.30 |
| Control Delay | 124.3 | 239.4 |  | 89.4 | 100.3 | 13.5 | 113.1 | 47.4 | 21.4 | 183.5 | 16.1 | 1.0 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 124.3 | 239.4 |  | 89.4 | 100.3 | 13.5 | 113.1 | 47.4 | 21.4 | 183.5 | 16.1 | 1.0 |
| LOS | F | F |  | F | F | B | F | D | C | F | B | A |
| Approach Delay |  | 224.3 |  |  | 74.1 |  |  | 49.2 |  |  | 75.2 |  |
| Approach LOS |  | F |  |  | E |  |  | D |  |  | E |  |
| Queue Length 50th (m) | ~39.2 | ~295.5 |  | 37.4 | $\sim 191.6$ | 18.9 | 36.9 | 71.7 | 27.7 | ~180.1 | 44.1 | 0.0 |
| Queue Length 95th (m) | \#87.0 | \#346.7 |  | \#87.2 | \#261.6 | 47.0 | \#79.5 | 91.1 | 55.4 m | \#241.5 | m49.1 | m 0.0 |
| Internal Link Dist (m) |  | 424.3 |  |  | 317.9 |  |  | 481.9 |  |  | 584.7 |  |
| Turn Bay Length (m) | 65.0 |  |  | 70.0 |  |  | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Base Capacity (vph) | 169 | 842 |  | 205 | 596 | 644 | 144 | 858 | 546 | 488 | 1576 | 804 |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 1.09 | 1.44 |  | 0.98 | 1.07 | 0.51 | 0.96 | 0.66 | 0.51 | 1.32 | 0.56 | 0.30 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 35 (27\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 140 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.44 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 109.4 Intersection LOS: F |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 106.1\% ICU Level of Service G |  |  |  |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| * User Entered Value |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| $m$ Volume for 95th percentile queue is metered by upstream signal. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 210: Yonge Street \& St. John's Sideroad


|  | $\rangle$ |  |  | 7 |  |  | 4 | 4 | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | $\uparrow$ |  | \％ | $\uparrow$ | F | \％ | 个个 | F | \％ | 个个 | F |
| Traffic Volume（vph） | 95 | 505 | 55 | 210 | 522 | 70 | 55 | 610 | 113 | 200 | 1205 | 300 |
| Future Volume（vph） | 95 | 505 | 55 | 210 | 522 | 70 | 55 | 610 | 113 | 200 | 1205 | 300 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.7 | 3.7 | 3.7 | 3.0 | 3.5 | 3.7 | 3.2 | 3.7 | 4.0 | 3.1 | 3.3 | 3.7 |
| Storage Length（m） | 30.0 |  | 0.0 | 50.0 |  | 50.0 | 60.0 |  | 60.0 | 60.0 |  | 60.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ $m$ ） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  | 1.00 |  |  |  |  |  |  |  |  |  |  |
| Fit |  | 0.985 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1738 | 1821 | 0 | 1668 | 1807 | 1601 | 1675 | 3510 | 1622 | 1688 | 3388 | 1617 |
| Flt Permitted | 0.117 |  |  | 0.283 |  |  | 0.127 |  |  | 0.283 |  |  |
| Satd．Flow（perm） | 214 | 1821 | 0 | 497 | 1807 | 1601 | 224 | 3510 | 1622 | 503 | 3388 | 1617 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 6 |  |  |  | 122 |  |  | 122 |  |  | 238 |
| Link Speed（kh） |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance（m） |  | 129.9 |  |  | 1758.6 |  |  | 451.2 |  |  | 794.7 |  |
| Travel Time（s） |  | 7.8 |  |  | 105.5 |  |  | 23.2 |  |  | 40.9 |  |
| Confl．Bikes（\＃／hr） |  |  | 1 |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles（\％） | 5\％ | 4\％ | 2\％ | 1\％ | 4\％ | 2\％ | 3\％ | 4\％ | 4\％ | 1\％ | 3\％ | 1\％ |
| Adj．Flow（vph） | 100 | 532 | 58 | 221 | 549 | 74 | 58 | 642 | 119 | 211 | 1268 | 316 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 100 | 590 | 0 | 221 | 549 | 74 | 58 | 642 | 119 | 211 | 1268 | 316 |
| Turn Type | pm＋pt | NA |  | Perm | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | 4 |  |  | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 8 | 8 | 8 | － | 6 | － | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（ $s$ ） | 7.0 | 10.0 |  | 10.0 | 10.0 | 10.0 | 20.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 |
| Minimum Split（s） | 11.0 | 17.5 |  | 38.5 | 38.5 | 38.5 | 36.5 | 36.5 | 36.5 | 11.0 | 36.5 | 36.5 |
| Total Split（s） | 16.0 | 37.5 |  | 37.5 | 37.5 | 37.5 | 47.5 | 47.5 | 47.5 | 11.0 | 47.5 | 47.5 |
| Total Split（\％） | 14．3\％ | 33．5\％ |  | 33．5\％ | 33．5\％ | 33．5\％ | 42．4\％ | 42．4\％ | 42．4\％ | 9．8\％ | 42．4\％ | 42．4\％ |
| Maximum Green（s） | 12.0 | 30.0 |  | 30.0 | 30.0 | 30.0 | 40.0 | 40.0 | 40.0 | 7.0 | 40.0 | 40.0 |
| Yellow Time（s） | 3.0 | 4.5 |  | 4.5 | 4.5 | 4.5 | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 |
| All－Red Time（s） | 1.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 2.5 | 2.5 | 2.5 | 1.0 | 2.5 | 2.5 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 7.5 |  | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead |  |  | Lag | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes |  |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 6.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 |
| Recall Mode | None | None |  | None | None | None | Min | Min | Min | None | Min | Min |
| Walk Time（s） |  |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  |  |  | 24.0 | 24.0 | 24.0 | 22.0 | 22.0 | 22.0 |  | 22.0 | 22.0 |
| Pedestrian Calls（\＃／hr） |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Act Effct Green（s） | 45.0 | 41.4 |  | 30.3 | 30.3 | 30.3 | 36.2 | 36.2 | 36.2 | 50.9 | 47.3 | 47.3 |
| Actuated g／C Ratio | 0.43 | 0.40 |  | 0.29 | 0.29 | 0.29 | 0.35 | 0.35 | 0.35 | 0.49 | 0.46 | 0.46 |



Splits and Phases: 220: Bathurst Street \& 18th Sideroad/St. John's Sideroad


|  | 4 |  |  | 7 |  | 4 | 4 | 4 | $>$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\uparrow$ | F | \% | $\uparrow$ | 「 |  | ¢ |  | \% | F |  |
| Traffic Volume (veh/h) | 160 | 945 | 3 | 20 | 681 | 206 | 1 | 14 | 65 | 234 | 14 | 132 |
| Future Volume (Veh/h) | 160 | 945 | 3 | 20 | 681 | 206 | 1 | 14 | 65 | 234 | 14 | 132 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Hourly flow rate (vph) | 170 | 1005 | 3 | 21 | 724 | 219 | 1 | 15 | 69 | 249 | 15 | 140 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (m/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  | None |  |  | None |  |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal ( $m$ ) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| VC , conflicting volume | 943 |  |  | 1008 |  |  | 2258 | 2330 | 1005 | 2188 | 2114 | 724 |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu, unblocked vol | 943 |  |  | 1008 |  |  | 2258 | 2330 | 1005 | 2188 | 2114 | 724 |
| tC , single (s) | 4.1 |  |  | 4.1 |  |  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 2.2 |  |  | 2.2 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free \% | 77 |  |  | 97 |  |  | 91 | 46 | 76 | 0 | 61 | 67 |
| cM capacity (veh/h) | 736 |  |  | 676 |  |  | 11 | 28 | 293 | 12 | 38 | 429 |
| Direction, Lane \# | EB 1 | EB 2 | EB 3 | WB 1 | WB 2 | WB 3 | NB 1 | SB 1 | SB 2 |  |  |  |
| Volume Total | 170 | 1005 | 3 | 21 | 724 | 219 | 85 | 249 | 155 |  |  |  |
| Volume Left | 170 | 0 | 0 | 21 | 0 | 0 | 1 | 249 | 0 |  |  |  |
| Volume Right | 0 | 0 | 3 | 0 | 0 | 219 | 69 | 0 | 140 |  |  |  |
| CSH | 736 | 1700 | 1700 | 676 | 1700 | 1700 | 99 | 12 | 216 |  |  |  |
| Volume to Capacity | 0.23 | 0.59 | 0.00 | 0.03 | 0.43 | 0.13 | 0.86 | 20.69 | 0.72 |  |  |  |
| Queue Length 95th ( m ) | 7.1 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 | 38.8 | Err | 37.7 |  |  |  |
| Control Delay (s) | 11.4 | 0.0 | 0.0 | 10.5 | 0.0 | 0.0 | 133.0 | Err | 55.3 |  |  |  |
| Lane LOS | B |  |  | B |  |  | F | F | F |  |  |  |
| Approach Delay (s) | 1.6 |  |  | 0.2 |  |  | 133.0 | 6184.0 |  |  |  |  |
| Approach LOS |  |  |  |  |  |  | F | F |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 954.7 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 82.7\% |  | CU Level | f Service |  |  | E |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |


| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | 7 | 个t |  | \％ | $\uparrow$ | 「 | \％ | 个个 | F | \％ | 个4 | F |
| Traffic Volume（vph） | 145 | 475 | 75 | 245 | 550 | 630 | 130 | 830 | 255 | 310 | 605 | 120 |
| Future Volume（vph） | 145 | 475 | 75 | 245 | 550 | 630 | 130 | 830 | 255 | 310 | 605 | 120 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.2 | 3.6 | 3.7 | 3.2 | 3.6 | 3.7 | 3.0 | 3.4 | 4.0 | 3.0 | 3.7 | 3.3 |
| Storage Length（m） | 65.0 |  | 50.0 | 70.0 |  | 0.0 | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（m） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | ＊0．75 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor | 1.00 | 1.00 |  | 1.00 |  | 0.98 | 1.00 |  | 0.99 | 1.00 |  | 0.97 |
| Frt |  | 0.980 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1725 | 2740 | 0 | 1708 | 1881 | 1633 | 1685 | 3461 | 1670 | ＊2068 | 3544 | 1516 |
| Flt Permitted | 0.103 |  |  | 0.238 |  |  | 0.410 |  |  | 0.107 |  |  |
| Satd．Flow（perm） | 187 | 2740 | 0 | 427 | 1881 | 1608 | 724 | 3461 | 1648 | 186 | 3544 | 1470 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 12 |  |  |  | 309 |  |  | 262 |  |  | 126 |
| Link Speed（k／h） |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance（m） |  | 448.3 |  |  | 341.9 |  |  | 505.9 |  |  | 2054.7 |  |
| Travel Time（s） |  | 26.9 |  |  | 20.5 |  |  | 30.4 |  |  | 123.3 |  |
| Confl．Peds．（\＃／hr） | 2 |  | 3 | 3 |  | 2 | 5 |  | 1 | 1 |  | 5 |
| Confl．Bikes（\＃／hr） |  |  |  |  |  | 2 |  |  |  |  |  | 1 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles（\％） | 0\％ | 2\％ | 0\％ | 1\％ | 1\％ | 0\％ | 0\％ | 2\％ | 1\％ | 2\％ | 3\％ | 3\％ |
| Adj．Flow（vph） | 153 | 500 | 79 | 258 | 579 | 663 | 137 | 874 | 268 | 326 | 637 | 126 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 153 | 579 | 0 | 258 | 579 | 663 | 137 | 874 | 268 | 326 | 637 | 126 |
| Turn Type | pm＋pt | NA |  | pm＋pt | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split（s） | 11.0 | 45.0 |  | 11.0 | 45.0 | 45.0 | 39.5 | 39.5 | 39.5 | 11.0 | 39.5 | 39.5 |
| Total Split（s） | 13.0 | 48.0 |  | 13.0 | 48.0 | 48.0 | 41.0 | 41.0 | 41.0 | 18.0 | 59.0 | 59.0 |
| Total Split（\％） | 10．8\％ | 40．0\％ |  | 10．8\％ | 40．0\％ | 40．0\％ | 34．2\％ | 34．2\％ | 34．2\％ | 15．0\％ | 49．2\％ | 49．2\％ |
| Maximum Green（s） | 9.0 | 40.0 |  | 9.0 | 40.0 | 40.0 | 33.5 | 33.5 | 33.5 | 14.0 | 51.5 | 51.5 |
| Yellow Time（s） | 3.0 | 4.5 |  | 3.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 1.0 | 3.5 |  | 1.0 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 1.0 | 3.0 | 3.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 8.0 |  | 4.0 | 8.0 | 8.0 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None | None | C－Max | C－Max | C－Max | None | C－Max | C－Max |
| Walk Time（s） |  | 7.0 |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  | 30.0 |  |  | 30.0 | 30.0 | 25.0 | 25.0 | 25.0 |  | 25.0 | 25.0 |
| Pedestrian Calls（\＃／hr） |  | 5 |  |  | 5 | 5 | 5 | 5 | 5 |  | 5 | 5 |
| Act Effct Green（s） | 52.0 | 39.0 |  | 52.0 | 39.0 | 39.0 | 34.5 | 34.5 | 34.5 | 56.0 | 52.5 | 52.5 |


|  | 4 | $\rightarrow$ |  | $\dagger$ |  |  | 4 | $\dagger$ | \% |  | $\dagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Actuated g/C Ratio | 0.43 | 0.32 |  | 0.43 | 0.32 | 0.32 | 0.29 | 0.29 | 0.29 | 0.47 | 0.44 | 0.44 |
| v/c Ratio | 0.78 | 0.64 |  | 0.92 | 0.95 | 0.91 | 0.66 | 0.88 | 0.41 | 1.07 | 0.41 | 0.18 |
| Control Delay | 49.5 | 37.5 |  | 61.9 | 65.2 | 37.8 | 55.2 | 52.5 | 6.4 | 103.4 | 24.4 | 4.2 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 49.5 | 37.5 |  | 61.9 | 65.2 | 37.8 | 55.2 | 52.5 | 6.4 | 103.4 | 24.4 | 4.2 |
| LOS | D | D |  | E | E | D | E | D | A | F | C | A |
| Approach Delay |  | 40.0 |  |  | 52.5 |  |  | 43.1 |  |  | 45.7 |  |
| Approach LOS |  | D |  |  | D |  |  | D |  |  | D |  |
| Queue Length 50th (m) | 21.3 | 78.6 |  | 38.5 | 137.5 | 92.1 | 30.2 | 110.1 | 1.1 | ~72.8 | 56.8 | 0.0 |
| Queue Length 95th (m) | \#53.8 | 104.4 |  | \#82.5 | \#207.6 | \#170.0 | \#60.3 | \#147.3 | 21.5 | \#132.6 | 72.8 | 11.5 |
| Internal Link Dist (m) |  | 424.3 |  |  | 317.9 |  |  | 481.9 |  |  | 2030.7 |  |
| Turn Bay Length (m) | 65.0 |  |  | 70.0 |  |  | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Base Capacity (vph) | 196 | 921 |  | 281 | 627 | 742 | 208 | 994 | 659 | 306 | 1548 | 713 |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.78 | 0.63 |  | 0.92 | 0.92 | 0.89 | 0.66 | 0.88 | 0.41 | 1.07 | 0.41 | 0.18 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 39 (33\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 110 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.07 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: $46.3 \quad$ Intersection LOS: D |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 100.5\% ICU Level of Service G |  |  |  |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| * User Entered Value |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 210: Yonge Street \& St. John's Sideroad


| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | 4 | 「 | ${ }^{*}$ | 44 | 「 | ${ }^{7}$ | 中4 | 「 |
| Traffic Volume（vph） | 235 | 445 | 35 | 120 | 385 | 150 | 80 | 1025 | 165 | 75 | 660 | 75 |
| Future Volume（vph） | 235 | 445 | 35 | 120 | 385 | 150 | 80 | 1025 | 165 | 75 | 660 | 75 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.7 | 3.7 | 3.7 | 3.0 | 3.5 | 3.7 | 3.2 | 3.7 | 4.0 | 3.1 | 3.3 | 3.7 |
| Storage Length（m） | 30.0 |  | 0.0 | 50.0 |  | 50.0 | 60.0 |  | 60.0 | 60.0 |  | 60.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（m） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  |  |  |  |  | 0.99 |  |  |  |  |  |  |
| Frt |  | 0.989 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1807 | 1880 | 0 | 1636 | 1842 | 1633 | 1708 | 3579 | 1670 | 1655 | 3421 | 1617 |
| Flt Permitted | 0.198 |  |  | 0.470 |  |  | 0.390 |  |  | 0.098 |  |  |
| Satd．Flow（perm） | 377 | 1880 | 0 | 809 | 1842 | 1612 | 701 | 3579 | 1670 | 171 | 3421 | 1617 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 4 |  |  |  | 124 |  |  | 130 |  |  | 83 |
| Link Speed（k／h） |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance（m） |  | 129.9 |  |  | 1758.6 |  |  | 451.2 |  |  | 794.7 |  |
| Travel Time（s） |  | 7.8 |  |  | 105.5 |  |  | 23.2 |  |  | 40.9 |  |
| Confl．Bikes（\＃／hr） |  |  |  |  |  | 1 |  |  |  |  |  |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Heavy Vehicles（\％） | 1\％ | 1\％ | 2\％ | 3\％ | 2\％ | 0\％ | 1\％ | 2\％ | 1\％ | 3\％ | 2\％ | 1\％ |
| Adj．Flow（vph） | 245 | 464 | 36 | 125 | 401 | 156 | 83 | 1068 | 172 | 78 | 688 | 78 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 245 | 500 | 0 | 125 | 401 | 156 | 83 | 1068 | 172 | 78 | 688 | 78 |
| Turn Type | pm＋pt | NA |  | Perm | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | 4 |  |  | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 8 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 7.0 | 10.0 |  | 10.0 | 10.0 | 10.0 | 20.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 |
| Minimum Split（s） | 11.0 | 17.5 |  | 38.5 | 38.5 | 38.5 | 36.5 | 36.5 | 36.5 | 11.0 | 36.5 | 36.5 |
| Total Split（s） | 16.0 | 37.5 |  | 37.5 | 37.5 | 37.5 | 47.5 | 47.5 | 47.5 | 11.0 | 47.5 | 47.5 |
| Total Split（\％） | 14．3\％ | 33．5\％ |  | 33．5\％ | 33．5\％ | 33．5\％ | 42．4\％ | 42．4\％ | 42．4\％ | 9．8\％ | 42．4\％ | 42．4\％ |
| Maximum Green（s） | 12.0 | 30.0 |  | 30.0 | 30.0 | 30.0 | 40.0 | 40.0 | 40.0 | 7.0 | 40.0 | 40.0 |
| Yellow Time（s） | 3.0 | 4.5 |  | 4.5 | 4.5 | 4.5 | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 |
| All－Red Time（s） | 1.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 2.5 | 2.5 | 2.5 | 1.0 | 2.5 | 2.5 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 7.5 |  | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead |  |  | Lag | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes |  |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 6.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 |
| Recall Mode | None | None |  | None | None | None | Min | Min | Min | None | Min | Min |
| Walk Time（s） |  |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  |  |  | 24.0 | 24.0 | 24.0 | 22.0 | 22.0 | 22.0 |  | 22.0 | 22.0 |
| Pedestrian Calls（\＃／hr） |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Act Effct Green（s） | 46.1 | 42.5 |  | 26.4 | 26.4 | 26.4 | 38.2 | 38.2 | 38.2 | 50.1 | 46.5 | 46.5 |
| Actuated g／C Ratio | 0.44 | 0.41 |  | 0.25 | 0.25 | 0.25 | 0.37 | 0.37 | 0.37 | 0.48 | 0.45 | 0.45 |



Splits and Phases: 220: Bathurst Street \& 18th Sideroad/St. John's Sideroad



|  | 4 |  |  |  |  |  | 4 |  |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个t |  | 7 | $\uparrow$ | 「 | \％ | 个 $\uparrow$ | 「 | \％ | 性 | F |
| Traffic Volume（vph） | 181 | 511 | 83 | 264 | 615 | 697 | 153 | 890 | 272 | 340 | 651 | 138 |
| Future Volume（vph） | 181 | 511 | 83 | 264 | 615 | 697 | 153 | 890 | 272 | 340 | 651 | 138 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.2 | 3.6 | 3.7 | 3.2 | 3.6 | 3.7 | 3.0 | 3.4 | 4.0 | 3.0 | 3.7 | 3.3 |
| Storage Length（ m ） | 65.0 |  | 50.0 | 70.0 |  | 0.0 | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（m） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | ＊0．75 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor | 1.00 | 1.00 |  | 1.00 |  | 0.98 | 1.00 |  | 0.99 | 1.00 |  | 0.97 |
| Frt |  | 0.979 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1725 | 2737 | 0 | 1708 | 1881 | 1633 | 1685 | 3461 | 1670 | ＊2068 | 3544 | 1516 |
| Flt Permitted | 0.100 |  |  | 0.210 |  |  | 0.391 |  |  | 0.107 |  |  |
| Satd．Flow（perm） | 181 | 2737 | 0 | 377 | 1881 | 1608 | 691 | 3461 | 1648 | 186 | 3544 | 1470 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 12 |  |  |  | 295 |  |  | 245 |  |  | 145 |
| Link Speed（k／h） |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance（m） |  | 448.3 |  |  | 341.9 |  |  | 505.9 |  |  | 2054.7 |  |
| Travel Time（s） |  | 26.9 |  |  | 20.5 |  |  | 30.4 |  |  | 123.3 |  |
| Confl．Peds．（\＃／hr） | 2 |  | 3 | 3 |  | 2 | 5 |  | 1 | 1 |  | 5 |
| Confl．Bikes（\＃／hr） |  |  |  |  |  | 2 |  |  |  |  |  | 1 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles（\％） | 0\％ | 2\％ | 0\％ | 1\％ | 1\％ | 0\％ | 0\％ | 2\％ | 1\％ | 2\％ | 3\％ | 3\％ |
| Adj．Flow（vph） | 191 | 538 | 87 | 278 | 647 | 734 | 161 | 937 | 286 | 358 | 685 | 145 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 191 | 625 | 0 | 278 | 647 | 734 | 161 | 937 | 286 | 358 | 685 | 145 |
| Turn Type | pm＋pt | NA |  | pm＋pt | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | ， |  | 3 | 8 |  |  | ， |  | 5 |  |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split（s） | 11.0 | 45.0 |  | 11.0 | 45.0 | 45.0 | 39.5 | 39.5 | 39.5 | 11.0 | 39.5 | 39.5 |
| Total Split（s） | 13.0 | 48.0 |  | 13.0 | 48.0 | 48.0 | 41.0 | 41.0 | 41.0 | 18.0 | 59.0 | 59.0 |
| Total Split（\％） | 10．8\％ | 40．0\％ |  | 10．8\％ | 40．0\％ | 40．0\％ | 34．2\％ | 34．2\％ | 34．2\％ | 15．0\％ | 49．2\％ | 49．2\％ |
| Maximum Green（s） | 9.0 | 40.0 |  | 9.0 | 40.0 | 40.0 | 33.5 | 33.5 | 33.5 | 14.0 | 51.5 | 51.5 |
| Yellow Time（s） | 3.0 | 4.5 |  | 3.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 1.0 | 3.5 |  | 1.0 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 1.0 | 3.0 | 3.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 8.0 |  | 4.0 | 8.0 | 8.0 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None | None | C－Max | C－Max | C－Max | None | C－Max | C－Max |
| Walk Time（s） |  | 7.0 |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  | 30.0 |  |  | 30.0 | 30.0 | 25.0 | 25.0 | 25.0 |  | 25.0 | 25.0 |
| Pedestrian Calls（\＃／hr） |  | 5 |  |  | 5 | 5 | 5 | 5 | 5 |  | 5 | 5 |
| Act Effct Green（s） | 53.0 | 40.0 |  | 53.0 | 40.0 | 40.0 | 33.5 | 33.5 | 33.5 | 55.0 | 51.5 | 51.5 |



Splits and Phases: 210: Yonge Street \& St. John's Sideroad


|  | $\rangle$ |  |  |  |  |  | 4 | $\uparrow$ |  |  | $\dagger$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | \% | $\uparrow$ | 「 | \% | 个4 | \% | \% | ¢4 | F |
| Traffic Volume (vph) | 250 | 487 | 35 | 135 | 428 | 164 | 85 | 1105 | 200 | 82 | 670 | 120 |
| Future Volume (vph) | 250 | 487 | 35 | 135 | 428 | 164 | 85 | 1105 | 200 | 82 | 670 | 120 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.7 | 3.7 | 3.7 | 3.0 | 3.5 | 3.7 | 3.2 | 3.7 | 4.0 | 3.1 | 3.3 | 3.7 |
| Storage Length (m) | 30.0 |  | 0.0 | 50.0 |  | 50.0 | 60.0 |  | 60.0 | 60.0 |  | 60.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length ( m ) | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  |  |  |  |  | 0.99 |  |  |  |  |  |  |
| Frt |  | 0.990 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1807 | 1882 | 0 | 1636 | 1842 | 1633 | 1708 | 3579 | 1670 | 1655 | 3421 | 1617 |
| Flt Permitted | 0.148 |  |  | 0.396 |  |  | 0.386 |  |  | 0.092 |  |  |
| Satd. Flow (perm) | 282 | 1882 | 0 | 682 | 1842 | 1612 | 694 | 3579 | 1670 | 160 | 3421 | 1617 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 4 |  |  |  | 122 |  |  | 146 |  |  | 125 |
| Link Speed (kh) |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance (m) |  | 129.9 |  |  | 1758.6 |  |  | 451.2 |  |  | 794.7 |  |
| Travel Time (s) |  | 7.8 |  |  | 105.5 |  |  | 23.2 |  |  | 40.9 |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  | 1 |  |  |  |  |  |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Heavy Vehicles (\%) | 1\% | 1\% | 2\% | 3\% | 2\% | 0\% | 1\% | 2\% | 1\% | 3\% | 2\% | 1\% |
| Adj. Flow (vph) | 260 | 507 | 36 | 141 | 446 | 171 | 89 | 1151 | 208 | 85 | 698 | 125 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 260 | 543 | 0 | 141 | 446 | 171 | 89 | 1151 | 208 | 85 | 698 | 125 |
| Turn Type | pm+pt | NA |  | Perm | NA | Perm | Perm | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 7 | 4 |  |  | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 8 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 10.0 |  | 10.0 | 10.0 | 10.0 | 20.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 |
| Minimum Split (s) | 11.0 | 17.5 |  | 38.5 | 38.5 | 38.5 | 36.5 | 36.5 | 36.5 | 11.0 | 36.5 | 36.5 |
| Total Split (s) | 16.0 | 37.5 |  | 37.5 | 37.5 | 37.5 | 47.5 | 47.5 | 47.5 | 11.0 | 47.5 | 47.5 |
| Total Split (\%) | 14.3\% | 33.5\% |  | 33.5\% | 33.5\% | 33.5\% | 42.4\% | 42.4\% | 42.4\% | 9.8\% | 42.4\% | 42.4\% |
| Maximum Green (s) | 12.0 | 30.0 |  | 30.0 | 30.0 | 30.0 | 40.0 | 40.0 | 40.0 | 7.0 | 40.0 | 40.0 |
| Yellow Time (s) | 3.0 | 4.5 |  | 4.5 | 4.5 | 4.5 | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 |
| All-Red Time (s) | 1.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 2.5 | 2.5 | 2.5 | 1.0 | 2.5 | 2.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.0 | 7.5 |  | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead/Lag | Lead |  |  | Lag | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 6.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 |
| Recall Mode | None | None |  | None | None | None | Min | Min | Min | None | Min | Min |
| Walk Time (s) |  |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk (s) |  |  |  | 24.0 | 24.0 | 24.0 | 22.0 | 22.0 | 22.0 |  | 22.0 | 22.0 |
| Pedestrian Calls (\#/hr) |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Act Effct Green (s) | 48.0 | 44.5 |  | 28.4 | 28.4 | 28.4 | 39.6 | 39.6 | 39.6 | 51.6 | 48.1 | 48.1 |
| Actuated g/C Ratio | 0.45 | 0.41 |  | 0.26 | 0.26 | 0.26 | 0.37 | 0.37 | 0.37 | 0.48 | 0.45 | 0.45 |



Splits and Phases: 220: Bathurst Street \& 18th Sideroad/St. John's Sideroad



|  | 4 |  |  |  |  |  | 4 |  |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个t |  | \％ | $\uparrow$ | 「 | 7 | 个 $\uparrow$ | 「 | \％ | 性 | F |
| Traffic Volume（vph） | 191 | 536 | 88 | 274 | 670 | 742 | 163 | 930 | 287 | 350 | 666 | 148 |
| Future Volume（vph） | 191 | 536 | 88 | 274 | 670 | 742 | 163 | 930 | 287 | 350 | 666 | 148 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.2 | 3.6 | 3.7 | 3.2 | 3.6 | 3.7 | 3.0 | 3.4 | 4.0 | 3.0 | 3.7 | 3.3 |
| Storage Length（ m ） | 65.0 |  | 50.0 | 70.0 |  | 0.0 | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（m） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | ＊0．75 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  | 1.00 |  | 1.00 |  | 0.98 | 1.00 |  | 0.99 | 1.00 |  | 0.97 |
| Frt |  | 0.979 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1725 | 2737 | 0 | 1708 | 1881 | 1633 | 1685 | 3461 | 1670 | ＊2068 | 3544 | 1516 |
| Flt Permitted | 0.100 |  |  | 0.188 |  |  | 0.385 |  |  | 0.107 |  |  |
| Satd．Flow（perm） | 182 | 2737 | 0 | 338 | 1881 | 1608 | 680 | 3461 | 1648 | 186 | 3544 | 1470 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 12 |  |  |  | 292 |  |  | 236 |  |  | 156 |
| Link Speed（k／h） |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance（m） |  | 448.3 |  |  | 341.9 |  |  | 505.9 |  |  | 2054.7 |  |
| Travel Time（s） |  | 26.9 |  |  | 20.5 |  |  | 30.4 |  |  | 123.3 |  |
| Confl．Peds．（\＃／hr） | 2 |  | 3 | 3 |  | 2 | 5 |  | 1 | 1 |  | 5 |
| Confl．Bikes（\＃／hr） |  |  |  |  |  | 2 |  |  |  |  |  | 1 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles（\％） | 0\％ | 2\％ | 0\％ | 1\％ | 1\％ | 0\％ | 0\％ | 2\％ | 1\％ | 2\％ | 3\％ | 3\％ |
| Adj．Flow（vph） | 201 | 564 | 93 | 288 | 705 | 781 | 172 | 979 | 302 | 368 | 701 | 156 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 201 | 657 | 0 | 288 | 705 | 781 | 172 | 979 | 302 | 368 | 701 | 156 |
| Turn Type | pm＋pt | NA |  | pm＋pt | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | ， |  | 3 | 8 |  |  | ， |  | 5 |  |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split（s） | 11.0 | 45.0 |  | 11.0 | 45.0 | 45.0 | 39.5 | 39.5 | 39.5 | 11.0 | 39.5 | 39.5 |
| Total Split（s） | 13.0 | 48.0 |  | 13.0 | 48.0 | 48.0 | 41.0 | 41.0 | 41.0 | 18.0 | 59.0 | 59.0 |
| Total Split（\％） | 10．8\％ | 40．0\％ |  | 10．8\％ | 40．0\％ | 40．0\％ | 34．2\％ | 34．2\％ | 34．2\％ | 15．0\％ | 49．2\％ | 49．2\％ |
| Maximum Green（s） | 9.0 | 40.0 |  | 9.0 | 40.0 | 40.0 | 33.5 | 33.5 | 33.5 | 14.0 | 51.5 | 51.5 |
| Yellow Time（s） | 3.0 | 4.5 |  | 3.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 1.0 | 3.5 |  | 1.0 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 1.0 | 3.0 | 3.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 8.0 |  | 4.0 | 8.0 | 8.0 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None | None | C－Max | C－Max | C－Max | None | C－Max | C－Max |
| Walk Time（s） |  | 7.0 |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  | 30.0 |  |  | 30.0 | 30.0 | 25.0 | 25.0 | 25.0 |  | 25.0 | 25.0 |
| Pedestrian Calls（\＃／hr） |  | 5 |  |  | 5 | 5 | 5 | 5 | 5 |  | 5 | 5 |
| Act Effct Green（s） | 53.0 | 40.0 |  | 53.0 | 40.0 | 40.0 | 33.5 | 33.5 | 33.5 | 55.0 | 51.5 | 51.5 |


|  |  |  |  |  |  |  | 4 | 4 |  |  | $\dagger$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Actuated g/C Ratio | 0.44 | 0.33 |  | 0.44 | 0.33 | 0.33 | 0.28 | 0.28 | 0.28 | 0.46 | 0.43 | 0.43 |
| v/c Ratio | 1.03 | 0.71 |  | 1.14 | 1.12 | 1.07 | 0.91 | 1.01 | 0.48 | 1.21 | 0.46 | 0.22 |
| Control Delay | 99.1 | 39.5 |  | 126.1 | 112.9 | 78.5 | 88.7 | 75.4 | 11.4 | 153.0 | 25.6 | 4.0 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 99.1 | 39.5 |  | 126.1 | 112.9 | 78.5 | 88.7 | 75.4 | 11.4 | 153.0 | 25.6 | 4.0 |
| LOS | F | D |  | F | F | E | F | E | B | F | C | A |
| Approach Delay |  | 53.5 |  |  | 99.9 |  |  | 63.7 |  |  | 61.1 |  |
| Approach LOS |  | D |  |  | F |  |  | E |  |  | E |  |
| Queue Length 50th ( m ) | -35.4 | 92.9 |  | -50.4 | ~201.9 | -162.9 | 41.2 | ~131.0 | 12.3 | -94.8 | 63.8 | 0.0 |
| Queue Length 95th (m) | \#85.2 | 121.7 |  | \#108.0 | \#276.7 | \#241.1 | \#85.7 | \#176.9 | 38.0 | \#157.2 | 81.2 | 12.7 |
| Internal Link Dist (m) |  | 424.3 |  |  | 317.9 |  |  | 481.9 |  |  | 2030.7 |  |
| Turn Bay Length (m) | 65.0 |  |  | 70.0 |  |  | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Base Capacity (vph) | 196 | 920 |  | 252 | 627 | 730 | 189 | 966 | 630 | 304 | 1520 | 719 |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 1.03 | 0.71 |  | 1.14 | 1.12 | 1.07 | 0.91 | 1.01 | 0.48 | 1.21 | 0.46 | 0.22 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 39 (33\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.21 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 73.5 |  |  | Intersection LOS: E |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 111.5\% |  |  | ICU Level of Service H |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| * User Entered Value |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 210: Yonge Street \& St. John's Sideroad


|  | $\rangle$ |  |  | 7 |  |  | 4 | 4 | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | $\uparrow$ |  | \％ | $\uparrow$ | F | \％ | 个个 | F | \％ | 个个 | F |
| Traffic Volume（vph） | 265 | 512 | 35 | 145 | 468 | 179 | 95 | 1210 | 210 | 87 | 690 | 130 |
| Future Volume（vph） | 265 | 512 | 35 | 145 | 468 | 179 | 95 | 1210 | 210 | 87 | 690 | 130 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.7 | 3.7 | 3.7 | 3.0 | 3.5 | 3.7 | 3.2 | 3.7 | 4.0 | 3.1 | 3.3 | 3.7 |
| Storage Length（m） | 30.0 |  | 0.0 | 50.0 |  | 50.0 | 60.0 |  | 60.0 | 60.0 |  | 60.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ $m$ ） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  |  |  |  |  | 0.99 |  |  |  |  |  |  |
| Fit |  | 0.991 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1807 | 1884 | 0 | 1636 | 1842 | 1633 | 1708 | 3579 | 1670 | 1655 | 3421 | 1617 |
| Flt Permitted | 0.117 |  |  | 0.355 |  |  | 0.378 |  |  | 0.091 |  |  |
| Satd．Flow（perm） | 223 | 1884 | 0 | 611 | 1842 | 1612 | 679 | 3579 | 1670 | 159 | 3421 | 1617 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 4 |  |  |  | 122 |  |  | 140 |  |  | 135 |
| Link Speed（k／h） |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance（m） |  | 129.9 |  |  | 1758.6 |  |  | 451.2 |  |  | 794.7 |  |
| Travel Time（s） |  | 7.8 |  |  | 105.5 |  |  | 23.2 |  |  | 40.9 |  |
| Confl．Bikes（\＃／hr） |  |  |  |  |  | 1 |  |  |  |  |  |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Heavy Vehicles（\％） | 1\％ | 1\％ | 2\％ | 3\％ | 2\％ | 0\％ | 1\％ | 2\％ | 1\％ | 3\％ | 2\％ | 1\％ |
| Adj．Flow（vph） | 276 | 533 | 36 | 151 | 488 | 186 | 99 | 1260 | 219 | 91 | 719 | 135 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 276 | 569 | 0 | 151 | 488 | 186 | 99 | 1260 | 219 | 91 | 719 | 135 |
| Turn Type | pm＋pt | NA |  | Perm | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | 4 |  |  | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 8 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（ $s$ ） | 7.0 | 10.0 |  | 10.0 | 10.0 | 10.0 | 20.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 |
| Minimum Split（s） | 11.0 | 17.5 |  | 38.5 | 38.5 | 38.5 | 36.5 | 36.5 | 36.5 | 11.0 | 36.5 | 36.5 |
| Total Split（s） | 16.0 | 37.5 |  | 37.5 | 37.5 | 37.5 | 47.5 | 47.5 | 47.5 | 11.0 | 47.5 | 47.5 |
| Total Split（\％） | 14．3\％ | 33．5\％ |  | 33．5\％ | 33．5\％ | 33．5\％ | 42．4\％ | 42．4\％ | 42．4\％ | 9．8\％ | 42．4\％ | 42．4\％ |
| Maximum Green（s） | 12.0 | 30.0 |  | 30.0 | 30.0 | 30.0 | 40.0 | 40.0 | 40.0 | 7.0 | 40.0 | 40.0 |
| Yellow Time（s） | 3.0 | 4.5 |  | 4.5 | 4.5 | 4.5 | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 |
| All－Red Time（s） | 1.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 2.5 | 2.5 | 2.5 | 1.0 | 2.5 | 2.5 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 7.5 |  | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead |  |  | Lag | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes |  |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 6.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 |
| Recall Mode | None | None |  | None | None | None | Min | Min | Min | None | Min | Min |
| Walk Time（s） |  |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  |  |  | 24.0 | 24.0 | 24.0 | 22.0 | 22.0 | 22.0 |  | 22.0 | 22.0 |
| Pedestrian Calls（\＃／hr） |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Act Effct Green（s） | 49.6 | 46.1 |  | 30.1 | 30.1 | 30.1 | 40.1 | 40.1 | 40.1 | 52.2 | 48.7 | 48.7 |
| Actuated g／C Ratio | 0.45 | 0.42 |  | 0.27 | 0.27 | 0.27 | 0.37 | 0.37 | 0.37 | 0.48 | 0.44 | 0.44 |



Splits and Phases: 220: Bathurst Street \& 18th Sideroad/St. John's Sideroad



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | 个t |  | ＊ | $\uparrow$ | 7 | \％ | 个个 | F＇ | ${ }^{7}$ | 个 $\uparrow$ | F |
| Traffic Volume（vph） | 199 | 533 | 98 | 259 | 664 | 697 | 176 | 889 | 271 | 340 | 648 | 159 |
| Future Volume（vph） | 199 | 533 | 98 | 259 | 664 | 697 | 176 | 889 | 271 | 340 | 648 | 159 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.2 | 3.6 | 3.7 | 3.2 | 3.6 | 3.7 | 3.0 | 3.4 | 4.0 | 3.0 | 3.7 | 3.3 |
| Storage Length（m） | 65.0 |  | 50.0 | 70.0 |  | 0.0 | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（m） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | ＊0．75 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  | 1.00 |  | 1.00 |  | 0.98 | 1.00 |  | 0.99 | 1.00 |  | 0.97 |
| Frt |  | 0.977 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1725 | 2732 | 0 | 1708 | 1881 | 1633 | 1685 | 3461 | 1670 | ＊2068 | 3544 | 1516 |
| Flt Permitted | 0.100 |  |  | 0.184 |  |  | 0.392 |  |  | 0.107 |  |  |
| Satd．Flow（perm） | 182 | 2732 | 0 | 330 | 1881 | 1608 | 693 | 3461 | 1648 | 186 | 3544 | 1470 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 14 |  |  |  | 292 |  |  | 238 |  |  | 167 |
| Link Speed（k／h） |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance（m） |  | 448.3 |  |  | 341.9 |  |  | 505.9 |  |  | 608.7 |  |
| Travel Time（s） |  | 26.9 |  |  | 20.5 |  |  | 30.4 |  |  | 36.5 |  |
| Confl．Peds．（\＃／hr） | 2 |  | 3 | 3 |  | 2 | 5 |  | 1 | 1 |  | 5 |
| Confl．Bikes（\＃／hr） |  |  |  |  |  | 2 |  |  |  |  |  | 1 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles（\％） | 0\％ | 2\％ | 0\％ | 1\％ | 1\％ | 0\％ | 0\％ | 2\％ | 1\％ | 2\％ | 3\％ | 3\％ |
| Adj．Flow（vph） | 209 | 561 | 103 | 273 | 699 | 734 | 185 | 936 | 285 | 358 | 682 | 167 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 209 | 664 | 0 | 273 | 699 | 734 | 185 | 936 | 285 | 358 | 682 | 167 |
| Turn Type | pm＋pt | NA |  | pm＋pt | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split（s） | 11.0 | 45.0 |  | 11.0 | 45.0 | 45.0 | 39.5 | 39.5 | 39.5 | 11.0 | 39.5 | 39.5 |
| Total Split（s） | 13.0 | 48.0 |  | 13.0 | 48.0 | 48.0 | 41.0 | 41.0 | 41.0 | 18.0 | 59.0 | 59.0 |
| Total Split（\％） | 10．8\％ | 40．0\％ |  | 10．8\％ | 40．0\％ | 40．0\％ | 34．2\％ | 34．2\％ | 34．2\％ | 15．0\％ | 49．2\％ | 49．2\％ |
| Maximum Green（s） | 9.0 | 40.0 |  | 9.0 | 40.0 | 40.0 | 33.5 | 33.5 | 33.5 | 14.0 | 51.5 | 51.5 |
| Yellow Time（s） | 3.0 | 4.5 |  | 3.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 1.0 | 3.5 |  | 1.0 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 1.0 | 3.0 | 3.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 8.0 |  | 4.0 | 8.0 | 8.0 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None | None | C－Max | C－Max | C－Max | None | C－Max | C－Max |
| Walk Time（s） |  | 7.0 |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  | 30.0 |  |  | 30.0 | 30.0 | 25.0 | 25.0 | 25.0 |  | 25.0 | 25.0 |
| Pedestrian Calls（\＃／hr） |  | 5 |  |  | 5 | 5 | 5 | 5 | 5 |  | 5 | 5 |
| Act Effct Green（s） | 53.0 | 40.0 |  | 53.0 | 40.0 | 40.0 | 33.5 | 33.5 | 33.5 | 55.0 | 51.5 | 51.5 |



Splits and Phases: 210: Yonge Street \& St. John's Sideroad


|  | 4 | $\rightarrow$ |  | 7 |  | 4 | 4 |  | 7 | ( | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1 /}$ | $\uparrow$ |  | ${ }^{7}$ | 4 | F' | ${ }^{1}$ | 44 | F' | ${ }^{7}$ | 44 | 「 |
| Traffic Volume (vph) | 250 | 517 | 35 | 140 | 439 | 172 | 85 | 1105 | 229 | 96 | 670 | 120 |
| Future Volume (vph) | 250 | 517 | 35 | 140 | 439 | 172 | 85 | 1105 | 229 | 96 | 670 | 120 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.7 | 3.7 | 3.7 | 3.0 | 3.5 | 3.7 | 3.2 | 3.7 | 4.0 | 3.1 | 3.3 | 3.7 |
| Storage Length (m) | 30.0 |  | 0.0 | 50.0 |  | 50.0 | 60.0 |  | 60.0 | 60.0 |  | 60.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length (m) | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  |  |  |  |  | 0.99 |  |  |  |  |  |  |
| Frt |  | 0.991 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1807 | 1884 | 0 | 1636 | 1842 | 1633 | 1708 | 3579 | 1670 | 1655 | 3421 | 1617 |
| Flt Permitted | 0.135 |  |  | 0.334 |  |  | 0.386 |  |  | 0.091 |  |  |
| Satd. Flow (perm) | 257 | 1884 | 0 | 575 | 1842 | 1612 | 694 | 3579 | 1670 | 159 | 3421 | 1617 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 4 |  |  |  | 125 |  |  | 168 |  |  | 125 |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance (m) |  | 129.9 |  |  | 1758.6 |  |  | 451.2 |  |  | 794.7 |  |
| Travel Time (s) |  | 7.8 |  |  | 105.5 |  |  | 23.2 |  |  | 40.9 |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  | 1 |  |  |  |  |  |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Heavy Vehicles (\%) | 1\% | 1\% | 2\% | 3\% | 2\% | 0\% | 1\% | 2\% | 1\% | 3\% | 2\% | 1\% |
| Adj. Flow (vph) | 260 | 539 | 36 | 146 | 457 | 179 | 89 | 1151 | 239 | 100 | 698 | 125 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 260 | 575 | 0 | 146 | 457 | 179 | 89 | 1151 | 239 | 100 | 698 | 125 |
| Turn Type | pm+pt | NA |  | Perm | NA | Perm | Perm | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 7 | 4 |  |  | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 8 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 10.0 |  | 10.0 | 10.0 | 10.0 | 20.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 |
| Minimum Split (s) | 11.0 | 17.5 |  | 38.5 | 38.5 | 38.5 | 36.5 | 36.5 | 36.5 | 11.0 | 36.5 | 36.5 |
| Total Split (s) | 16.0 | 37.5 |  | 37.5 | 37.5 | 37.5 | 47.5 | 47.5 | 47.5 | 11.0 | 47.5 | 47.5 |
| Total Split (\%) | 14.3\% | 33.5\% |  | 33.5\% | 33.5\% | 33.5\% | 42.4\% | 42.4\% | 42.4\% | 9.8\% | 42.4\% | 42.4\% |
| Maximum Green (s) | 12.0 | 30.0 |  | 30.0 | 30.0 | 30.0 | 40.0 | 40.0 | 40.0 | 7.0 | 40.0 | 40.0 |
| Yellow Time (s) | 3.0 | 4.5 |  | 4.5 | 4.5 | 4.5 | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 |
| All-Red Time (s) | 1.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 2.5 | 2.5 | 2.5 | 1.0 | 2.5 | 2.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.0 | 7.5 |  | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead/Lag | Lead |  |  | Lag | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 6.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 |
| Recall Mode | None | None |  | None | None | None | Min | Min | Min | None | Min | Min |
| Walk Time (s) |  |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk (s) |  |  |  | 24.0 | 24.0 | 24.0 | 22.0 | 22.0 | 22.0 |  | 22.0 | 22.0 |
| Pedestrian Calls (\#/hr) |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Act Effct Green (s) | 48.9 | 45.4 |  | 29.4 | 29.4 | 29.4 | 40.0 | 40.0 | 40.0 | 54.5 | 51.0 | 51.0 |
| Actuated g/C Ratio | 0.44 | 0.41 |  | 0.26 | 0.26 | 0.26 | 0.36 | 0.36 | 0.36 | 0.49 | 0.46 | 0.46 |



Splits and Phases: 220: Bathurst Street \& 18th Sideroad/St. John's Sideroad



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ＊ | 个t |  | \％ | $\uparrow$ | 「 | ${ }^{7}$ | 个4 | F＇ | \％ | 个个 | F |
| Traffic Volume（vph） | 214 | 573 | 118 | 269 | 719 | 742 | 181 | 927 | 283 | 350 | 663 | 169 |
| Future Volume（vph） | 214 | 573 | 118 | 269 | 719 | 742 | 181 | 927 | 283 | 350 | 663 | 169 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.2 | 3.6 | 3.7 | 3.2 | 3.6 | 3.7 | 3.0 | 3.4 | 4.0 | 3.0 | 3.7 | 3.3 |
| Storage Length（m） | 65.0 |  | 50.0 | 70.0 |  | 0.0 | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ m ） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | ＊0．75 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  | 1.00 |  | 1.00 |  | 0.98 | 1.00 |  | 0.99 | 1.00 |  | 0.97 |
| Frt |  | 0.974 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1725 | 2724 | 0 | 1708 | 1881 | 1633 | 1685 | 3461 | 1670 | ＊2068 | 3544 | 1516 |
| Flt Permitted | 0.100 |  |  | 0.144 |  |  | 0.386 |  |  | 0.107 |  |  |
| Satd．Flow（perm） | 182 | 2724 | 0 | 259 | 1881 | 1608 | 682 | 3461 | 1648 | 186 | 3544 | 1470 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 15 |  |  |  | 288 |  |  | 226 |  |  | 178 |
| Link Speed（k／h） |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance（m） |  | 448.3 |  |  | 341.9 |  |  | 505.9 |  |  | 608.7 |  |
| Travel Time（s） |  | 26.9 |  |  | 20.5 |  |  | 30.4 |  |  | 36.5 |  |
| Confl．Peds．（\＃／hr） | 2 |  | 3 | 3 |  | 2 | 5 |  | 1 | 1 |  | 5 |
| Confl．Bikes（\＃／hr） |  |  |  |  |  | 2 |  |  |  |  |  | 1 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles（\％） | 0\％ | 2\％ | 0\％ | 1\％ | 1\％ | 0\％ | 0\％ | 2\％ | 1\％ | 2\％ | 3\％ | 3\％ |
| Adj．Flow（vph） | 225 | 603 | 124 | 283 | 757 | 781 | 191 | 976 | 298 | 368 | 698 | 178 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 225 | 727 | 0 | 283 | 757 | 781 | 191 | 976 | 298 | 368 | 698 | 178 |
| Turn Type | pm＋pt | NA |  | pm＋pt | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split（s） | 11.0 | 45.0 |  | 11.0 | 45.0 | 45.0 | 39.5 | 39.5 | 39.5 | 11.0 | 39.5 | 39.5 |
| Total Split（s） | 13.0 | 48.0 |  | 13.0 | 48.0 | 48.0 | 41.0 | 41.0 | 41.0 | 18.0 | 59.0 | 59.0 |
| Total Split（\％） | 10．8\％ | 40．0\％ |  | 10．8\％ | 40．0\％ | 40．0\％ | 34．2\％ | 34．2\％ | 34．2\％ | 15．0\％ | 49．2\％ | 49．2\％ |
| Maximum Green（s） | 9.0 | 40.0 |  | 9.0 | 40.0 | 40.0 | 33.5 | 33.5 | 33.5 | 14.0 | 51.5 | 51.5 |
| Yellow Time（s） | 3.0 | 4.5 |  | 3.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 1.0 | 3.5 |  | 1.0 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 1.0 | 3.0 | 3.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 8.0 |  | 4.0 | 8.0 | 8.0 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None | None | C－Max | C－Max | C－Max | None | C－Max | C－Max |
| Walk Time（s） |  | 7.0 |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  | 30.0 |  |  | 30.0 | 30.0 | 25.0 | 25.0 | 25.0 |  | 25.0 | 25.0 |
| Pedestrian Calls（\＃／hr） |  | 5 |  |  | 5 | 5 | 5 | 5 | 5 |  | 5 | 5 |
| Act Effct Green（s） | 53.0 | 40.0 |  | 53.0 | 40.0 | 40.0 | 33.5 | 33.5 | 33.5 | 55.0 | 51.5 | 51.5 |



Splits and Phases: 210: Yonge Street \& St. John's Sideroad


|  | 4 | $\rightarrow$ |  | 7 |  | 4 | 4 |  | 7 | ( | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | 4 | F | ${ }^{1 /}$ | 44 | F' | ${ }^{7}$ | 44 | 「 |
| Traffic Volume (vph) | 265 | 542 | 35 | 158 | 485 | 192 | 95 | 1210 | 239 | 101 | 690 | 130 |
| Future Volume (vph) | 265 | 542 | 35 | 158 | 485 | 192 | 95 | 1210 | 239 | 101 | 690 | 130 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.7 | 3.7 | 3.7 | 3.0 | 3.5 | 3.7 | 3.2 | 3.7 | 4.0 | 3.1 | 3.3 | 3.7 |
| Storage Length (m) | 30.0 |  | 0.0 | 50.0 |  | 50.0 | 60.0 |  | 60.0 | 60.0 |  | 60.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length (m) | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  |  |  |  |  | 0.99 |  |  |  |  |  |  |
| Frt |  | 0.991 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1807 | 1884 | 0 | 1636 | 1842 | 1633 | 1708 | 3579 | 1670 | 1655 | 3421 | 1617 |
| Flt Permitted | 0.118 |  |  | 0.298 |  |  | 0.378 |  |  | 0.091 |  |  |
| Satd. Flow (perm) | 224 | 1884 | 0 | 513 | 1842 | 1612 | 679 | 3579 | 1670 | 159 | 3421 | 1617 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 3 |  |  |  | 126 |  |  | 160 |  |  | 135 |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance (m) |  | 129.9 |  |  | 1758.6 |  |  | 451.2 |  |  | 794.7 |  |
| Travel Time (s) |  | 7.8 |  |  | 105.5 |  |  | 23.2 |  |  | 40.9 |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  | 1 |  |  |  |  |  |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Heavy Vehicles (\%) | 1\% | 1\% | 2\% | 3\% | 2\% | 0\% | 1\% | 2\% | 1\% | 3\% | 2\% | 1\% |
| Adj. Flow (vph) | 276 | 565 | 36 | 165 | 505 | 200 | 99 | 1260 | 249 | 105 | 719 | 135 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 276 | 601 | 0 | 165 | 505 | 200 | 99 | 1260 | 249 | 105 | 719 | 135 |
| Turn Type | pm+pt | NA |  | Perm | NA | Perm | Perm | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 7 | 4 |  |  | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 8 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 10.0 |  | 10.0 | 10.0 | 10.0 | 20.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 |
| Minimum Split (s) | 11.0 | 17.5 |  | 38.5 | 38.5 | 38.5 | 36.5 | 36.5 | 36.5 | 11.0 | 36.5 | 36.5 |
| Total Split (s) | 16.0 | 37.5 |  | 37.5 | 37.5 | 37.5 | 47.5 | 47.5 | 47.5 | 11.0 | 47.5 | 47.5 |
| Total Split (\%) | 14.3\% | 33.5\% |  | 33.5\% | 33.5\% | 33.5\% | 42.4\% | 42.4\% | 42.4\% | 9.8\% | 42.4\% | 42.4\% |
| Maximum Green (s) | 12.0 | 30.0 |  | 30.0 | 30.0 | 30.0 | 40.0 | 40.0 | 40.0 | 7.0 | 40.0 | 40.0 |
| Yellow Time (s) | 3.0 | 4.5 |  | 4.5 | 4.5 | 4.5 | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 |
| All-Red Time (s) | 1.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 2.5 | 2.5 | 2.5 | 1.0 | 2.5 | 2.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.0 | 7.5 |  | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead/Lag | Lead |  |  | Lag | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 6.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 |
| Recall Mode | None | None |  | None | None | None | Min | Min | Min | None | Min | Min |
| Walk Time (s) |  |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk (s) |  |  |  | 24.0 | 24.0 | 24.0 | 22.0 | 22.0 | 22.0 |  | 22.0 | 22.0 |
| Pedestrian Calls (\#/hr) |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Act Effct Green (s) | 49.5 | 46.0 |  | 30.0 | 30.0 | 30.0 | 40.0 | 40.0 | 40.0 | 54.5 | 51.0 | 51.0 |
| Actuated g/C Ratio | 0.44 | 0.41 |  | 0.27 | 0.27 | 0.27 | 0.36 | 0.36 | 0.36 | 0.49 | 0.46 | 0.46 |



Splits and Phases: 220: Bathurst Street \& 18th Sideroad/St. John's Sideroad


|  | 4 |  |  | 7 |  | 4 |  | 4 | $>$ |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\uparrow$ | 7 | \% | $\uparrow$ | 「 |  | ¢ |  | \% | F |  |
| Traffic Volume (veh/h) | 80 | 762 | 6 | 60 | 915 | 94 | 5 | 3 | 46 | 98 | 3 | 50 |
| Future Volume (Veh/h) | 80 | 762 | 6 | 60 | 915 | 94 | 5 | 3 | 46 | 98 | 3 | 50 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Hourly flow rate (vph) | 90 | 856 | 7 | 67 | 1028 | 106 | 6 | 3 | 52 | 110 | 3 | 56 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (m/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  | None |  |  | None |  |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal ( $m$ ) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| VC , conflicting volume | 1134 |  |  | 863 |  |  | 2256 | 2304 | 856 | 2252 | 2205 | 1028 |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu, unblocked vol | 1134 |  |  | 863 |  |  | 2256 | 2304 | 856 | 2252 | 2205 | 1028 |
| tC , single (s) | 4.1 |  |  | 4.1 |  |  | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 2.2 |  |  | 2.2 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free \% | 86 |  |  | 91 |  |  | 68 | 90 | 86 | 0 | 91 | 80 |
| cM capacity (veh/h) | 623 |  |  | 788 |  |  | 19 | 31 | 360 | 20 | 35 | 287 |
| Direction, Lane \# | EB 1 | EB 2 | EB 3 | WB 1 | WB 2 | WB 3 | NB 1 | SB 1 | SB 2 |  |  |  |
| Volume Total | 90 | 856 | 7 | 67 | 1028 | 106 | 61 | 110 | 59 |  |  |  |
| Volume Left | 90 | 0 | 0 | 67 | 0 | 0 | 6 | 110 | 0 |  |  |  |
| Volume Right | 0 | 0 | 7 | 0 | 0 | 106 | 52 | 0 | 56 |  |  |  |
| cSH | 623 | 1700 | 1700 | 788 | 1700 | 1700 | 108 | 20 | 210 |  |  |  |
| Volume to Capacity | 0.14 | 0.50 | 0.00 | 0.09 | 0.60 | 0.06 | 0.56 | 5.57 | 0.28 |  |  |  |
| Queue Length 95th ( m ) | 4.0 | 0.0 | 0.0 | 2.2 | 0.0 | 0.0 | 21.4 | Err | 8.8 |  |  |  |
| Control Delay (s) | 11.7 | 0.0 | 0.0 | 10.0 | 0.0 | 0.0 | 74.7 | Err | 28.6 |  |  |  |
| Lane LOS | B |  |  | A |  |  | F | F | D |  |  |  |
| Approach Delay (s) | 1.1 |  |  | 0.6 |  |  | 74.7 | 6518.2 |  |  |  |  |
| Approach LOS |  |  |  |  |  |  | F | F |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 464.7 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 74.7\% |  | CU Level | f Service |  |  | D |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |


|  | 4 | $\rightarrow$ | 7 | 7 |  |  | 4 |  | 7 | $V$ |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1}$ | 中 ${ }^{\text {a }}$ |  | ${ }^{1}$ | 4 | F | ${ }^{7}$ | 44 | 「 | ${ }^{7}$ | 44 | 「 |
| Traffic Volume（vph） | 116 | 677 | 169 | 188 | 452 | 281 | 73 | 500 | 253 | 538 | 757 | 168 |
| Future Volume（vph） | 116 | 677 | 169 | 188 | 452 | 281 | 73 | 500 | 253 | 538 | 757 | 168 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.2 | 3.6 | 3.7 | 3.2 | 3.6 | 3.7 | 3.0 | 3.4 | 4.0 | 3.0 | 3.7 | 3.3 |
| Storage Length（m） | 65.0 |  | 50.0 | 70.0 |  | 0.0 | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（m） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | ＊0．75 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  | 1.00 |  |  |  |  | 1.00 |  |  |  |  | 0.97 |
| Frt |  | 0.970 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1612 | 2703 | 0 | 1708 | 1845 | 1512 | 1652 | 3330 | 1670 | ＊2068 | 3444 | 1516 |
| Flt Permitted | 0.167 |  |  | 0.098 |  |  | 0.332 |  |  | 0.197 |  |  |
| Satd．Flow（perm） | 283 | 2703 | 0 | 176 | 1845 | 1512 | 576 | 3330 | 1670 | 336 | 3444 | 1473 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 17 |  |  |  | 277 |  |  | 154 |  |  | 189 |
| Link Speed（k／h） |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance（m） |  | 448.3 |  |  | 341.9 |  |  | 505.9 |  |  | 2054.7 |  |
| Travel Time（s） |  | 26.9 |  |  | 20.5 |  |  | 30.4 |  |  | 123.3 |  |
| Confl．Peds．（\＃／hr） |  |  | 2 | 2 |  |  | 4 |  |  |  |  | 4 |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles（\％） | 7\％ | 2\％ | 2\％ | 1\％ | 3\％ | 8\％ | 2\％ | 6\％ | 1\％ | 4\％ | 6\％ | 3\％ |
| Adj．Flow（vph） | 130 | 761 | 190 | 211 | 508 | 316 | 82 | 562 | 284 | 604 | 851 | 189 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 130 | 951 | 0 | 211 | 508 | 316 | 82 | 562 | 284 | 604 | 851 | 189 |
| Turn Type | pm＋pt | NA |  | pm＋pt | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split（s） | 11.0 | 45.0 |  | 11.0 | 45.0 | 45.0 | 39.5 | 39.5 | 39.5 | 11.0 | 39.5 | 39.5 |
| Total Split（s） | 12.0 | 48.0 |  | 13.0 | 49.0 | 49.0 | 34.0 | 34.0 | 34.0 | 35.0 | 69.0 | 69.0 |
| Total Split（\％） | 9．2\％ | 36．9\％ |  | 10．0\％ | 37．7\％ | 37．7\％ | 26．2\％ | 26．2\％ | 26．2\％ | 26．9\％ | 53．1\％ | 53．1\％ |
| Maximum Green（s） | 8.0 | 40.0 |  | 9.0 | 41.0 | 41.0 | 26.5 | 26.5 | 26.5 | 31.0 | 61.5 | 61.5 |
| Yellow Time（s） | 3.0 | 4.5 |  | 3.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 1.0 | 3.5 |  | 1.0 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 1.0 | 3.0 | 3.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 8.0 |  | 4.0 | 8.0 | 8.0 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None | None | C－Max | C－Max | C－Max | None | C－Max | C－Max |
| Walk Time（s） |  | 7.0 |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  | 30.0 |  |  | 30.0 | 30.0 | 25.0 | 25.0 | 25.0 |  | 25.0 | 25.0 |
| Pedestrian Calls（\＃／hr） |  | 0 |  |  | 0 | 0 | 5 | 5 | 5 |  | 5 | 5 |
| Act Effct Green（s） | 52.0 | 40.0 |  | 54.0 | 41.0 | 41.0 | 26.5 | 26.5 | 26.5 | 65.0 | 61.5 | 61.5 |
| Actuated g／C Ratio | 0.40 | 0.31 |  | 0.42 | 0.32 | 0.32 | 0.20 | 0.20 | 0.20 | 0.50 | 0.47 | 0.47 |


|  | 4 |  |  |  |  | 4 | 4 | $\dagger$ | \% |  | $\dagger$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.67 | 1.13 |  | 1.18 | 0.87 | 0.47 | 0.70 | 0.83 | 0.61 | 1.04 | 0.52 | 0.24 |
| Control Delay | 41.5 | 113.2 |  | 151.7 | 59.3 | 8.5 | 79.5 | 61.1 | 27.3 | 80.9 | 13.0 | 0.8 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 41.5 | 113.2 |  | 151.7 | 59.3 | 8.5 | 79.5 | 61.1 | 27.3 | 80.9 | 13.0 | 0.8 |
| LOS | D | F |  | F | E | A | E | E | C | F | B | A |
| Approach Delay |  | 104.6 |  |  | 62.7 |  |  | 52.4 |  |  | 36.6 |  |
| Approach LOS |  | F |  |  | E |  |  | D |  |  | D |  |
| Queue Length 50th (m) | 21.1 | ~196.0 |  | ~50.7 | 129.4 | 7.4 | 20.7 | 77.1 | 31.5 | ~143.4 | 34.3 | 0.1 |
| Queue Length 95th (m) | \#37.6 | \#246.4 |  | \#101.4 | \#187.7 | 30.9 | \#46.7 | \#98.8 | 61.8 m | \#210.0 | m40.1 | m0.6 |
| Internal Link Dist (m) |  | 424.3 |  |  | 317.9 |  |  | 481.9 |  |  | 2030.7 |  |
| Turn Bay Length (m) | 65.0 |  |  | 70.0 |  |  | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Base Capacity (vph) | 194 | 843 |  | 179 | 581 | 666 | 117 | 678 | 463 | 581 | 1629 | 796 |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.67 | 1.13 |  | 1.18 | 0.87 | 0.47 | 0.70 | 0.83 | 0.61 | 1.04 | 0.52 | 0.24 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 35 (27\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 150 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.18 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 61.1 Intersection LOS: E |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 98.2\% ICU Level of Service F |  |  |  |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| * User Entered Value |  |  |  |  |  |  |  |  |  |  |  |  |
| $\sim$ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| $m$ Volume for 95th percentile queue is metered by upstream signal. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 210: Yonge Street \& St. John's Sideroad


|  | $\stackrel{ }{*}$ |  |  | $\checkmark$ |  |  | 4 | $\dagger$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | $\hat{+}$ |  | \％ | $\uparrow$ | 「 | ${ }^{*}$ | 个个 | ${ }^{7}$ | ${ }_{1}$ | ¢4 | 「 |
| Traffic Volume（vph） | 90 | 419 | 50 | 158 | 457 | 43 | 50 | 600 | 61 | 151 | 1100 | 280 |
| Future Volume（vph） | 90 | 419 | 50 | 158 | 457 | 43 | 50 | 600 | 61 | 151 | 1100 | 280 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.7 | 3.7 | 3.7 | 3.0 | 3.5 | 3.7 | 3.2 | 3.7 | 4.0 | 3.1 | 3.3 | 3.7 |
| Storage Length（m） | 30.0 |  | 0.0 | 50.0 |  | 50.0 | 60.0 |  | 60.0 | 60.0 |  | 60.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ m ） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  | 1.00 |  |  |  |  |  |  |  |  |  |  |
| Frt |  | 0.984 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1738 | 1819 | 0 | 1668 | 1807 | 1601 | 1675 | 3510 | 1622 | 1688 | 3388 | 1617 |
| Flt Permitted | 0.445 |  |  | 0.157 |  |  | 0.169 |  |  | 0.279 |  |  |
| Satd．Flow（perm） | 814 | 1819 | 0 | 276 | 1807 | 1601 | 298 | 3510 | 1622 | 496 | 3388 | 1617 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 6 |  |  |  | 87 |  |  | 127 |  |  | 211 |
| Link Speed（k／h） |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance（m） |  | 129.9 |  |  | 1758.6 |  |  | 451.2 |  |  | 794.7 |  |
| Travel Time（s） |  | 7.8 |  |  | 105.5 |  |  | 23.2 |  |  | 40.9 |  |
| Confl．Bikes（\＃／hr） |  |  | 1 |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles（\％） | 5\％ | 4\％ | 2\％ | 1\％ | 4\％ | 2\％ | 3\％ | 4\％ | 4\％ | 1\％ | 3\％ | 1\％ |
| Adj．Flow（vph） | 95 | 441 | 53 | 166 | 481 | 45 | 53 | 632 | 64 | 159 | 1158 | 295 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 95 | 494 | 0 | 166 | 481 | 45 | 53 | 632 | 64 | 159 | 1158 | 295 |
| Turn Type | Perm | NA |  | pm＋pt | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases |  | 4 |  | 3 | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 4 | 4 |  | 3 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 10.0 | 10.0 |  | 7.0 | 10.0 | 10.0 | 20.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 |
| Minimum Split（s） | 17.5 | 17.5 |  | 11.0 | 38.5 | 38.5 | 36.5 | 36.5 | 36.5 | 11.0 | 36.5 | 36.5 |
| Total Split（s） | 37.5 | 37.5 |  | 11.0 | 37.5 | 37.5 | 47.5 | 47.5 | 47.5 | 11.0 | 47.5 | 47.5 |
| Total Split（\％） | 35．0\％ | 35．0\％ |  | 10．3\％ | 35．0\％ | 35．0\％ | 44．4\％ | 44．4\％ | 44．4\％ | 10．3\％ | 44．4\％ | 44．4\％ |
| Maximum Green（s） | 30.0 | 30.0 |  | 7.0 | 30.0 | 30.0 | 40.0 | 40.0 | 40.0 | 7.0 | 40.0 | 40.0 |
| Yellow Time（s） | 4.5 | 4.5 |  | 3.0 | 4.5 | 4.5 | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 |
| All－Red Time（s） | 3.0 | 3.0 |  | 1.0 | 3.0 | 3.0 | 2.5 | 2.5 | 2.5 | 1.0 | 2.5 | 2.5 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 7.5 | 7.5 |  | 4.0 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lag | Lag |  | Lead |  |  | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes |  |  | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 6.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 |
| Recall Mode | None | None |  | None | None | None | Min | Min | Min | None | Min | Min |
| Walk Time（s） |  |  |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  |  |  |  | 24.0 | 24.0 | 22.0 | 22.0 | 22.0 |  | 22.0 | 22.0 |
| Pedestrian Calls（\＃／hr） |  |  |  |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Act Effct Green（s） | 29.3 | 29.3 |  | 43.9 | 40.4 | 40.4 | 31.8 | 31.8 | 31.8 | 46.4 | 42.9 | 42.9 |
| Actuated g／C Ratio | 0.30 | 0.30 |  | 0.45 | 0.41 | 0.41 | 0.32 | 0.32 | 0.32 | 0.47 | 0.44 | 0.44 |



Splits and Phases: 220: Bathurst Street \& 18th Sideroad/St. John's Sideroad


|  | 4 | $\rightarrow$ |  | $\checkmark$ |  |  | 4 | $\dagger$ | $p$ | （ | $\dagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1}$ | 中 ${ }^{\text {a }}$ |  | ${ }^{1}$ | 4 | 「 | ${ }^{7}$ | 44 | 「 | ${ }^{7}$ | 中4 | 「 |
| Traffic Volume（vph） | 121 | 737 | 179 | 198 | 477 | 291 | 78 | 510 | 268 | 573 | 792 | 173 |
| Future Volume（vph） | 121 | 737 | 179 | 198 | 477 | 291 | 78 | 510 | 268 | 573 | 792 | 173 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.2 | 3.6 | 3.7 | 3.2 | 3.6 | 3.7 | 3.0 | 3.4 | 4.0 | 3.0 | 3.7 | 3.3 |
| Storage Length（m） | 65.0 |  | 50.0 | 70.0 |  | 0.0 | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（m） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | ＊0．75 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  | 1.00 |  |  |  |  | 1.00 |  |  |  |  | 0.97 |
| Frt |  | 0.971 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Fit Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1612 | 2706 | 0 | 1708 | 1845 | 1512 | 1652 | 3330 | 1670 | ＊2068 | 3444 | 1516 |
| Flt Permitted | 0.156 |  |  | 0.093 |  |  | 0.320 |  |  | 0.188 |  |  |
| Satd．Flow（perm） | 265 | 2706 | 0 | 167 | 1845 | 1512 | 555 | 3330 | 1670 | 321 | 3444 | 1473 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 17 |  |  |  | 278 |  |  | 132 |  |  | 194 |
| Link Speed（k／h） |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance（m） |  | 448.3 |  |  | 341.9 |  |  | 505.9 |  |  | 2054.7 |  |
| Travel Time（s） |  | 26.9 |  |  | 20.5 |  |  | 30.4 |  |  | 123.3 |  |
| Confl．Peds．（\＃／hr） |  |  | 2 | 2 |  |  | 4 |  |  |  |  | 4 |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles（\％） | 7\％ | 2\％ | 2\％ | 1\％ | 3\％ | 8\％ | 2\％ | 6\％ | 1\％ | 4\％ | 6\％ | 3\％ |
| Adj．Flow（vph） | 136 | 828 | 201 | 222 | 536 | 327 | 88 | 573 | 301 | 644 | 890 | 194 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 136 | 1029 | 0 | 222 | 536 | 327 | 88 | 573 | 301 | 644 | 890 | 194 |
| Turn Type | pm＋pt | NA |  | pm＋pt | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split（s） | 11.0 | 45.0 |  | 11.0 | 45.0 | 45.0 | 39.5 | 39.5 | 39.5 | 11.0 | 39.5 | 39.5 |
| Total Split（s） | 11.0 | 50.0 |  | 12.0 | 51.0 | 51.0 | 34.0 | 34.0 | 34.0 | 34.0 | 68.0 | 68.0 |
| Total Split（\％） | 8．5\％ | 38．5\％ |  | 9．2\％ | 39．2\％ | 39．2\％ | 26．2\％ | 26．2\％ | 26．2\％ | 26．2\％ | 52．3\％ | 52．3\％ |
| Maximum Green（s） | 7.0 | 42.0 |  | 8.0 | 43.0 | 43.0 | 26.5 | 26.5 | 26.5 | 30.0 | 60.5 | 60.5 |
| Yellow Time（s） | 3.0 | 4.5 |  | 3.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 1.0 | 3.5 |  | 1.0 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 1.0 | 3.0 | 3.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 8.0 |  | 4.0 | 8.0 | 8.0 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None | None | C－Max | C－Max | C－Max | None | C－Max | C－Max |
| Walk Time（s） |  | 7.0 |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  | 30.0 |  |  | 30.0 | 30.0 | 25.0 | 25.0 | 25.0 |  | 25.0 | 25.0 |
| Pedestrian Calls（\＃／hr） |  | 0 |  |  | 0 | 0 | 5 | 5 | 5 |  | 5 | 5 |
| Act Effct Green（s） | 53.0 | 42.0 |  | 55.0 | 43.0 | 43.0 | 26.5 | 26.5 | 26.5 | 64.0 | 60.5 | 60.5 |
| Actuated g／C Ratio | 0.41 | 0.32 |  | 0.42 | 0.33 | 0.33 | 0.20 | 0.20 | 0.20 | 0.49 | 0.47 | 0.47 |


|  | 4 |  |  | $\checkmark$ |  |  | 4 | $\dagger$ | \% |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.76 | 1.16 |  | 1.35 | 0.88 | 0.48 | 0.78 | 0.85 | 0.68 | 1.15 | 0.56 | 0.25 |
| Control Delay | 50.8 | 124.7 |  | 216.0 | 58.1 | 8.7 | 90.7 | 62.4 | 34.8 | 118.2 | 14.2 | 0.8 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 50.8 | 124.7 |  | 216.0 | 58.1 | 8.7 | 90.7 | 62.4 | 34.8 | 118.2 | 14.2 | 0.8 |
| LOS | D | F |  | F | E | A | F | E | C | F | B | A |
| Approach Delay |  | 116.1 |  |  | 75.5 |  |  | 56.3 |  |  | 51.5 |  |
| Approach LOS |  | F |  |  | E |  |  | E |  |  | D |  |
| Queue Length 50th (m) | 21.8 | $\sim 217.5$ |  | ~61.1 | 136.1 | 9.1 | 22.7 | 79.0 | 42.5 | $\sim 172.9$ | 38.6 | 0.1 |
| Queue Length 95th (m) | \#44.9 | \#268.3 |  | \#112.3 | \#196.0 | 33.4 | \#52.4 | \#104.5 | 74.4 m | \#241.1 | m44.9 | m0.6 |
| Internal Link Dist (m) |  | 424.3 |  |  | 317.9 |  |  | 481.9 |  |  | 2030.7 |  |
| Turn Bay Length (m) | 65.0 |  |  | 70.0 |  |  | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Base Capacity (vph) | 180 | 885 |  | 165 | 610 | 686 | 113 | 678 | 445 | 561 | 1602 | 789 |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.76 | 1.16 |  | 1.35 | 0.88 | 0.48 | 0.78 | 0.85 | 0.68 | 1.15 | 0.56 | 0.25 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: <br> Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 35 (27\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 150 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.35 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 72.9 Intersection LOS: E |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 102.8\% ICU Level of Service G |  |  |  |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| * User Entered Value |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| $m$ Volume for 95th percentile queue is metered by upstream signal. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 210: Yonge Street \& St. John's Sideroad


|  | $\rangle$ |  |  |  |  |  | 4 |  |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | $\hat{\beta}$ |  | ${ }^{7}$ | $\uparrow$ | 「 | \％ | 性 | F | ${ }^{7}$ | 性 | F |
| Traffic Volume（vph） | 95 | 459 | 55 | 168 | 482 | 48 | 55 | 610 | 61 | 166 | 1205 | 300 |
| Future Volume（vph） | 95 | 459 | 55 | 168 | 482 | 48 | 55 | 610 | 61 | 166 | 1205 | 300 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.7 | 3.7 | 3.7 | 3.0 | 3.5 | 3.7 | 3.2 | 3.7 | 4.0 | 3.1 | 3.3 | 3.7 |
| Storage Length（ m ） | 30.0 |  | 0.0 | 50.0 |  | 50.0 | 60.0 |  | 60.0 | 60.0 |  | 60.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（m） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  | 1.00 |  |  |  |  |  |  |  |  |  |  |
| Frt |  | 0.984 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1738 | 1819 | 0 | 1668 | 1807 | 1601 | 1675 | 3510 | 1622 | 1688 | 3388 | 1617 |
| Flt Permitted | 0.393 |  |  | 0.118 |  |  | 0.119 |  |  | 0.278 |  |  |
| Satd．Flow（perm） | 719 | 1819 | 0 | 207 | 1807 | 1601 | 210 | 3510 | 1622 | 494 | 3388 | 1617 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 6 |  |  |  | 83 |  |  | 122 |  |  | 217 |
| Link Speed（k／h） |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance（m） |  | 129.9 |  |  | 1758.6 |  |  | 451.2 |  |  | 794.7 |  |
| Travel Time（s） |  | 7.8 |  |  | 105.5 |  |  | 23.2 |  |  | 40.9 |  |
| Confl．Bikes（\＃／hr） |  |  | 1 |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles（\％） | 5\％ | 4\％ | 2\％ | 1\％ | 4\％ | 2\％ | 3\％ | 4\％ | 4\％ | 1\％ | 3\％ | 1\％ |
| Adj．Flow（vph） | 100 | 483 | 58 | 177 | 507 | 51 | 58 | 642 | 64 | 175 | 1268 | 316 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 100 | 541 | 0 | 177 | 507 | 51 | 58 | 642 | 64 | 175 | 1268 | 316 |
| Turn Type | Perm | NA |  | pm＋pt | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases |  | 4 |  | 3 | 8 |  |  | 6 |  | 5 | ， |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 4 | 4 |  | 3 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 10.0 | 10.0 |  | 7.0 | 10.0 | 10.0 | 20.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 |
| Minimum Split（s） | 17.5 | 17.5 |  | 11.0 | 38.5 | 38.5 | 36.5 | 36.5 | 36.5 | 11.0 | 36.5 | 36.5 |
| Total Split（s） | 42.5 | 42.5 |  | 11.0 | 42.5 | 42.5 | 47.5 | 47.5 | 47.5 | 11.0 | 47.5 | 47.5 |
| Total Split（\％） | 37．9\％ | 37．9\％ |  | 9．8\％ | 37．9\％ | 37．9\％ | 42．4\％ | 42．4\％ | 42．4\％ | 9．8\％ | 42．4\％ | 42．4\％ |
| Maximum Green（s） | 35.0 | 35.0 |  | 7.0 | 35.0 | 35.0 | 40.0 | 40.0 | 40.0 | 7.0 | 40.0 | 40.0 |
| Yellow Time（s） | 4.5 | 4.5 |  | 3.0 | 4.5 | 4.5 | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 |
| All－Red Time（s） | 3.0 | 3.0 |  | 1.0 | 3.0 | 3.0 | 2.5 | 2.5 | 2.5 | 1.0 | 2.5 | 2.5 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 7.5 | 7.5 |  | 4.0 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lag | Lag |  | Lead |  |  | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes |  |  | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 6.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 |
| Recall Mode | None | None |  | None | None | None | Min | Min | Min | None | Min | Min |
| Walk Time（s） |  |  |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  |  |  |  | 24.0 | 24.0 | 22.0 | 22.0 | 22.0 |  | 22.0 | 22.0 |
| Pedestrian Calls（\＃／hr） |  |  |  |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Act Efft Green（s） | 33.6 | 33.6 |  | 48.2 | 44.7 | 44.7 | 36.3 | 36.3 | 36.3 | 50.9 | 47.3 | 47.3 |
| Actuated g／C Ratio | 0.31 | 0.31 |  | 0.45 | 0.42 | 0.42 | 0.34 | 0.34 | 0.34 | 0.48 | 0.44 | 0.44 |



Splits and Phases: 220: Bathurst Street \& 18th Sideroad/St. John's Sideroad


|  | 4 | $\rightarrow$ | 1 | 7 |  | 4 | 4 | 9 | $p$ | （ | $\frac{1}{\dagger}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 中 ${ }^{\text {a }}$ |  | ${ }^{1}$ | 4 | 「 | ${ }^{1}$ | 44 | 「 | ${ }^{7}$ | 44 | 7 |
| Traffic Volume（vph） | 144 | 717 | 202 | 183 | 482 | 281 | 95 | 497 | 248 | 538 | 754 | 182 |
| Future Volume（vph） | 144 | 717 | 202 | 183 | 482 | 281 | 95 | 497 | 248 | 538 | 754 | 182 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.2 | 3.6 | 3.7 | 3.2 | 3.6 | 3.7 | 3.0 | 3.4 | 4.0 | 3.0 | 3.7 | 3.3 |
| Storage Length（m） | 65.0 |  | 50.0 | 70.0 |  | 0.0 | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（m） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | ＊0．75 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  | 1.00 |  |  |  |  | 1.00 |  |  |  |  | 0.98 |
| Frt |  | 0.967 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1612 | 2694 | 0 | 1708 | 1845 | 1512 | 1652 | 3330 | 1670 | ＊2068 | 3444 | 1516 |
| Flt Permitted | 0.149 |  |  | 0.093 |  |  | 0.334 |  |  | 0.201 |  |  |
| Satd．Flow（perm） | 253 | 2694 | 0 | 167 | 1845 | 1512 | 580 | 3330 | 1670 | 343 | 3444 | 1490 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 20 |  |  |  | 265 |  |  | 138 |  |  | 204 |
| Link Speed（k／h） |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance（m） |  | 448.3 |  |  | 341.9 |  |  | 505.9 |  |  | 608.7 |  |
| Travel Time（s） |  | 26.9 |  |  | 20.5 |  |  | 30.4 |  |  | 36.5 |  |
| Confl．Peds．（\＃／hr） |  |  | 2 | 2 |  |  | 4 |  |  |  |  | 4 |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles（\％） | 7\％ | 2\％ | 2\％ | 1\％ | 3\％ | 8\％ | 2\％ | 6\％ | 1\％ | 4\％ | 6\％ | 3\％ |
| Adj．Flow（vph） | 162 | 806 | 227 | 206 | 542 | 316 | 107 | 558 | 279 | 604 | 847 | 204 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 162 | 1033 | 0 | 206 | 542 | 316 | 107 | 558 | 279 | 604 | 847 | 204 |
| Turn Type | pm＋pt | NA |  | pm＋pt | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split（s） | 11.0 | 45.0 |  | 11.0 | 45.0 | 45.0 | 39.5 | 39.5 | 39.5 | 11.0 | 39.5 | 39.5 |
| Total Split（s） | 11.0 | 50.0 |  | 12.0 | 51.0 | 51.0 | 34.0 | 34.0 | 34.0 | 34.0 | 68.0 | 68.0 |
| Total Split（\％） | 8．5\％ | 38．5\％ |  | 9．2\％ | 39．2\％ | 39．2\％ | 26．2\％ | 26．2\％ | 26．2\％ | 26．2\％ | 52．3\％ | 52．3\％ |
| Maximum Green（s） | 7.0 | 42.0 |  | 8.0 | 43.0 | 43.0 | 26.5 | 26.5 | 26.5 | 30.0 | 60.5 | 60.5 |
| Yellow Time（s） | 3.0 | 4.5 |  | 3.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 1.0 | 3.5 |  | 1.0 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 1.0 | 3.0 | 3.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 8.0 |  | 4.0 | 8.0 | 8.0 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None | None | C－Max | C－Max | C－Max | None | C－Max | C－Max |
| Walk Time（s） |  | 7.0 |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  | 30.0 |  |  | 30.0 | 30.0 | 25.0 | 25.0 | 25.0 |  | 25.0 | 25.0 |
| Pedestrian Calls（\＃／hr） |  | 0 |  |  | 0 | 0 | 5 | 5 | 5 |  | 5 | 5 |
| Act Effct Green（s） | 53.0 | 42.0 |  | 55.0 | 43.0 | 43.0 | 26.5 | 26.5 | 26.5 | 64.0 | 60.5 | 60.5 |
| Actuated g／C Ratio | 0.41 | 0.32 |  | 0.42 | 0.33 | 0.33 | 0.20 | 0.20 | 0.20 | 0.49 | 0.47 | 0.47 |


|  | 4 |  |  | 7 |  | 4 | 4 | $\dagger$ | \% |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.92 | 1.17 |  | 1.25 | 0.89 | 0.47 | 0.91 | 0.82 | 0.62 | 1.07 | 0.53 | 0.25 |
| Control Delay | 71.7 | 124.3 |  | 178.7 | 59.3 | 9.0 | 112.2 | 60.7 | 30.0 | 90.4 | 16.0 | 1.0 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 71.7 | 124.3 |  | 178.7 | 59.3 | 9.0 | 112.2 | 60.7 | 30.0 | 90.4 | 16.0 | 1.0 |
| LOS | E | F |  | F | E | A | F | E | C | F | B | A |
| Approach Delay |  | 117.2 |  |  | 67.5 |  |  | 57.5 |  |  | 41.3 |  |
| Approach LOS |  | F |  |  | E |  |  | E |  |  | D |  |
| Queue Length 50th (m) | 24.0 | $\sim 219.0$ |  | ~52.0 | 138.1 | 9.5 | 28.5 | 76.4 | 34.5 | ~148.7 | 43.5 | 0.3 |
| Queue Length 95th (m) | m\#51.4 | \#269.8 |  | \#102.0 | \#199.9 | 33.3 | \#64.9 | 97.1 | 64.6 m | \#209.7 | m49.9 | m0.7 |
| Internal Link Dist (m) |  | 424.3 |  |  | 317.9 |  |  | 481.9 |  |  | 584.7 |  |
| Turn Bay Length (m) | 65.0 |  |  | 70.0 |  |  | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Base Capacity (vph) | 176 | 883 |  | 165 | 610 | 677 | 118 | 678 | 450 | 566 | 1602 | 802 |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.92 | 1.17 |  | 1.25 | 0.89 | 0.47 | 0.91 | 0.82 | 0.62 | 1.07 | 0.53 | 0.25 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 35 (27\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 150 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.25 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 68.8 Intersection LOS: E |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 99.9\% ICU Level of Service F |  |  |  |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| * User Entered Value |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| $m$ Volume for 95th percentile queue is metered by upstream signal. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 210: Yonge Street \& St. John's Sideroad


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


|  | $\stackrel{ }{*}$ |  |  |  |  |  |  | $\dagger$ | $p$ |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.43 | 0.92 |  | 0.88 | 0.68 | 0.08 | 0.56 | 0.56 | 0.13 | 0.55 | 0.79 | 0.36 |
| Control Delay | 36.3 | 57.7 |  | 60.5 | 30.4 | 1.9 | 52.3 | 29.6 | 1.6 | 22.6 | 28.5 | 7.7 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 36.3 | 57.7 |  | 60.5 | 30.4 | 1.9 | 52.3 | 29.6 | 1.6 | 22.6 | 28.5 | 7.7 |
| LOS | D | E |  | E | C | A | D | C | A | C | C | A |
| Approach Delay |  | 54.4 |  |  | 35.9 |  |  | 28.2 |  |  | 24.1 |  |
| Approach LOS |  | D |  |  | D |  |  | C |  |  | C |  |
| Queue Length 50th (m) | 14.5 | 93.2 |  | 21.6 | 77.6 | 0.0 | 8.8 | 55.0 | 0.0 | 19.9 | 102.8 | 12.5 |
| Queue Length 95th (m) | 34.6 | \#181.4 |  | \#66.0 | 136.9 | 3.5 | \#23.9 | 72.2 | 3.3 | 33.1 | 128.8 | 29.9 |
| Internal Link Dist (m) |  | 105.9 |  |  | 1734.6 |  |  | 427.2 |  |  | 770.7 |  |
| Turn Bay Length ( m ) | 30.0 |  |  | 50.0 |  | 50.0 | 60.0 |  | 60.0 | 60.0 |  | 60.0 |
| Base Capacity (vph) | 223 | 554 |  | 214 | 747 | 713 | 118 | 1417 | 730 | 316 | 1744 | 925 |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.43 | 0.92 |  | 0.88 | 0.68 | 0.08 | 0.45 | 0.45 | 0.11 | 0.55 | 0.66 | 0.32 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 107 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 99.3 |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.92 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 32.2 |  |  |  | Intersection LOS: C |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 105.9\% |  |  |  | ICU Level of Service G |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  | eue may be longer. |  |  | $\square$ |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, qued Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 220: Bathurst Street \& 18th Sideroad/St. John's Sideroad


|  | 4 |  |  | 7 |  | 4 | 4 | $\dagger$ | 7 | $t$ | $\frac{1}{\dagger}$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 4 | 「 | ${ }^{7}$ | 4 | 「 |  | * |  | ${ }^{7}$ | $\hat{\beta}$ |  |
| Traffic Volume (vph) | 52 | 890 | 3 | 20 | 666 | 72 | 1 | 4 | 65 | 107 | 4 | 66 |
| Future Volume (vph) | 52 | 890 | 3 | 20 | 666 | 72 | 1 | 4 | 65 | 107 | 4 | 66 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.0 | 3.7 | 3.7 | 3.4 | 3.3 | 3.3 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 |
| Storage Length (m) | 15.0 |  | 15.0 | 30.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 0 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  |  | 0.850 |  |  | 0.850 |  | 0.874 |  |  | 0.858 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  |  | 0.999 |  | 0.950 |  |  |
| Satd. Flow (prot) | 1685 | 1883 | 1633 | 1681 | 1801 | 1561 | 0 | 1647 | 0 | 1825 | 1648 | 0 |
| Flt Permitted | 0.323 |  |  | 0.187 |  |  |  | 0.995 |  | 0.709 |  |  |
| Satd. Flow (perm) | 573 | 1883 | 1633 | 331 | 1801 | 1561 | 0 | 1640 | 0 | 1362 | 1648 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 50 |  |  | 77 |  | 69 |  |  | 70 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 40 |  |  | 50 |  |
| Link Distance (m) |  | 1758.6 |  |  | 448.3 |  |  | 195.4 |  |  | 116.6 |  |
| Travel Time (s) |  | 105.5 |  |  | 26.9 |  |  | 17.6 |  |  | 8.4 |  |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Heavy Vehicles (\%) | 0\% | 2\% | 0\% | 5\% | 2\% | 0\% | 0\% | 0\% | 2\% | 0\% | 0\% | 0\% |
| Adj. Flow (vph) | 55 | 947 | 3 | 21 | 709 | 77 | 1 | 4 | 69 | 114 | 4 | 70 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 55 | 947 | 3 | 21 | 709 | 77 | 0 | 74 | 0 | 114 | 74 | 0 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 8 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 | 2 | 6 | 6 | 6 | 8 | 8 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 24.0 | 24.0 | 24.0 | 24.0 | 24.0 | 24.0 | 27.0 | 27.0 |  | 27.0 | 27.0 |  |
| Total Split (s) | 38.0 | 38.0 | 38.0 | 38.0 | 38.0 | 38.0 | 27.0 | 27.0 |  | 27.0 | 27.0 |  |
| Total Split (\%) | 58.5\% | 58.5\% | 58.5\% | 58.5\% | 58.5\% | 58.5\% | 41.5\% | 41.5\% |  | 41.5\% | 41.5\% |  |
| Maximum Green (s) | 32.0 | 32.0 | 32.0 | 32.0 | 32.0 | 32.0 | 21.0 | 21.0 |  | 21.0 | 21.0 |  |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | C-Max | C-Max | C-Max | C-Max | C-Max | C-Max | None | None |  | None | None |  |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 9.0 | 9.0 | 9.0 | 9.0 | 9.0 | 9.0 | 14.0 | 14.0 |  | 14.0 | 14.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Act Effct Green (s) | 45.9 | 45.9 | 45.9 | 45.9 | 45.9 | 45.9 |  | 10.6 |  | 10.7 | 10.7 |  |
| Actuated g/C Ratio | 0.71 | 0.71 | 0.71 | 0.71 | 0.71 | 0.71 |  | 0.16 |  | 0.16 | 0.16 |  |
| v/c Ratio | 0.14 | 0.71 | 0.00 | 0.09 | 0.56 | 0.07 |  | 0.23 |  | 0.51 | 0.22 |  |
| Control Delay | 6.7 | 13.5 | 0.0 | 1.8 | 5.8 | 0.2 |  | 8.7 |  | 31.7 | 8.5 |  |



Splits and Phases: 330: Willow Farm Lane/Street "A" \& St. John's Sideroad


|  | $\stackrel{ }{*}$ |  |  | 7 |  |  | 4 | 4 | P |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个 ${ }^{\text {a }}$ |  | \％ | 4 | F | ${ }^{7}$ | 个4 | F | \％ | 个4 | F |
| Traffic Volume（vph） | 164 | 833 | 247 | 179 | 570 | 291 | 123 | 501 | 250 | 573 | 782 | 214 |
| Future Volume（vph） | 164 | 833 | 247 | 179 | 570 | 291 | 123 | 501 | 250 | 573 | 782 | 214 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.2 | 3.6 | 3.7 | 3.2 | 3.6 | 3.7 | 3.0 | 3.4 | 4.0 | 3.0 | 3.7 | 3.3 |
| Storage Length（ m ） | 65.0 |  | 50.0 | 70.0 |  | 0.0 | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ m ） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | ＊0．75 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  | 1.00 |  |  |  |  | 1.00 |  |  |  |  | 0.98 |
| Frt |  | 0.966 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1612 | 2690 | 0 | 1708 | 1845 | 1512 | 1652 | 3330 | 1670 | ＊2068 | 3444 | 1516 |
| Flt Permitted | 0.085 |  |  | 0.087 |  |  | 0.273 |  |  | 0.197 |  |  |
| Satd．Flow（perm） | 144 | 2690 | 0 | 156 | 1845 | 1512 | 474 | 3330 | 1670 | 336 | 3444 | 1490 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 23 |  |  |  | 241 |  |  | 144 |  |  | 240 |
| Link Speed（kh） |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance（m） |  | 448.3 |  |  | 341.9 |  |  | 505.9 |  |  | 608.7 |  |
| Travel Time（s） |  | 26.9 |  |  | 20.5 |  |  | 30.4 |  |  | 36.5 |  |
| Confl．Peds．（\＃／hr） |  |  | 2 | 2 |  |  | 4 |  |  |  |  | 4 |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles（\％） | 7\％ | 2\％ | 2\％ | 1\％ | 3\％ | 8\％ | 2\％ | 6\％ | 1\％ | 4\％ | 6\％ | 3\％ |
| Adj．Flow（vph） | 184 | 936 | 278 | 201 | 640 | 327 | 138 | 563 | 281 | 644 | 879 | 240 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 184 | 1214 | 0 | 201 | 640 | 327 | 138 | 563 | 281 | 644 | 879 | 240 |
| Turn Type | pm＋pt | NA |  | pm＋pt | NA | Perm | pm＋pt | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | ， |  | ， | 8 |  | 1 | － |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 1 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split（s） | 11.0 | 45.0 |  | 11.0 | 45.0 | 45.0 | 11.0 | 39.5 | 39.5 | 11.0 | 39.5 | 39.5 |
| Total Split（s） | 13.0 | 55.0 |  | 12.0 | 54.0 | 54.0 | 11.0 | 34.0 | 34.0 | 29.0 | 52.0 | 52.0 |
| Total Split（\％） | 10．0\％ | 42．3\％ |  | 9．2\％ | 41．5\％ | 41．5\％ | 8．5\％ | 26．2\％ | 26．2\％ | 22．3\％ | 40．0\％ | 40．0\％ |
| Maximum Green（s） | 9.0 | 47.0 |  | 8.0 | 46.0 | 46.0 | 7.0 | 26.5 | 26.5 | 25.0 | 44.5 | 44.5 |
| Yellow Time（s） | 3.0 | 4.5 |  | 3.0 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 1.0 | 3.5 |  | 1.0 | 3.5 | 3.5 | 1.0 | 3.0 | 3.0 | 1.0 | 3.0 | 3.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 8.0 |  | 4.0 | 8.0 | 8.0 | 4.0 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None | None | None | C－Max | C－Max | None | C－Max | C－Max |
| Walk Time（s） |  | 7.0 |  |  | 7.0 | 7.0 |  | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  | 30.0 |  |  | 30.0 | 30.0 |  | 25.0 | 25.0 |  | 25.0 | 25.0 |
| Pedestrian Calls（\＃／hr） |  | 0 |  |  | 0 | 0 |  | 5 | 5 |  | 5 | 5 |
| Act Effct Green（s） | 60.0 | 47.0 |  | 58.0 | 46.0 | 46.0 | 37.0 | 26.5 | 26.5 | 59.0 | 44.5 | 44.5 |
| Actuated g／C Ratio | 0.46 | 0.36 |  | 0.45 | 0.35 | 0.35 | 0.28 | 0.20 | 0.20 | 0.45 | 0.34 | 0.34 |


|  | $\Rightarrow$ |  |  | 7 |  |  | 4 |  | $p$ |  | $\pm$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 1.10 | 1.23 |  | 1.22 | 0.98 | 0.47 | 0.70 | 0.83 | 0.62 | 1.33 | 0.75 | 0.36 |
| Control Delay | 117.8 | 145.9 |  | 168.1 | 72.8 | 11.1 | 46.1 | 61.2 | 29.0 | 199.1 | 49.0 | 13.9 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 117.8 | 145.9 |  | 168.1 | 72.8 | 11.1 | 46.1 | 61.2 | 29.0 | 199.1 | 49.0 | 13.9 |
| LOS | F | F |  | F | E | B | D | E | C | F | D | B |
| Approach Delay |  | 142.2 |  |  | 71.9 |  |  | 49.9 |  |  | 99.0 |  |
| Approach LOS |  | F |  |  | E |  |  | D |  |  | F |  |
| Queue Length 50th (m) | ~39.9 | $\sim 264.8$ |  | $\sim 49.3$ | 170.0 | 15.8 | 21.8 | 77.2 | 33.4 | ~204.5 | 100.5 | 11.3 |
| Queue Length 95th (m) | m\#71.6m | \#314.6 |  | \#98.9 | \#245.7 | 41.7 | \#40.3 | \#99.2 | 63.5 m | \#267.0 | m124.3 | m26.4 |
| Internal Link Dist (m) |  | 424.3 |  |  | 317.9 |  |  | 481.9 |  |  | 584.7 |  |
| Turn Bay Length (m) | 65.0 |  |  | 70.0 |  |  | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Base Capacity (vph) | 168 | 987 |  | 165 | 652 | 690 | 198 | 678 | 455 | 485 | 1178 | 667 |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 1.10 | 1.23 |  | 1.22 | 0.98 | 0.47 | 0.70 | 0.83 | 0.62 | 1.33 | 0.75 | 0.36 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 0 (0\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 150 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.33 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 95.3 Intersection LOS: F |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 106.1\% ICU Level of Service G |  |  |  |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| * User Entered Value |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| $m$ Volume for 95th percentile queue is metered by upstream signal. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 210: Yonge Street \& St. John's Sideroad


|  | 4 | $\rightarrow$ |  | 7 |  |  | 4 | 4 | $p$ | ( | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | 4 | F | ${ }^{1}$ | 44 | 「 | ${ }^{7}$ | 44 | 「 |
| Traffic Volume (vph) | 95 | 505 | 55 | 210 | 522 | 70 | 55 | 610 | 113 | 200 | 1205 | 300 |
| Future Volume (vph) | 95 | 505 | 55 | 210 | 522 | 70 | 55 | 610 | 113 | 200 | 1205 | 300 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.7 | 3.7 | 3.7 | 3.0 | 3.5 | 3.7 | 3.2 | 3.7 | 4.0 | 3.1 | 3.3 | 3.7 |
| Storage Length (m) | 30.0 |  | 0.0 | 50.0 |  | 50.0 | 60.0 |  | 60.0 | 60.0 |  | 60.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length (m) | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  | 1.00 |  |  |  |  |  |  |  |  |  |  |
| Frt |  | 0.985 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1738 | 1821 | 0 | 1668 | 1807 | 1601 | 1675 | 3510 | 1622 | 1688 | 3388 | 1617 |
| Flt Permitted | 0.383 |  |  | 0.091 |  |  | 0.099 |  |  | 0.273 |  |  |
| Satd. Flow (perm) | 701 | 1821 | 0 | 160 | 1807 | 1601 | 175 | 3510 | 1622 | 485 | 3388 | 1617 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 5 |  |  |  | 73 |  |  | 119 |  |  | 204 |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance (m) |  | 129.9 |  |  | 1758.6 |  |  | 451.2 |  |  | 794.7 |  |
| Travel Time (s) |  | 7.8 |  |  | 105.5 |  |  | 23.2 |  |  | 40.9 |  |
| Confl. Bikes (\#/hr) |  |  | 1 |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles (\%) | 5\% | 4\% | 2\% | 1\% | 4\% | 2\% | 3\% | 4\% | 4\% | 1\% | 3\% | 1\% |
| Adj. Flow (vph) | 100 | 532 | 58 | 221 | 549 | 74 | 58 | 642 | 119 | 211 | 1268 | 316 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 100 | 590 | 0 | 221 | 549 | 74 | 58 | 642 | 119 | 211 | 1268 | 316 |
| Turn Type | Perm | NA |  | pm+pt | NA | Perm | Perm | NA | Perm | pm+pt | NA | Perm |
| Protected Phases |  | 4 |  | 3 | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 4 | 4 |  | 3 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 10.0 | 10.0 |  | 7.0 | 10.0 | 10.0 | 20.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 |
| Minimum Split (s) | 17.5 | 17.5 |  | 11.0 | 38.5 | 38.5 | 36.5 | 36.5 | 36.5 | 11.0 | 36.5 | 36.5 |
| Total Split (s) | 47.5 | 47.5 |  | 16.0 | 47.5 | 47.5 | 52.5 | 52.5 | 52.5 | 11.0 | 52.5 | 52.5 |
| Total Split (\%) | 37.4\% | 37.4\% |  | 12.6\% | 37.4\% | 37.4\% | 41.3\% | 41.3\% | 41.3\% | 8.7\% | 41.3\% | 41.3\% |
| Maximum Green (s) | 40.0 | 40.0 |  | 12.0 | 40.0 | 40.0 | 45.0 | 45.0 | 45.0 | 7.0 | 45.0 | 45.0 |
| Yellow Time (s) | 4.5 | 4.5 |  | 3.0 | 4.5 | 4.5 | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 |
| All-Red Time (s) | 3.0 | 3.0 |  | 1.0 | 3.0 | 3.0 | 2.5 | 2.5 | 2.5 | 1.0 | 2.5 | 2.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.5 | 7.5 |  | 4.0 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead/Lag | Lag | Lag |  | Lead |  |  | Lag | Lag | Lag | Lead |  |  |
| Lead-Lag Optimize? | Yes | Yes |  | Yes |  |  | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 6.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 |
| Recall Mode | None | None |  | None | None | None | Min | Min | Min | None | Min | Min |
| Walk Time (s) |  |  |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk (s) |  |  |  |  | 24.0 | 24.0 | 22.0 | 22.0 | 22.0 |  | 22.0 | 22.0 |
| Pedestrian Calls (\#/hr) |  |  |  |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Act Effct Green (s) | 40.1 | 40.1 |  | 59.6 | 56.1 | 56.1 | 42.7 | 42.7 | 42.7 | 57.2 | 53.7 | 53.7 |
| Actuated g/C Ratio | 0.32 | 0.32 |  | 0.48 | 0.45 | 0.45 | 0.34 | 0.34 | 0.34 | 0.46 | 0.43 | 0.43 |



Splits and Phases: 220: Bathurst Street \& 18th Sideroad/St. John's Sideroad


|  | 4 |  | $\checkmark$ | 7 | 4 | 4 | 4 | $\dagger$ | 7 | $1$ | $\dagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 4 | F | ${ }^{7}$ | 4 | 「 |  | \$ |  | ${ }^{7}$ | $\dagger$ |  |
| Traffic Volume (vph) | 160 | 945 | 3 | 20 | 681 | 206 | 1 | 14 | 65 | 234 | 14 | 132 |
| Future Volume (vph) | 160 | 945 | 3 | 20 | 681 | 206 | 1 | 14 | 65 | 234 | 14 | 132 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.0 | 3.7 | 3.7 | 3.4 | 3.3 | 3.3 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 |
| Storage Length (m) | 15.0 |  | 15.0 | 30.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 0 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  |  | 0.850 |  |  | 0.850 |  | 0.890 |  |  | 0.865 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  |  | 0.999 |  | 0.950 |  |  |
| Satd. Flow (prot) | 1685 | 1883 | 1633 | 1681 | 1801 | 1561 | 0 | 1681 | 0 | 1825 | 1662 | 0 |
| Flt Permitted | 0.250 |  |  | 0.187 |  |  |  | 0.998 |  | 0.692 |  |  |
| Satd. Flow (perm) | 443 | 1883 | 1633 | 331 | 1801 | 1561 | 0 | 1679 | 0 | 1329 | 1662 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 25 |  |  | 219 |  | 69 |  |  | 140 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 40 |  |  | 50 |  |
| Link Distance (m) |  | 1758.6 |  |  | 448.3 |  |  | 195.4 |  |  | 116.6 |  |
| Travel Time (s) |  | 105.5 |  |  | 26.9 |  |  | 17.6 |  |  | 8.4 |  |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Heavy Vehicles (\%) | 0\% | 2\% | 0\% | 5\% | 2\% | 0\% | 0\% | 0\% | 2\% | 0\% | 0\% | 0\% |
| Adj. Flow (vph) | 170 | 1005 | 3 | 21 | 724 | 219 | 1 | 15 | 69 | 249 | 15 | 140 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 170 | 1005 | 3 | 21 | 724 | 219 | 0 | 85 | 0 | 249 | 155 | 0 |
| Turn Type | pm+pt | NA | Perm | Perm | NA | Perm | Perm | NA |  | Perm | NA |  |
| Protected Phases | 5 | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 8 |  |  | 4 |  |  |
| Detector Phase | 5 | 2 | 2 | 6 | 6 | 6 | 8 | 8 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 11.0 | 24.0 | 24.0 | 24.0 | 24.0 | 24.0 | 27.0 | 27.0 |  | 27.0 | 27.0 |  |
| Total Split (s) | 11.0 | 98.0 | 98.0 | 87.0 | 87.0 | 87.0 | 32.0 | 32.0 |  | 32.0 | 32.0 |  |
| Total Split (\%) | 8.5\% | 75.4\% | 75.4\% | 66.9\% | 66.9\% | 66.9\% | 24.6\% | 24.6\% |  | 24.6\% | 24.6\% |  |
| Maximum Green (s) | 7.0 | 92.0 | 92.0 | 81.0 | 81.0 | 81.0 | 26.0 | 26.0 |  | 26.0 | 26.0 |  |
| Yellow Time (s) | 3.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 1.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 4.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag | Lead |  |  | Lag | Lag | Lag |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes | Yes |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | C-Max | C-Max | C-Max | C-Max | C-Max | None | None |  | None | None |  |
| Walk Time (s) |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) |  | 9.0 | 9.0 | 9.0 | 9.0 | 9.0 | 14.0 | 14.0 |  | 14.0 | 14.0 |  |
| Pedestrian Calls (\#/hr) |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Act Effct Green (s) | 94.4 | 92.4 | 92.4 | 81.4 | 81.4 | 81.4 |  | 25.6 |  | 25.6 | 25.6 |  |
| Actuated g/C Ratio | 0.73 | 0.71 | 0.71 | 0.63 | 0.63 | 0.63 |  | 0.20 |  | 0.20 | 0.20 |  |
| v/c Ratio | 0.44 | 0.75 | 0.00 | 0.10 | 0.64 | 0.21 |  | 0.22 |  | 0.95 | 0.35 |  |
| Control Delay | 9.1 | 16.3 | 0.0 | 5.2 | 6.4 | 0.3 |  | 15.0 |  | 96.7 | 11.4 |  |



Splits and Phases: 330: Willow Farm Lane/Street "A" \& St. John's Sideroad


|  | 4 |  |  | 7 |  | 4 | 4 | $\dagger$ | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个t |  | \％ | $\uparrow$ | F | \％ | 个4 | F | ${ }^{7}$ | 个个 | F |
| Traffic Volume（vph） | 181 | 511 | 83 | 264 | 615 | 697 | 153 | 890 | 272 | 340 | 651 | 138 |
| Future Volume（vph） | 181 | 511 | 83 | 264 | 615 | 697 | 153 | 890 | 272 | 340 | 651 | 138 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.2 | 3.6 | 3.7 | 3.2 | 3.6 | 3.7 | 3.0 | 3.4 | 4.0 | 3.0 | 3.7 | 3.3 |
| Storage Length（m） | 65.0 |  | 50.0 | 70.0 |  | 0.0 | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ m ） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | ＊0．75 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor | 1.00 | 1.00 |  | 1.00 |  | 0.98 | 1.00 |  | 0.99 | 1.00 |  | 0.97 |
| Fit |  | 0.979 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1725 | 2737 | 0 | 1708 | 1881 | 1633 | 1685 | 3461 | 1670 | ＊2068 | 3544 | 1516 |
| Flt Permitted | 0.108 |  |  | 0.176 |  |  | 0.391 |  |  | 0.104 |  |  |
| Satd．Flow（perm） | 196 | 2737 | 0 | 316 | 1881 | 1608 | 691 | 3461 | 1648 | 181 | 3544 | 1470 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 11 |  |  |  | 307 |  |  | 208 |  |  | 145 |
| Link Speed（kh） |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance（m） |  | 448.3 |  |  | 341.9 |  |  | 505.9 |  |  | 2054.7 |  |
| Travel Time（s） |  | 26.9 |  |  | 20.5 |  |  | 30.4 |  |  | 123.3 |  |
| Confl．Peds．（\＃／hr） | 2 |  | 3 | 3 |  | 2 | 5 |  | 1 | 1 |  | 5 |
| Confl．Bikes（\＃／hr） |  |  |  |  |  | 2 |  |  |  |  |  | 1 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles（\％） | 0\％ | 2\％ | 0\％ | 1\％ | 1\％ | 0\％ | 0\％ | 2\％ | 1\％ | 2\％ | 3\％ | 3\％ |
| Adj．Flow（vph） | 191 | 538 | 87 | 278 | 647 | 734 | 161 | 937 | 286 | 358 | 685 | 145 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 191 | 625 | 0 | 278 | 647 | 734 | 161 | 937 | 286 | 358 | 685 | 145 |
| Turn Type | pm＋pt | NA |  | pm＋pt | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split（s） | 11.0 | 45.0 |  | 11.0 | 45.0 | 45.0 | 39.5 | 39.5 | 39.5 | 11.0 | 39.5 | 39.5 |
| Total Split（s） | 11.0 | 45.0 |  | 14.0 | 48.0 | 48.0 | 42.0 | 42.0 | 42.0 | 19.0 | 61.0 | 61.0 |
| Total Split（\％） | 9．2\％ | 37．5\％ |  | 11．7\％ | 40．0\％ | 40．0\％ | 35．0\％ | 35．0\％ | 35．0\％ | 15．8\％ | 50．8\％ | 50．8\％ |
| Maximum Green（s） | 7.0 | 37.0 |  | 10.0 | 40.0 | 40.0 | 34.5 | 34.5 | 34.5 | 15.0 | 53.5 | 53.5 |
| Yellow Time（s） | 3.0 | 4.5 |  | 3.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 1.0 | 3.5 |  | 1.0 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 1.0 | 3.0 | 3.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 8.0 |  | 4.0 | 8.0 | 8.0 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None | None | C－Max | C－Max | C－Max | None | C－Max | C－Max |
| Walk Time（s） |  | 7.0 |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  | 30.0 |  |  | 30.0 | 30.0 | 25.0 | 25.0 | 25.0 |  | 25.0 | 25.0 |
| Pedestrian Calls（\＃／hr） |  | 5 |  |  | 5 | 5 | 5 | 5 | 5 |  | 5 | 5 |
| Act Efft Green（s） | 48.0 | 37.0 |  | 54.0 | 40.0 | 40.0 | 34.5 | 34.5 | 34.5 | 57.0 | 53.5 | 53.5 |


|  | 4 | $\rightarrow$ |  | $\dagger$ |  |  | 4 | $\dagger$ | $p$ |  | $\dagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Actuated g/C Ratio | 0.40 | 0.31 |  | 0.45 | 0.33 | 0.33 | 0.29 | 0.29 | 0.29 | 0.48 | 0.45 | 0.45 |
| v/c Ratio | 1.14 | 0.73 |  | 1.08 | 1.03 | 0.99 | 0.81 | 0.94 | 0.46 | 1.12 | 0.43 | 0.20 |
| Control Delay | 139.0 | 42.5 |  | 104.0 | 84.1 | 55.0 | 70.9 | 59.6 | 12.6 | 118.4 | 23.9 | 3.8 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 139.0 | 42.5 |  | 104.0 | 84.1 | 55.0 | 70.9 | 59.6 | 12.6 | 118.4 | 23.9 | 3.8 |
| LOS | F | D |  | F | F | D | E | E | B | F | C | A |
| Approach Delay |  | 65.1 |  |  | 74.6 |  |  | 51.2 |  |  | 49.9 |  |
| Approach LOS |  | E |  |  | E |  |  | D |  |  | D |  |
| Queue Length 50th (m) | -37.2 | 90.6 |  | ~46.0 | ~172.0 | 121.7 | 37.1 | 119.5 | 14.5 | ~85.1 | 60.1 | 0.0 |
| Queue Length 95th (m) | \#86.4 | 119.2 |  | \#102.2 | \#244.8 | \#209.5 | \#76.7 | \#161.3 | 39.6 | \#146.5 | 76.6 | 11.8 |
| Internal Link Dist (m) |  | 424.3 |  |  | 317.9 |  |  | 481.9 |  |  | 2030.7 |  |
| Turn Bay Length (m) | 65.0 |  |  | 70.0 |  |  | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Base Capacity (vph) | 167 | 851 |  | 258 | 627 | 740 | 198 | 995 | 622 | 321 | 1580 | 735 |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 1.14 | 0.73 |  | 1.08 | 1.03 | 0.99 | 0.81 | 0.94 | 0.46 | 1.12 | 0.43 | 0.20 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 39 (33\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.14 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 60.8 Intersection LOS: E |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 107.5\% ICU Level of Service G |  |  |  |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| * User Entered Value |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 210: Yonge Street \& St. John's Sideroad


|  | 4 | $\rightarrow$ |  | $\checkmark$ |  |  | 4 | $\dagger$ | $p$ | ， | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1}$ | $\uparrow$ |  | ${ }^{1}$ | 4 | 「 | ${ }^{7}$ | 44 | 「 | ${ }^{7}$ | 44 | 「 |
| Traffic Volume（vph） | 250 | 487 | 35 | 135 | 428 | 164 | 85 | 1105 | 200 | 82 | 670 | 120 |
| Future Volume（vph） | 250 | 487 | 35 | 135 | 428 | 164 | 85 | 1105 | 200 | 82 | 670 | 120 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.7 | 3.7 | 3.7 | 3.0 | 3.5 | 3.7 | 3.2 | 3.7 | 4.0 | 3.1 | 3.3 | 3.7 |
| Storage Length（m） | 30.0 |  | 0.0 | 50.0 |  | 50.0 | 60.0 |  | 60.0 | 60.0 |  | 60.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（m） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  |  |  |  |  | 0.99 |  |  |  |  |  |  |
| Frt |  | 0.990 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Fit Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1807 | 1882 | 0 | 1636 | 1842 | 1633 | 1708 | 3579 | 1670 | 1655 | 3421 | 1617 |
| Flt Permitted | 0.175 |  |  | 0.368 |  |  | 0.386 |  |  | 0.092 |  |  |
| Satd．Flow（perm） | 333 | 1882 | 0 | 634 | 1842 | 1612 | 694 | 3579 | 1670 | 160 | 3421 | 1617 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 4 |  |  |  | 125 |  |  | 140 |  |  | 125 |
| Link Speed（k／h） |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance（m） |  | 129.9 |  |  | 1758.6 |  |  | 451.2 |  |  | 794.7 |  |
| Travel Time（s） |  | 7.8 |  |  | 105.5 |  |  | 23.2 |  |  | 40.9 |  |
| Confl．Bikes（\＃／hr） |  |  |  |  |  | 1 |  |  |  |  |  |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Heavy Vehicles（\％） | 1\％ | 1\％ | 2\％ | 3\％ | 2\％ | 0\％ | 1\％ | 2\％ | 1\％ | 3\％ | 2\％ | 1\％ |
| Adj．Flow（vph） | 260 | 507 | 36 | 141 | 446 | 171 | 89 | 1151 | 208 | 85 | 698 | 125 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 260 | 543 | 0 | 141 | 446 | 171 | 89 | 1151 | 208 | 85 | 698 | 125 |
| Turn Type | pm＋pt | NA |  | Perm | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | 4 |  |  | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 8 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 7.0 | 10.0 |  | 10.0 | 10.0 | 10.0 | 20.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 |
| Minimum Split（s） | 11.0 | 17.5 |  | 38.5 | 38.5 | 38.5 | 36.5 | 36.5 | 36.5 | 11.0 | 36.5 | 36.5 |
| Total Split（s） | 14.0 | 42.5 |  | 42.5 | 42.5 | 42.5 | 47.5 | 47.5 | 47.5 | 11.0 | 47.5 | 47.5 |
| Total Split（\％） | 12．2\％ | 37．0\％ |  | 37．0\％ | 37．0\％ | 37．0\％ | 41．3\％ | 41．3\％ | 41．3\％ | 9．6\％ | 41．3\％ | 41．3\％ |
| Maximum Green（s） | 10.0 | 35.0 |  | 35.0 | 35.0 | 35.0 | 40.0 | 40.0 | 40.0 | 7.0 | 40.0 | 40.0 |
| Yellow Time（s） | 3.0 | 4.5 |  | 4.5 | 4.5 | 4.5 | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 |
| All－Red Time（s） | 1.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 2.5 | 2.5 | 2.5 | 1.0 | 2.5 | 2.5 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 7.5 |  | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead |  |  | Lag | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes |  |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 6.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 |
| Recall Mode | None | None |  | None | None | None | Min | Min | Min | None | Min | Min |
| Walk Time（s） |  |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  |  |  | 24.0 | 24.0 | 24.0 | 22.0 | 22.0 | 22.0 |  | 22.0 | 22.0 |
| Pedestrian Calls（\＃／hr） |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Act Effct Green（s） | 47.7 | 44.1 |  | 29.9 | 29.9 | 29.9 | 39.7 | 39.7 | 39.7 | 51.6 | 48.1 | 48.1 |
| Actuated g／C Ratio | 0.44 | 0.41 |  | 0.28 | 0.28 | 0.28 | 0.37 | 0.37 | 0.37 | 0.48 | 0.45 | 0.45 |



Splits and Phases: 220: Bathurst Street \& 18th Sideroad/St. John's Sideroad


|  | $\rangle$ |  |  |  |  |  | 4 | 4 | $>$ |  | $\frac{1}{7}$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％ | 个t |  | \％ | 4 | 「 | ${ }^{7}$ | 个 $\uparrow$ | F | ${ }^{7}$ | 性 | F |
| Traffic Volume（vph） | 191 | 536 | 88 | 274 | 670 | 742 | 163 | 930 | 287 | 350 | 666 | 148 |
| Future Volume（vph） | 191 | 536 | 88 | 274 | 670 | 742 | 163 | 930 | 287 | 350 | 666 | 148 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.2 | 3.6 | 3.7 | 3.2 | 3.6 | 3.7 | 3.0 | 3.4 | 4.0 | 3.0 | 3.7 | 3.3 |
| Storage Length（m） | 65.0 |  | 50.0 | 70.0 |  | 0.0 | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（ m ） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | ＊0．75 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor | 1.00 | 1.00 |  | 1.00 |  | 0.98 | 1.00 |  | 0.99 | 1.00 |  | 0.97 |
| Fit |  | 0.979 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1725 | 2737 | 0 | 1708 | 1881 | 1633 | 1685 | 3461 | 1670 | ＊2068 | 3544 | 1516 |
| Flt Permitted | 0.108 |  |  | 0.151 |  |  | 0.385 |  |  | 0.104 |  |  |
| Satd．Flow（perm） | 196 | 2737 | 0 | 271 | 1881 | 1608 | 680 | 3461 | 1648 | 181 | 3544 | 1470 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 12 |  |  |  | 290 |  |  | 200 |  |  | 156 |
| Link Speed（k／h） |  | 60 |  |  | 60 |  |  | 60 |  |  | 60 |  |
| Link Distance（m） |  | 448.3 |  |  | 341.9 |  |  | 505.9 |  |  | 2054.7 |  |
| Travel Time（s） |  | 26.9 |  |  | 20.5 |  |  | 30.4 |  |  | 123.3 |  |
| Confl．Peds．（\＃／hr） | 2 |  | 3 | 3 |  | 2 | 5 |  | 1 | 1 |  | 5 |
| Confl．Bikes（\＃／hr） |  |  |  |  |  | 2 |  |  |  |  |  | 1 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles（\％） | 0\％ | 2\％ | 0\％ | 1\％ | 1\％ | 0\％ | 0\％ | 2\％ | 1\％ | 2\％ | 3\％ | 3\％ |
| Adj．Flow（vph） | 201 | 564 | 93 | 288 | 705 | 781 | 172 | 979 | 302 | 368 | 701 | 156 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 201 | 657 | 0 | 288 | 705 | 781 | 172 | 979 | 302 | 368 | 701 | 156 |
| Turn Type | pm＋pt | NA |  | pm＋pt | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 7.0 | 7.0 |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |
| Minimum Split（s） | 11.0 | 45.0 |  | 11.0 | 45.0 | 45.0 | 39.5 | 39.5 | 39.5 | 11.0 | 39.5 | 39.5 |
| Total Split（s） | 11.0 | 45.0 |  | 15.0 | 49.0 | 49.0 | 42.0 | 42.0 | 42.0 | 18.0 | 60.0 | 60.0 |
| Total Split（\％） | 9．2\％ | 37．5\％ |  | 12．5\％ | 40．8\％ | 40．8\％ | 35．0\％ | 35．0\％ | 35．0\％ | 15．0\％ | 50．0\％ | 50．0\％ |
| Maximum Green（s） | 7.0 | 37.0 |  | 11.0 | 41.0 | 41.0 | 34.5 | 34.5 | 34.5 | 14.0 | 52.5 | 52.5 |
| Yellow Time（s） | 3.0 | 4.5 |  | 3.0 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 3.0 | 4.5 | 4.5 |
| All－Red Time（s） | 1.0 | 3.5 |  | 1.0 | 3.5 | 3.5 | 3.0 | 3.0 | 3.0 | 1.0 | 3.0 | 3.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 8.0 |  | 4.0 | 8.0 | 8.0 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead | Lag |  | Lead | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None | None | C－Max | C－Max | C－Max | None | C－Max | C－Max |
| Walk Time（s） |  | 7.0 |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  | 30.0 |  |  | 30.0 | 30.0 | 25.0 | 25.0 | 25.0 |  | 25.0 | 25.0 |
| Pedestrian Calls（\＃／hr） |  | 5 |  |  | 5 | 5 | 5 | 5 | 5 |  | 5 | 5 |
| Act Effct Green（s） | 48.0 | 37.0 |  | 56.0 | 41.0 | 41.0 | 34.5 | 34.5 | 34.5 | 56.0 | 52.5 | 52.5 |


|  | 4 | $\rightarrow$ |  | $\downarrow$ |  |  | 4 | $\dagger$ | \% |  | $\dagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Actuated g/C Ratio | 0.40 | 0.31 |  | 0.47 | 0.34 | 0.34 | 0.29 | 0.29 | 0.29 | 0.47 | 0.44 | 0.44 |
| v/c Ratio | 1.20 | 0.77 |  | 1.12 | 1.10 | 1.06 | 0.88 | 0.98 | 0.49 | 1.21 | 0.45 | 0.21 |
| Control Delay | 160.0 | 44.1 |  | 115.3 | 103.1 | 73.6 | 82.0 | 67.7 | 14.8 | 153.1 | 24.8 | 3.9 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 160.0 | 44.1 |  | 115.3 | 103.1 | 73.6 | 82.0 | 67.7 | 14.8 | 153.1 | 24.8 | 3.9 |
| LOS | F | D |  | F | F | E | F | E | B | F | C | A |
| Approach Delay |  | 71.3 |  |  | 92.1 |  |  | 58.4 |  |  | 60.7 |  |
| Approach LOS |  | E |  |  | F |  |  | E |  |  | E |  |
| Queue Length 50th (m) | $\sim 42.9$ | 96.6 |  | ~55.1 | ~197.9 | ~161.4 | 40.7 | 127.0 | 19.2 | ~94.9 | 62.8 | 0.0 |
| Queue Length 95th (m) | \#92.7 | 126.8 |  | \#112.3 | \#272.7 | \#239.5 | \#84.2 | \#173.0 | 46.7 | \#157.3 | 79.8 | 12.5 |
| Internal Link Dist (m) |  | 424.3 |  |  | 317.9 |  |  | 481.9 |  |  | 2030.7 |  |
| Turn Bay Length (m) | 65.0 |  |  | 70.0 |  |  | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Base Capacity (vph) | 167 | 852 |  | 258 | 642 | 740 | 195 | 995 | 616 | 304 | 1550 | 730 |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 1.20 | 0.77 |  | 1.12 | 1.10 | 1.06 | 0.88 | 0.98 | 0.49 | 1.21 | 0.45 | 0.21 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 39 (33\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.21 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 72.3 Intersection LOS: E |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 111.5\% ICU Level of Service H |  |  |  |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| * User Entered Value |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 210: Yonge Street \& St. John's Sideroad


|  | 4 | $\rightarrow$ | 7 | 7 |  |  | 4 | 4 | 7 | $1$ | $\ddagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | 4 | 「 | ${ }^{1}$ | 44 | 「 | ${ }^{7}$ | 44 | 「 |
| Traffic Volume（vph） | 265 | 512 | 35 | 145 | 468 | 179 | 95 | 1210 | 210 | 87 | 690 | 130 |
| Future Volume（vph） | 265 | 512 | 35 | 145 | 468 | 179 | 95 | 1210 | 210 | 87 | 690 | 130 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width（m） | 3.7 | 3.7 | 3.7 | 3.0 | 3.5 | 3.7 | 3.2 | 3.7 | 4.0 | 3.1 | 3.3 | 3.7 |
| Storage Length（m） | 30.0 |  | 0.0 | 50.0 |  | 50.0 | 60.0 |  | 60.0 | 60.0 |  | 60.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length（m） | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util．Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  |  |  |  |  | 0.99 |  |  |  |  |  |  |
| Frt |  | 0.991 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Fit Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1807 | 1884 | 0 | 1636 | 1842 | 1633 | 1708 | 3579 | 1670 | 1655 | 3421 | 1617 |
| Flt Permitted | 0.115 |  |  | 0.326 |  |  | 0.378 |  |  | 0.082 |  |  |
| Satd．Flow（perm） | 219 | 1884 | 0 | 561 | 1842 | 1612 | 679 | 3579 | 1670 | 143 | 3421 | 1617 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  | 3 |  |  |  | 114 |  |  | 131 |  |  | 135 |
| Link Speed（k／h） |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance（m） |  | 129.9 |  |  | 1758.6 |  |  | 451.2 |  |  | 794.7 |  |
| Travel Time（s） |  | 7.8 |  |  | 105.5 |  |  | 23.2 |  |  | 40.9 |  |
| Confl．Bikes（\＃／hr） |  |  |  |  |  | 1 |  |  |  |  |  |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Heavy Vehicles（\％） | 1\％ | 1\％ | 2\％ | 3\％ | 2\％ | 0\％ | 1\％ | 2\％ | 1\％ | 3\％ | 2\％ | 1\％ |
| Adj．Flow（vph） | 276 | 533 | 36 | 151 | 488 | 186 | 99 | 1260 | 219 | 91 | 719 | 135 |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 276 | 569 | 0 | 151 | 488 | 186 | 99 | 1260 | 219 | 91 | 719 | 135 |
| Turn Type | pm＋pt | NA |  | Perm | NA | Perm | Perm | NA | Perm | pm＋pt | NA | Perm |
| Protected Phases | 7 | 4 |  |  | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 8 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 7.0 | 10.0 |  | 10.0 | 10.0 | 10.0 | 20.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 |
| Minimum Split（s） | 11.0 | 17.5 |  | 38.5 | 38.5 | 38.5 | 36.5 | 36.5 | 36.5 | 11.0 | 36.5 | 36.5 |
| Total Split（s） | 16.0 | 42.5 |  | 42.5 | 42.5 | 42.5 | 52.5 | 52.5 | 52.5 | 11.0 | 52.5 | 52.5 |
| Total Split（\％） | 13．1\％ | 34．8\％ |  | 34．8\％ | 34．8\％ | 34．8\％ | 43．0\％ | 43．0\％ | 43．0\％ | 9．0\％ | 43．0\％ | 43．0\％ |
| Maximum Green（s） | 12.0 | 35.0 |  | 35.0 | 35.0 | 35.0 | 45.0 | 45.0 | 45.0 | 7.0 | 45.0 | 45.0 |
| Yellow Time（s） | 3.0 | 4.5 |  | 4.5 | 4.5 | 4.5 | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 |
| All－Red Time（s） | 1.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 2.5 | 2.5 | 2.5 | 1.0 | 2.5 | 2.5 |
| Lost Time Adjust（s） | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.0 | 7.5 |  | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead／Lag | Lead |  |  | Lag | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes |  |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 6.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 |
| Recall Mode | None | None |  | None | None | None | Min | Min | Min | None | Min | Min |
| Walk Time（s） |  |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk（s） |  |  |  | 24.0 | 24.0 | 24.0 | 22.0 | 22.0 | 22.0 |  | 22.0 | 22.0 |
| Pedestrian Calls（\＃／hr） |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Act Effct Green（s） | 53.3 | 49.8 |  | 33.8 | 33.8 | 33.8 | 45.0 | 45.0 | 45.0 | 59.5 | 56.0 | 56.0 |
| Actuated g／C Ratio | 0.44 | 0.41 |  | 0.28 | 0.28 | 0.28 | 0.37 | 0.37 | 0.37 | 0.49 | 0.46 | 0.46 |



Splits and Phases: 220: Bathurst Street \& 18th Sideroad/St. John's Sideroad


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


|  | $\psi$ |  |  |  |  |  | 4 | 4 | \% |  | $\downarrow$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Actuated g/C Ratio | 0.41 | 0.31 |  | 0.48 | 0.34 | 0.34 | 0.28 | 0.28 | 0.28 | 0.46 | 0.43 | 0.43 |
| v/c Ratio | 1.15 | 0.78 |  | 1.01 | 1.09 | 0.99 | 0.96 | 0.97 | 0.46 | 1.18 | 0.45 | 0.23 |
| Control Delay | 141.2 | 43.1 |  | 83.3 | 100.1 | 54.8 | 98.7 | 65.4 | 12.0 | 140.8 | 25.4 | 3.9 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 141.2 | 43.1 |  | 83.3 | 100.1 | 54.8 | 98.7 | 65.4 | 12.0 | 140.8 | 25.4 | 3.9 |
| LOS | F | D |  | F | F | D | F | E | B | F | C | A |
| Approach Delay |  | 66.6 |  |  | 77.9 |  |  | 58.9 |  |  | 56.7 |  |
| Approach LOS |  | E |  |  | E |  |  | E |  |  | E |  |
| Queue Length 50th (m) | ~42.5 | 104.8 |  | ~43.3 | ~194.8 | 124.5 | 45.1 | 120.7 | 12.7 | ~89.6 | 61.7 | 0.0 |
| Queue Length 95th (m) | \#96.0 | 137.1 |  | \#101.0 | \#269.1 | \#212.2 | \#92.9 | \#165.0 | 37.6 | \#150.9 | 78.5 | 13.0 |
| Internal Link Dist (m) |  | 424.3 |  |  | 317.9 |  |  | 481.9 |  |  | 584.7 |  |
| Turn Bay Length (m) | 65.0 |  |  | 70.0 |  |  | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Base Capacity (vph) | 181 | 851 |  | 269 | 642 | 742 | 193 | 966 | 616 | 304 | 1520 | 733 |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 1.15 | 0.78 |  | 1.01 | 1.09 | 0.99 | 0.96 | 0.97 | 0.46 | 1.18 | 0.45 | 0.23 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 39 (33\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.18 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 65.9 Intersection LOS: E |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 111.1\% ICU Level of Service H |  |  |  |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| * User Entered Value |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 210: Yonge Street \& St. John's Sideroad


|  | 4 | $\rightarrow$ |  | 7 |  | 4 | 4 |  | 7 | ( | $\frac{1}{\dagger}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1 /}$ | $\uparrow$ |  | ${ }^{7}$ | 4 | F' | ${ }^{1}$ | 44 | F' | ${ }^{7}$ | 44 | 「 |
| Traffic Volume (vph) | 250 | 517 | 35 | 140 | 439 | 172 | 85 | 1105 | 229 | 96 | 670 | 120 |
| Future Volume (vph) | 250 | 517 | 35 | 140 | 439 | 172 | 85 | 1105 | 229 | 96 | 670 | 120 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.7 | 3.7 | 3.7 | 3.0 | 3.5 | 3.7 | 3.2 | 3.7 | 4.0 | 3.1 | 3.3 | 3.7 |
| Storage Length (m) | 30.0 |  | 0.0 | 50.0 |  | 50.0 | 60.0 |  | 60.0 | 60.0 |  | 60.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length (m) | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  |  |  |  |  | 0.99 |  |  |  |  |  |  |
| Frt |  | 0.991 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1807 | 1884 | 0 | 1636 | 1842 | 1633 | 1708 | 3579 | 1670 | 1655 | 3421 | 1617 |
| Flt Permitted | 0.168 |  |  | 0.314 |  |  | 0.386 |  |  | 0.091 |  |  |
| Satd. Flow (perm) | 320 | 1884 | 0 | 541 | 1842 | 1612 | 694 | 3579 | 1670 | 159 | 3421 | 1617 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 4 |  |  |  | 128 |  |  | 161 |  |  | 125 |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance (m) |  | 129.9 |  |  | 1758.6 |  |  | 451.2 |  |  | 794.7 |  |
| Travel Time (s) |  | 7.8 |  |  | 105.5 |  |  | 23.2 |  |  | 40.9 |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  | 1 |  |  |  |  |  |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Heavy Vehicles (\%) | 1\% | 1\% | 2\% | 3\% | 2\% | 0\% | 1\% | 2\% | 1\% | 3\% | 2\% | 1\% |
| Adj. Flow (vph) | 260 | 539 | 36 | 146 | 457 | 179 | 89 | 1151 | 239 | 100 | 698 | 125 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 260 | 575 | 0 | 146 | 457 | 179 | 89 | 1151 | 239 | 100 | 698 | 125 |
| Turn Type | pm+pt | NA |  | Perm | NA | Perm | Perm | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 7 | 4 |  |  | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 8 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 10.0 |  | 10.0 | 10.0 | 10.0 | 20.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 |
| Minimum Split (s) | 11.0 | 17.5 |  | 38.5 | 38.5 | 38.5 | 36.5 | 36.5 | 36.5 | 11.0 | 36.5 | 36.5 |
| Total Split (s) | 14.0 | 42.5 |  | 42.5 | 42.5 | 42.5 | 47.5 | 47.5 | 47.5 | 11.0 | 47.5 | 47.5 |
| Total Split (\%) | 12.2\% | 37.0\% |  | 37.0\% | 37.0\% | 37.0\% | 41.3\% | 41.3\% | 41.3\% | 9.6\% | 41.3\% | 41.3\% |
| Maximum Green (s) | 10.0 | 35.0 |  | 35.0 | 35.0 | 35.0 | 40.0 | 40.0 | 40.0 | 7.0 | 40.0 | 40.0 |
| Yellow Time (s) | 3.0 | 4.5 |  | 4.5 | 4.5 | 4.5 | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 |
| All-Red Time (s) | 1.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 2.5 | 2.5 | 2.5 | 1.0 | 2.5 | 2.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.0 | 7.5 |  | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead/Lag | Lead |  |  | Lag | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 6.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 |
| Recall Mode | None | None |  | None | None | None | Min | Min | Min | None | Min | Min |
| Walk Time (s) |  |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk (s) |  |  |  | 24.0 | 24.0 | 24.0 | 22.0 | 22.0 | 22.0 |  | 22.0 | 22.0 |
| Pedestrian Calls (\#/hr) |  |  |  | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Act Effct Green (s) | 49.3 | 45.8 |  | 31.7 | 31.7 | 31.7 | 40.1 | 40.1 | 40.1 | 54.6 | 51.1 | 51.1 |
| Actuated g/C Ratio | 0.44 | 0.41 |  | 0.28 | 0.28 | 0.28 | 0.36 | 0.36 | 0.36 | 0.49 | 0.46 | 0.46 |



Splits and Phases: 220: Bathurst Street \& 18th Sideroad/St. John's Sideroad


|  | 4 |  |  | 7 |  | 4 | 4 | 4 | \% | $1$ | $\ddagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 4 | 「 | ${ }^{7}$ | 4 | 「 |  | \& |  | ${ }^{7}$ | F |  |
| Traffic Volume (vph) | 80 | 722 | 6 | 60 | 845 | 94 | 5 | 3 | 46 | 63 | 1 | 25 |
| Future Volume (vph) | 80 | 722 | 6 | 60 | 845 | 94 | 5 | 3 | 46 | 63 | 1 | 25 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.0 | 3.7 | 3.7 | 3.4 | 3.3 | 3.3 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 |
| Storage Length (m) | 15.0 |  | 15.0 | 30.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 0 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  |  | 0.850 |  |  | 0.850 |  | 0.885 |  |  | 0.855 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  |  | 0.995 |  | 0.950 |  |  |
| Satd. Flow (prot) | 1685 | 1902 | 1633 | 1765 | 1818 | 1561 | 0 | 1692 | 0 | 1825 | 1643 | 0 |
| Flt Permitted | 0.209 |  |  | 0.284 |  |  |  | 0.960 |  | 0.717 |  |  |
| Satd. Flow (perm) | 371 | 1902 | 1633 | 528 | 1818 | 1561 | 0 | 1632 | 0 | 1377 | 1643 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 55 |  |  | 106 |  | 52 |  |  | 28 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 40 |  |  | 50 |  |
| Link Distance (m) |  | 1758.6 |  |  | 448.3 |  |  | 195.4 |  |  | 116.6 |  |
| Travel Time (s) |  | 105.5 |  |  | 26.9 |  |  | 17.6 |  |  | 8.4 |  |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles (\%) | 0\% | 1\% | 0\% | 0\% | 1\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% |
| Adj. Flow (vph) | 90 | 811 | 7 | 67 | 949 | 106 | 6 | 3 | 52 | 71 | 1 | 28 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 90 | 811 | 7 | 67 | 949 | 106 | 0 | 61 | 0 | 71 | 29 | 0 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 8 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 | 2 | 6 | 6 | 6 | 8 | 8 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 24.0 | 24.0 | 24.0 | 24.0 | 24.0 | 24.0 | 27.0 | 27.0 |  | 27.0 | 27.0 |  |
| Total Split (s) | 33.0 | 33.0 | 33.0 | 33.0 | 33.0 | 33.0 | 27.0 | 27.0 |  | 27.0 | 27.0 |  |
| Total Split (\%) | 55.0\% | 55.0\% | 55.0\% | 55.0\% | 55.0\% | 55.0\% | 45.0\% | 45.0\% |  | 45.0\% | 45.0\% |  |
| Maximum Green (s) | 27.0 | 27.0 | 27.0 | 27.0 | 27.0 | 27.0 | 21.0 | 21.0 |  | 21.0 | 21.0 |  |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | C-Max | C-Max | C-Max | C-Max | C-Max | C-Max | None | None |  | None | None |  |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 9.0 | 9.0 | 9.0 | 9.0 | 9.0 | 9.0 | 14.0 | 14.0 |  | 14.0 | 14.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Act Effct Green (s) | 46.7 | 46.7 | 46.7 | 46.7 | 46.7 | 46.7 |  | 8.3 |  | 8.6 | 8.6 |  |
| Actuated g/C Ratio | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 |  | 0.14 |  | 0.14 | 0.14 |  |
| v/c Ratio | 0.31 | 0.55 | 0.01 | 0.16 | 0.67 | 0.09 |  | 0.23 |  | 0.36 | 0.11 |  |
| Control Delay | 9.3 | 7.5 | 0.0 | 2.1 | 9.3 | 0.2 |  | 10.8 |  | 27.6 | 10.2 |  |


|  |  |  |  |  |  |  |  | 4 |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 9.3 | 7.5 | 0.0 | 2.1 | 9.3 | 0.2 |  | 10.8 |  | 27.6 | 10.2 |  |
| LOS | A | A | A | A | A | A |  | B |  | C | B |  |
| Approach Delay |  | 7.6 |  |  | 8.0 |  |  | 10.8 |  |  | 22.6 |  |
| Approach LOS |  | A |  |  | A |  |  | B |  |  | C |  |
| Queue Length 50th (m) | 3.8 | 45.3 | 0.0 | 1.0 | 35.5 | 0.0 |  | 0.9 |  | 7.6 | 0.1 |  |
| Queue Length 95th (m) | 15.3 | 93.0 | 0.0 | m1.8 | m178.8 | m0.0 |  | 9.0 |  | 16.7 | 5.7 |  |
| Internal Link Dist (m) |  | 1734.6 |  |  | 424.3 |  |  | 171.4 |  |  | 92.6 |  |
| Turn Bay Length (m) | 15.0 |  | 15.0 | 30.0 |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 289 | 1481 | 1284 | 411 | 1416 | 1239 |  | 605 |  | 481 | 593 |  |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.31 | 0.55 | 0.01 | 0.16 | 0.67 | 0.09 |  | 0.10 |  | 0.15 | 0.05 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 60 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 60 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: $11(18 \%)$, Referenced to phase 2:EBTL and 6:WBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 80 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.67 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 8.6 |  |  |  |  | intersection | LOS: A |  |  |  |  |  |  |
| Intersection Capacity Utilization 74.1\% |  |  |  | ICU Level of Service D |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| $m$ Volume for 95th percentile queue is metered by upstream signal. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 330: Willow Farm Lane/Street "A" \& St. John's Sideroad


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


|  | $\psi$ |  |  |  |  |  | 4 | 4 | \% |  | $\frac{1}{7}$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Actuated g/C Ratio | 0.41 | 0.31 |  | 0.48 | 0.35 | 0.35 | 0.38 | 0.28 | 0.28 | 0.45 | 0.31 | 0.31 |
| v/c Ratio | 1.24 | 0.86 |  | 1.10 | 1.15 | 1.12 | 0.69 | 1.01 | 0.47 | 1.28 | 0.63 | 0.30 |
| Control Delay | 170.6 | 48.6 |  | 113.0 | 120.8 | 98.7 | 36.9 | 74.7 | 11.1 | 181.3 | 38.4 | 5.8 |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 170.6 | 48.6 |  | 113.0 | 120.8 | 98.7 | 36.9 | 74.7 | 11.1 | 181.3 | 38.4 | 5.8 |
| LOS | F | D |  | F | F | F | D | E | B | F | D | A |
| Approach Delay |  | 77.4 |  |  | 110.1 |  |  | 56.8 |  |  | 76.0 |  |
| Approach LOS |  | E |  |  | F |  |  | E |  |  | E |  |
| Queue Length 50th (m) | ~49.9 | 119.8 |  | ~59.9 | ~220.7 | ~186.8 | 28.7 | ~129.8 | 11.5 | ~99.4 | 77.7 | 0.0 |
| Queue Length 95th (m) | \#104.6 | \#154.0 |  | \#117.1 | \#297.0 | \#265.0 | \#47.7 | \#175.8 | 36.9 | \#161.8 | 98.8 | 16.3 |
| Internal Link Dist (m) |  | 424.3 |  |  | 317.9 |  |  | 481.9 |  |  | 584.7 |  |
| Turn Bay Length (m) | 65.0 |  |  | 70.0 |  |  | 35.0 |  | 100.0 | 115.0 |  | 230.0 |
| Base Capacity (vph) | 181 | 850 |  | 258 | 658 | 699 | 276 | 966 | 630 | 287 | 1107 | 587 |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 1.24 | 0.86 |  | 1.10 | 1.15 | 1.12 | 0.69 | 1.01 | 0.47 | 1.28 | 0.63 | 0.30 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 0 (0\%), Referenced to phase 2:SBTL and 6:NBTL, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 150 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.28 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 82.5 Intersection LOS: F |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 115.3\% ICU Level of Service H |  |  |  |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| * User Entered Value |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 210: Yonge Street \& St. John's Sideroad


|  | 4 | $\rightarrow$ |  | 7 |  |  | 4 |  | 7 | ( | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1 /}$ | $\uparrow$ |  | ${ }^{7}$ | 4 | F | ${ }^{1 /}$ | 44 | F' | ${ }^{7}$ | 44 | 「 |
| Traffic Volume (vph) | 265 | 542 | 35 | 158 | 485 | 192 | 95 | 1210 | 239 | 101 | 690 | 130 |
| Future Volume (vph) | 265 | 542 | 35 | 158 | 485 | 192 | 95 | 1210 | 239 | 101 | 690 | 130 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.7 | 3.7 | 3.7 | 3.0 | 3.5 | 3.7 | 3.2 | 3.7 | 4.0 | 3.1 | 3.3 | 3.7 |
| Storage Length (m) | 30.0 |  | 0.0 | 50.0 |  | 50.0 | 60.0 |  | 60.0 | 60.0 |  | 60.0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 1 | 1 |  | 1 | 1 |  | 1 |
| Taper Length (m) | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor |  |  |  |  |  | 0.99 |  |  |  |  |  |  |
| Frt |  | 0.991 |  |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1807 | 1884 | 0 | 1636 | 1842 | 1633 | 1708 | 3579 | 1670 | 1655 | 3421 | 1617 |
| Flt Permitted | 0.104 |  |  | 0.116 |  |  | 0.378 |  |  | 0.082 |  |  |
| Satd. Flow (perm) | 198 | 1884 | 0 | 200 | 1842 | 1612 | 679 | 3579 | 1670 | 143 | 3421 | 1617 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 3 |  |  |  | 119 |  |  | 149 |  |  | 135 |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 70 |  |  | 70 |  |
| Link Distance (m) |  | 129.9 |  |  | 1758.6 |  |  | 451.2 |  |  | 794.7 |  |
| Travel Time (s) |  | 7.8 |  |  | 105.5 |  |  | 23.2 |  |  | 40.9 |  |
| Confl. Bikes (\#/hr) |  |  |  |  |  | 1 |  |  |  |  |  |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Heavy Vehicles (\%) | 1\% | 1\% | 2\% | 3\% | 2\% | 0\% | 1\% | 2\% | 1\% | 3\% | 2\% | 1\% |
| Adj. Flow (vph) | 276 | 565 | 36 | 165 | 505 | 200 | 99 | 1260 | 249 | 105 | 719 | 135 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 276 | 601 | 0 | 165 | 505 | 200 | 99 | 1260 | 249 | 105 | 719 | 135 |
| Turn Type | pm+pt | NA |  | pm+pt | NA | Perm | Perm | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 6 |  | 5 | 2 |  |
| Permitted Phases | 4 |  |  | 8 |  | 8 | 6 |  | 6 | 2 |  | 2 |
| Detector Phase | 7 | 4 |  | 3 | 8 | 8 | 6 | 6 | 6 | 5 | 2 | 2 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 7.0 | 10.0 |  | 7.0 | 10.0 | 10.0 | 20.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 |
| Minimum Split (s) | 11.0 | 17.5 |  | 11.0 | 38.5 | 38.5 | 36.5 | 36.5 | 36.5 | 11.0 | 36.5 | 36.5 |
| Total Split (s) | 16.0 | 42.5 |  | 12.0 | 42.5 | 42.5 | 52.5 | 52.5 | 52.5 | 11.0 | 52.5 | 52.5 |
| Total Split (\%) | 13.1\% | 34.8\% |  | 9.8\% | 34.8\% | 34.8\% | 43.0\% | 43.0\% | 43.0\% | 9.0\% | 43.0\% | 43.0\% |
| Maximum Green (s) | 12.0 | 35.0 |  | 8.0 | 35.0 | 35.0 | 45.0 | 45.0 | 45.0 | 7.0 | 45.0 | 45.0 |
| Yellow Time (s) | 3.0 | 4.5 |  | 3.0 | 4.5 | 4.5 | 5.0 | 5.0 | 5.0 | 3.0 | 5.0 | 5.0 |
| All-Red Time (s) | 1.0 | 3.0 |  | 1.0 | 3.0 | 3.0 | 2.5 | 2.5 | 2.5 | 1.0 | 2.5 | 2.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.0 | 7.5 |  | 4.0 | 7.5 | 7.5 | 7.5 | 7.5 | 7.5 | 4.0 | 7.5 | 7.5 |
| Lead/Lag | Lead | Lag |  | Lead | Lag | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead-Lag Optimize? | Yes | Yes |  | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 6.0 | 6.0 | 6.0 | 3.0 | 6.0 | 6.0 |
| Recall Mode | None | None |  | None | None | None | Min | Min | Min | None | Min | Min |
| Walk Time (s) |  |  |  |  | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |
| Flash Dont Walk (s) |  |  |  |  | 24.0 | 24.0 | 22.0 | 22.0 | 22.0 |  | 22.0 | 22.0 |
| Pedestrian Calls (\#/hr) |  |  |  |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Act Effct Green (s) | 54.0 | 38.5 |  | 46.0 | 34.5 | 34.5 | 45.0 | 45.0 | 45.0 | 59.5 | 56.0 | 56.0 |
| Actuated g/C Ratio | 0.44 | 0.32 |  | 0.38 | 0.28 | 0.28 | 0.37 | 0.37 | 0.37 | 0.49 | 0.46 | 0.46 |



Splits and Phases: 220: Bathurst Street \& 18th Sideroad/St. John's Sideroad


|  | 4 |  |  | 7 |  | 4 | 4 | $\dagger$ | 7 | $t$ | $\frac{1}{\dagger}$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 4 | 「 | ${ }^{7}$ | 4 | 「 |  | * |  | ${ }^{7}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 80 | 762 | 6 | 60 | 915 | 94 | 5 | 3 | 46 | 98 | 3 | 50 |
| Future Volume (vph) | 80 | 762 | 6 | 60 | 915 | 94 | 5 | 3 | 46 | 98 | 3 | 50 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.0 | 3.7 | 3.7 | 3.4 | 3.3 | 3.3 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 | 3.7 |
| Storage Length (m) | 15.0 |  | 15.0 | 30.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 1 | 0 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  | 7.5 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  |  | 0.850 |  |  | 0.850 |  | 0.885 |  |  | 0.858 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  |  | 0.995 |  | 0.950 |  |  |
| Satd. Flow (prot) | 1685 | 1902 | 1633 | 1765 | 1818 | 1561 | 0 | 1692 | 0 | 1825 | 1648 | 0 |
| Flt Permitted | 0.128 |  |  | 0.230 |  |  |  | 0.963 |  | 0.717 |  |  |
| Satd. Flow (perm) | 227 | 1902 | 1633 | 427 | 1818 | 1561 | 0 | 1637 | 0 | 1377 | 1648 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 55 |  |  | 106 |  | 52 |  |  | 51 |  |
| Link Speed (k/h) |  | 60 |  |  | 60 |  |  | 40 |  |  | 50 |  |
| Link Distance (m) |  | 1758.6 |  |  | 448.3 |  |  | 195.4 |  |  | 116.6 |  |
| Travel Time (s) |  | 105.5 |  |  | 26.9 |  |  | 17.6 |  |  | 8.4 |  |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles (\%) | 0\% | 1\% | 0\% | 0\% | 1\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% | 0\% |
| Adj. Flow (vph) | 90 | 856 | 7 | 67 | 1028 | 106 | 6 | 3 | 52 | 110 | 3 | 56 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 90 | 856 | 7 | 67 | 1028 | 106 | 0 | 61 | 0 | 110 | 59 | 0 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | Perm | NA |  | Perm | NA |  |
| Protected Phases |  | 2 |  |  | 6 |  |  | 8 |  |  | 4 |  |
| Permitted Phases | 2 |  | 2 | 6 |  | 6 | 8 |  |  | 4 |  |  |
| Detector Phase | 2 | 2 | 2 | 6 | 6 | 6 | 8 | 8 |  | 4 | 4 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Minimum Split (s) | 24.0 | 24.0 | 24.0 | 24.0 | 24.0 | 24.0 | 27.0 | 27.0 |  | 27.0 | 27.0 |  |
| Total Split (s) | 33.0 | 33.0 | 33.0 | 33.0 | 33.0 | 33.0 | 27.0 | 27.0 |  | 27.0 | 27.0 |  |
| Total Split (\%) | 55.0\% | 55.0\% | 55.0\% | 55.0\% | 55.0\% | 55.0\% | 45.0\% | 45.0\% |  | 45.0\% | 45.0\% |  |
| Maximum Green (s) | 27.0 | 27.0 | 27.0 | 27.0 | 27.0 | 27.0 | 21.0 | 21.0 |  | 21.0 | 21.0 |  |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  |  |  |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | C-Max | C-Max | C-Max | C-Max | C-Max | C-Max | None | None |  | None | None |  |
| Walk Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 |  | 7.0 | 7.0 |  |
| Flash Dont Walk (s) | 9.0 | 9.0 | 9.0 | 9.0 | 9.0 | 9.0 | 14.0 | 14.0 |  | 14.0 | 14.0 |  |
| Pedestrian Calls (\#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Act Effct Green (s) | 41.4 | 41.4 | 41.4 | 41.4 | 41.4 | 41.4 |  | 10.1 |  | 10.1 | 10.1 |  |
| Actuated g/C Ratio | 0.69 | 0.69 | 0.69 | 0.69 | 0.69 | 0.69 |  | 0.17 |  | 0.17 | 0.17 |  |
| v/c Ratio | 0.58 | 0.65 | 0.01 | 0.23 | 0.82 | 0.10 |  | 0.19 |  | 0.48 | 0.18 |  |
| Control Delay | 30.8 | 11.7 | 0.0 | 5.5 | 16.0 | 1.2 |  | 9.4 |  | 28.5 | 9.2 |  |



Splits and Phases: 330: Willow Farm Lane/Street "A" \& St. John's Sideroad



[^0]:    ${ }^{1}$ Shining Hill Estates, Phase 3, Towns of Newmarket and Aurora, Transportation Mobility Plan, October 2019. At that time, the remainder of the overall development was referred to as "Phase 3". The current subarea is now being referred to as Phase 3, and in this report the remainder of the development lands are being referred to as the "overall development".

[^1]:    ${ }^{2}$ At the time of this report, YRT is operating a modified route network and service plan due to reduced ridership during the ongoing COVID-19 pandemic. Some routes, including 31 Aurora North, are temporarily suspended, while others are operating at reduced headways. The descriptions and schedule information shown in this report refer to conditions that existed prior to the beginning of the pandemic in March 2020.

[^2]:    ${ }^{3}$ Mekuria, M., Furth, P., \& Nixon, H. (2012). Low-stress bicycling and network connectivity (MTI report 11-19). San Jose: Mineta Transportation Institute. Accessed at https://transweb.sjsu.edu/sites/default/files/1005-low-stress-bicycling-networkconnectivity.pdf
    ${ }^{4}$ http://www.northeastern.edu/peter.furth/research/level-of-traffic-stress/

[^3]:    ${ }^{5}$ http://www.northeastern.edu/peter.furth/wp-content/uploads/2014/05/LTS-Tables1.pdf

